

Design and Development of a Low Cost, Manufacturable High Voltage Power Module for Energy Storage Systems

DOE Phase II SBIR

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Motivation

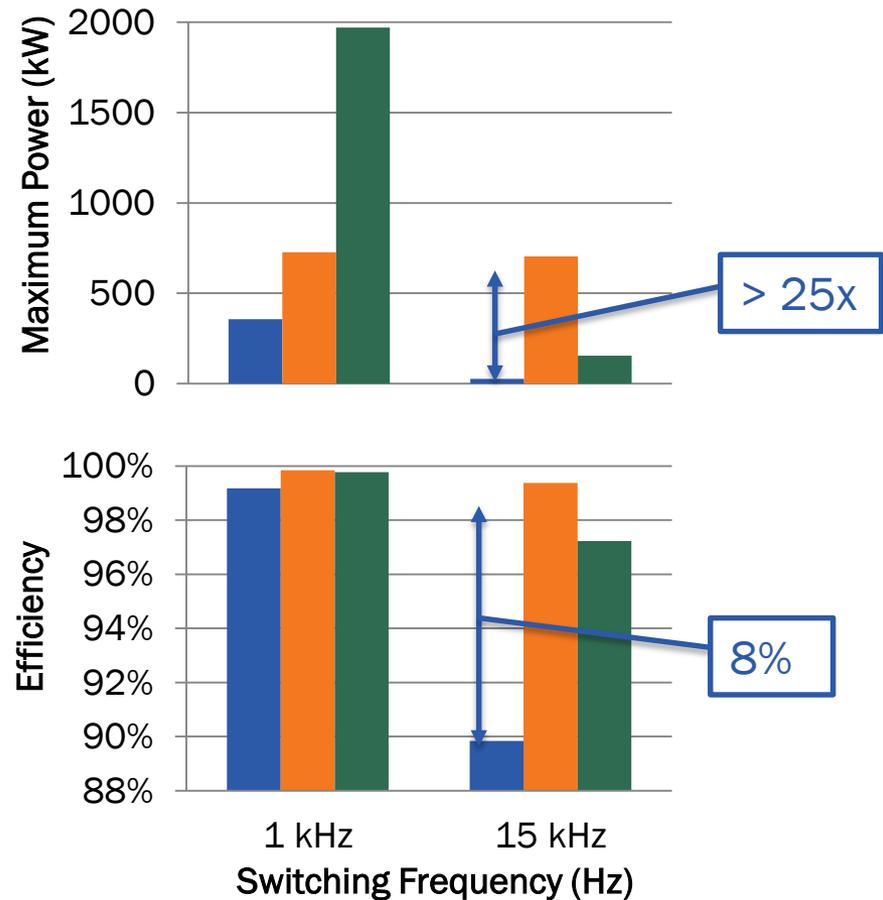
Wide bandgap enables higher efficiency and power density

Objective

Develop a high voltage (> 15kV) silicon carbide (SiC) power module to aid in the emergence of smarter, seamless powered grids.

Applications

- Energy storage systems
- Solid-state transformers
- Naval power distribution
- Electric locomotives
- Medium voltage drives
- Solid-state circuit breakers

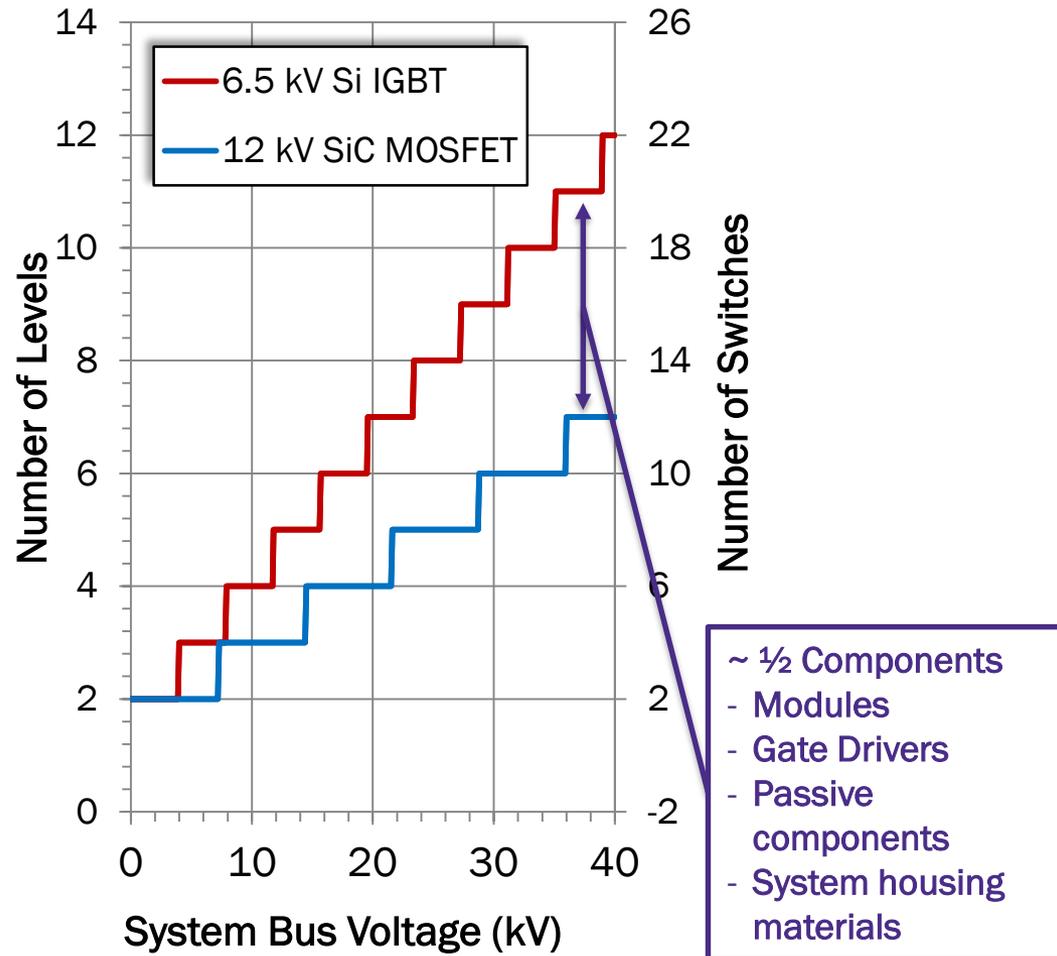


■ 6.5 kV 200 A Si IGBT ■ 10 kV 50 A SiC MOSFET ■ 15 kV 100 A SiC IGBT

Motivation - Reduce System Complexity, Reduce Cost

Advantages

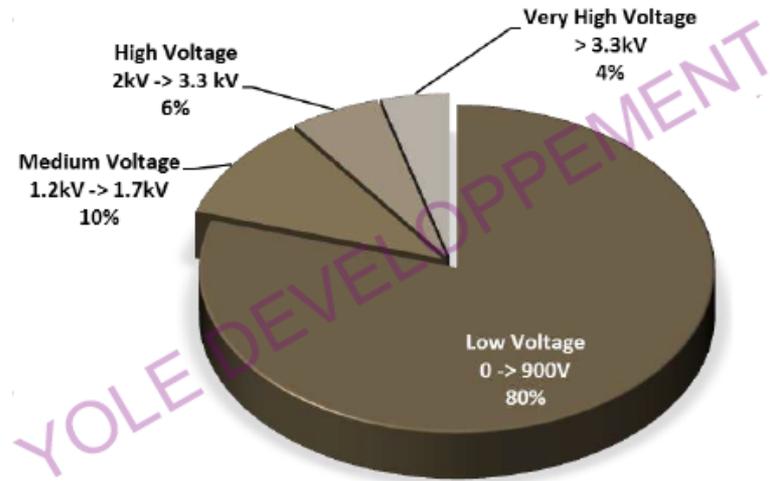
- Reduce size/complexity of multi-level systems
- Eliminate cooling systems
- Increase efficiency and power density



Power Electronics and Energy Storage Market

SiC Power Electronics Market

- < 600 V - Strong Competition With Si and GaN
- > 1.2 kV – Ideal Area for SiC; Apps are less cost driven and performance improvement is obvious



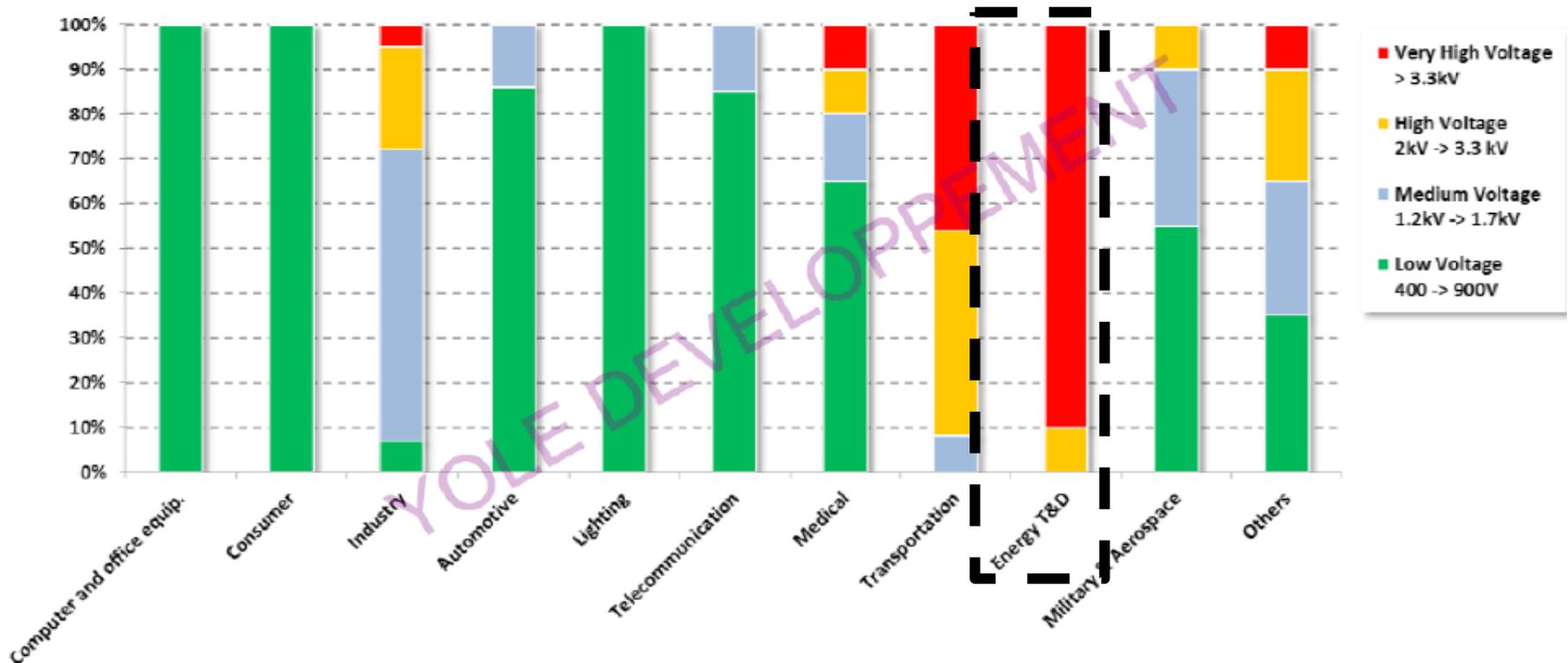
Power electronics market split by voltage range

Source: Yole Développement 2012

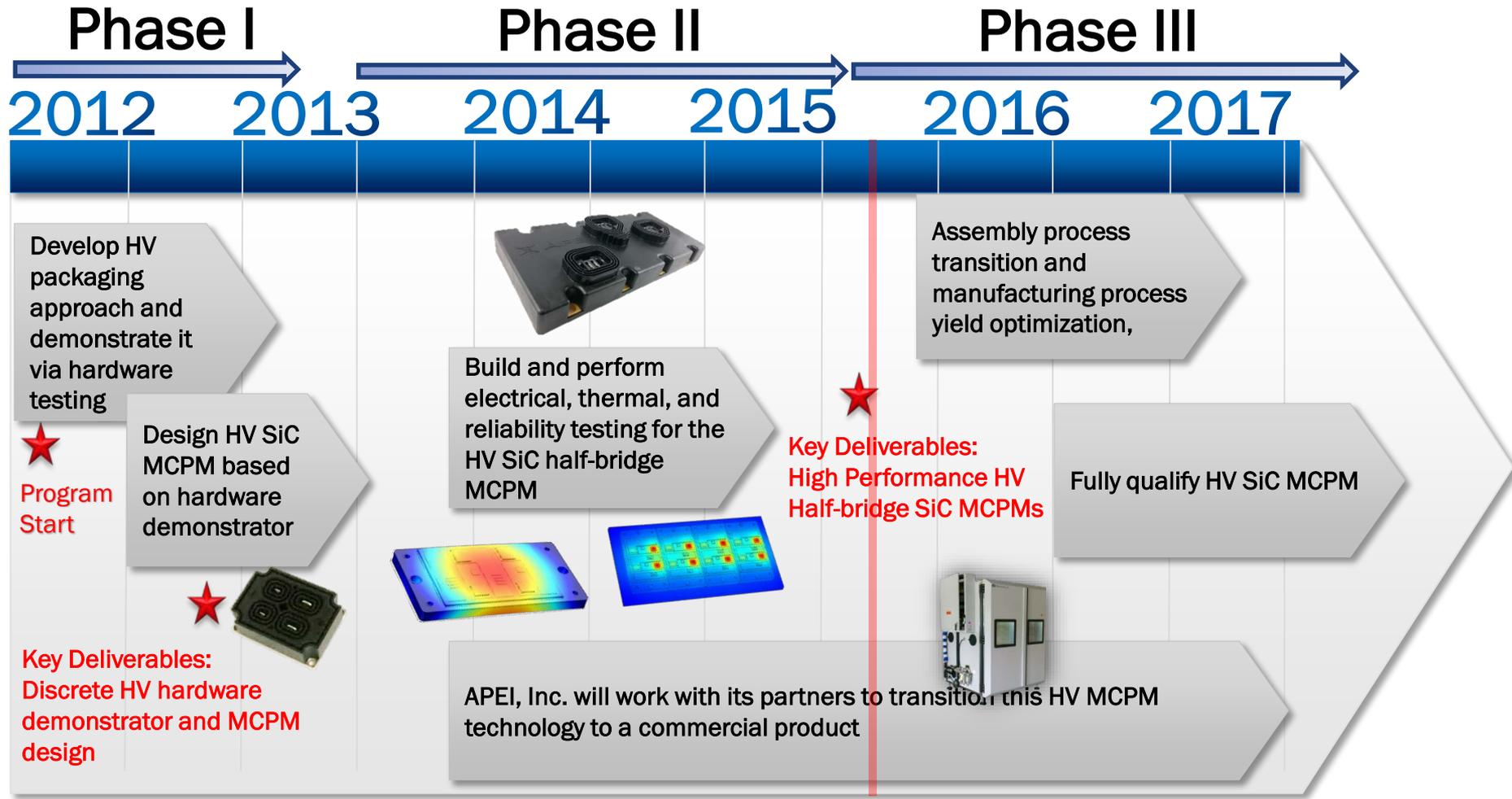
Energy Storage Market

- The global energy storage market is expected to grow from \$39.7B in 2011 to \$61.9B by 2016 at an annual growth rate of 9.3% [1]

Market Segmentation in Power Electronics by Application and Voltage



Project Plan



Design Features of XHV-3

Advantages of SiC Devices

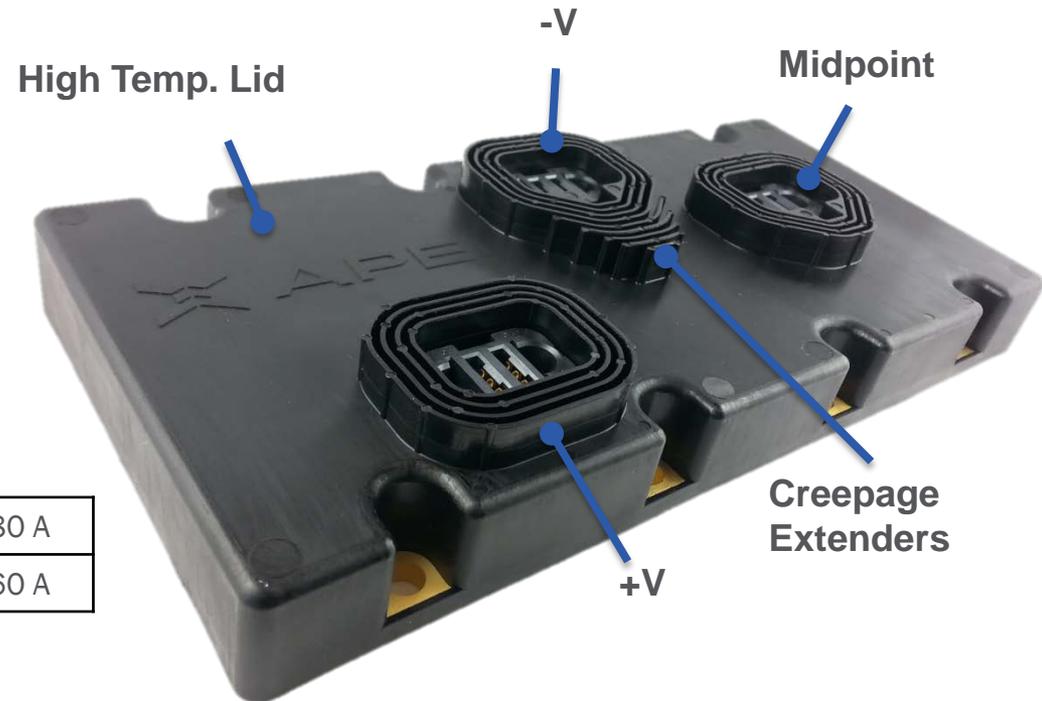
- High breakdown voltage
- High thermal conductivity
- High switching frequency
- High temperature operation

Power Module Features

- SiC MOSFETs or SiC IGBTs

| | | |
|-----------------|-------|------|
| SiC IGBT MCPM | 15 kV | 80 A |
| SiC MOSFET MCPM | 10 kV | 60 A |

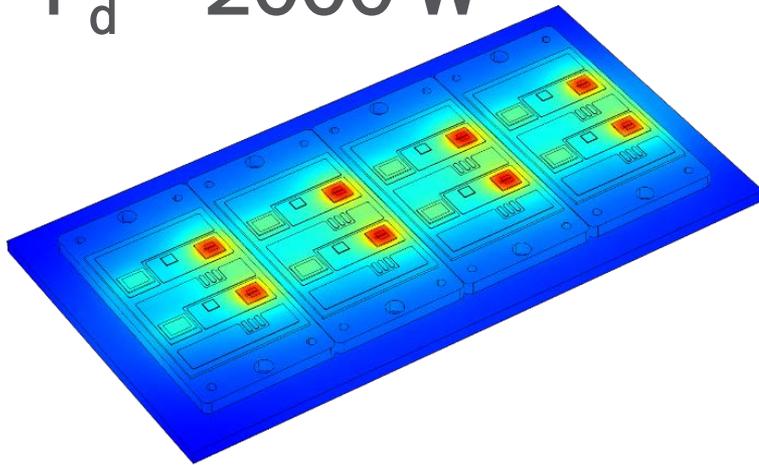
- Low profile
- Reduced volume/weight
- High temperature capable
- Reworkable



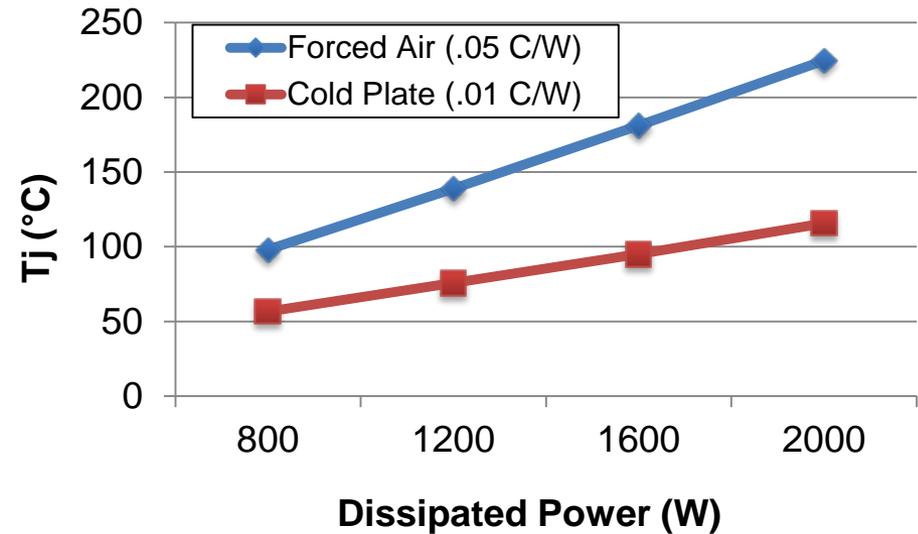
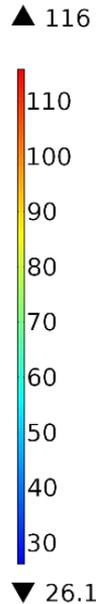
210 mm × 102 mm × 32 mm

Thermal Modeling Results

$P_d = 2000 \text{ W}$



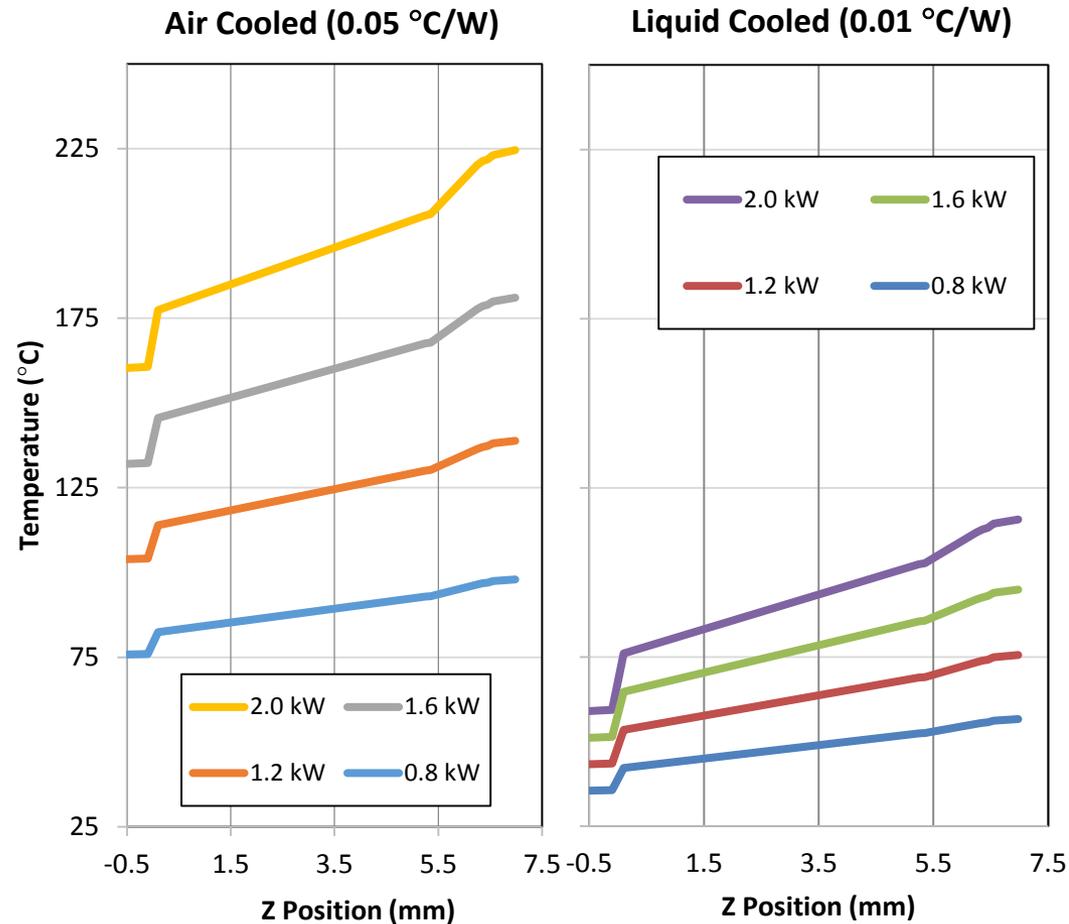
$R_{jc} < 0.06 \text{ } ^\circ\text{C/W}$
(per switch position)



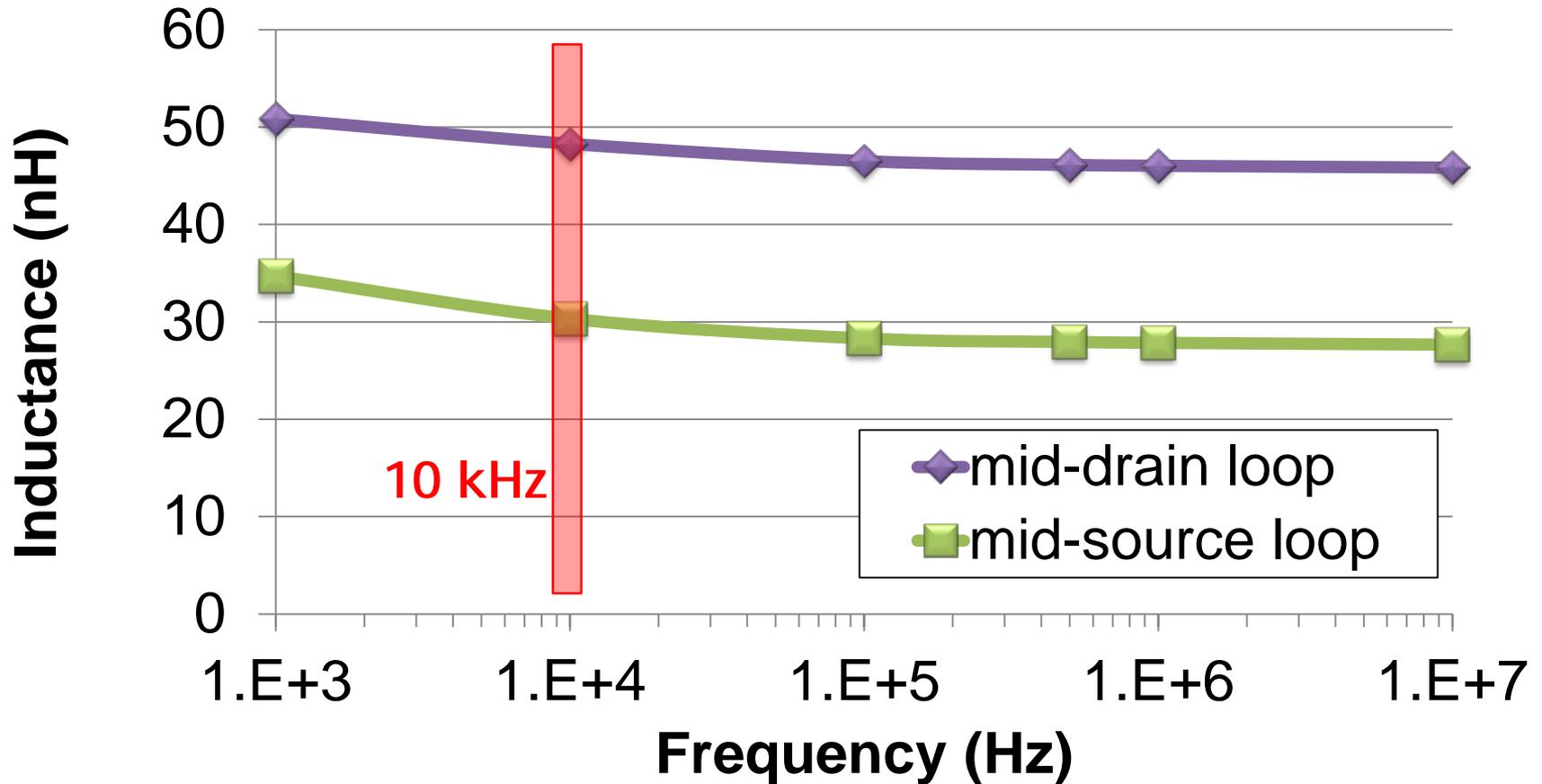
Thermal Simulations

The change in temperature through the thickness of the power module stack-up for a (top) fan-cooled heat sink and (bottom) liquid cold plate.

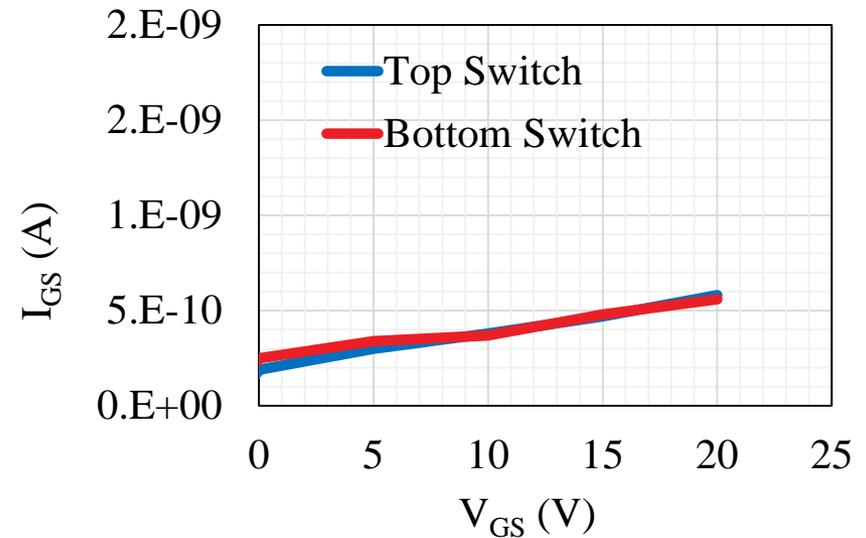
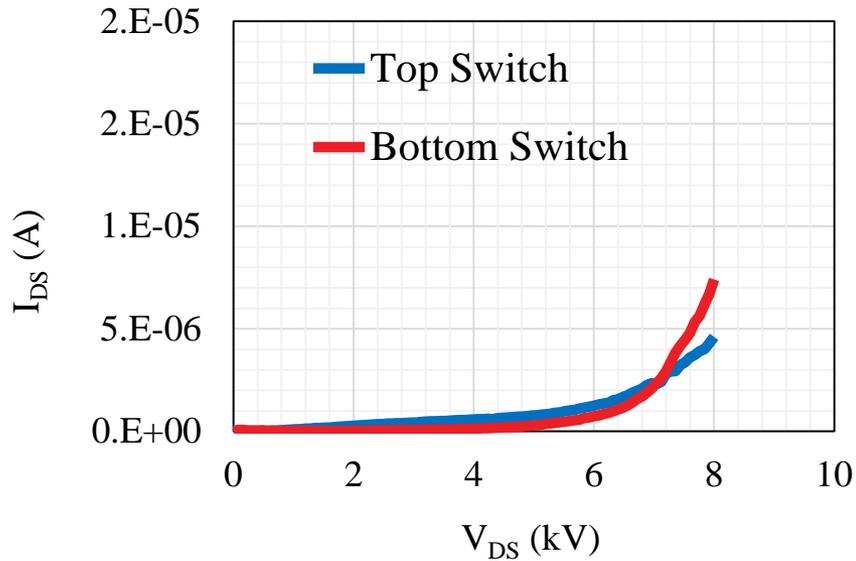
Thick dielectric necessary for voltage isolation hinders thermal performance



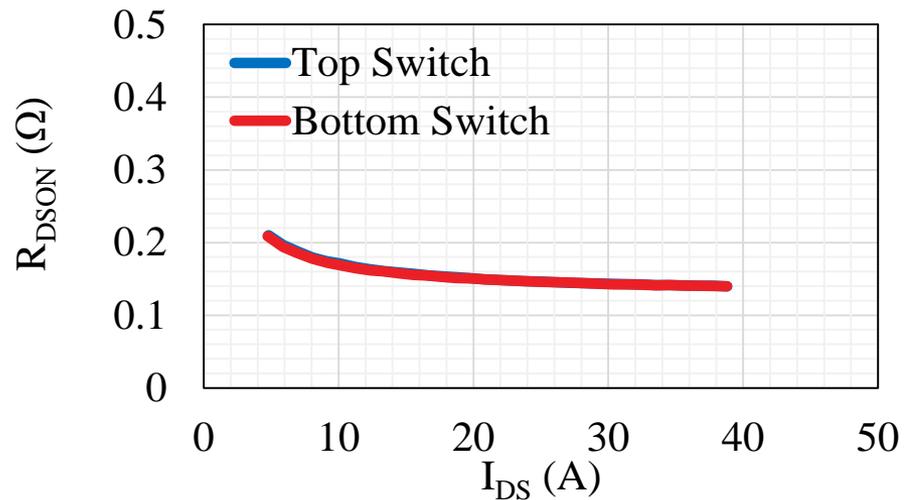
Parasitic Simulations



Static Testing

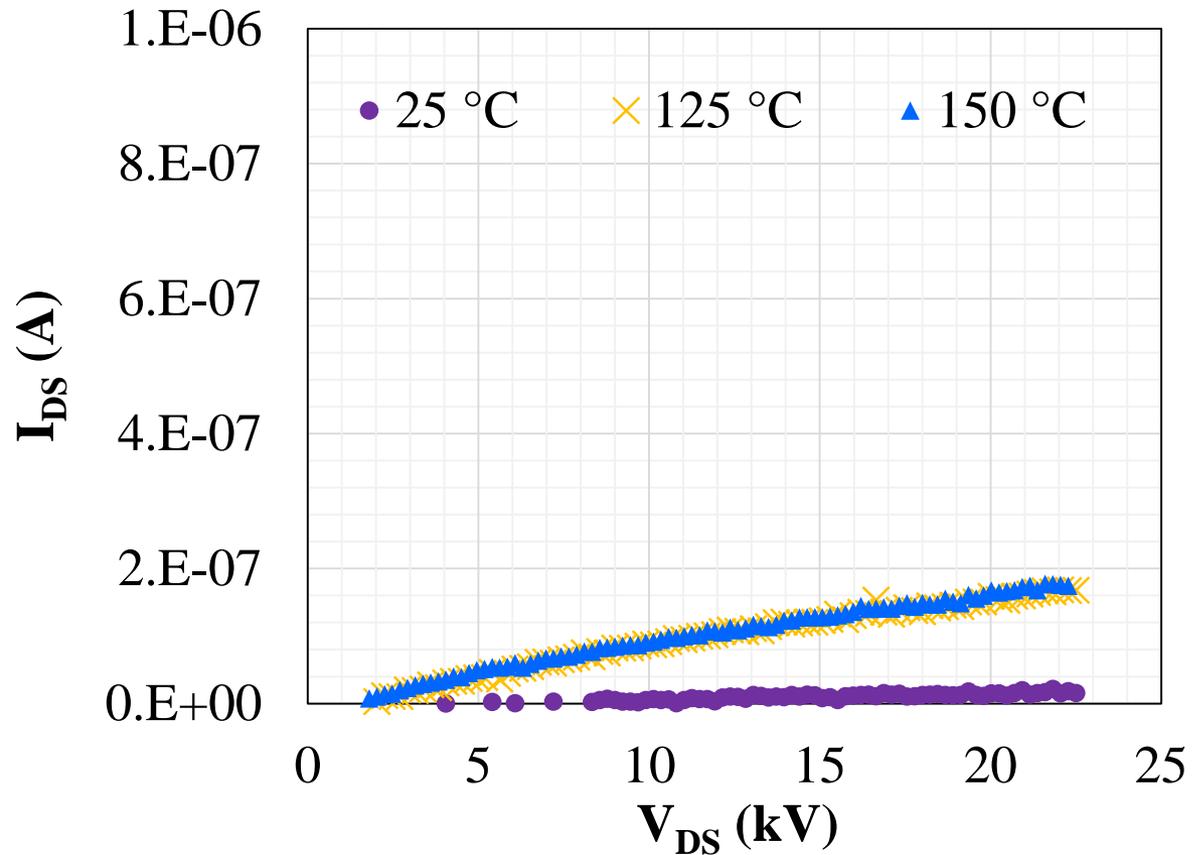


Four 10 kV / 10 A SiC MOSFETs and Four 10 kV / 10 A Schottky Diodes Per Switch Position



High Voltage, High Temperature Static Isolation Tests

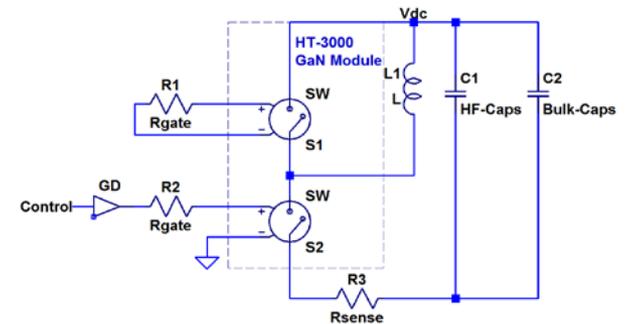
- Tested BV and leakage of a fully assembled/potted module as a function of temperature
- Isolation test = All connections were shorted and the baseplate was connected to low
- The leakage was less than 0.2 μA at 150 $^{\circ}\text{C}$.
- This is orders of magnitude lower than the device leakage at temperature



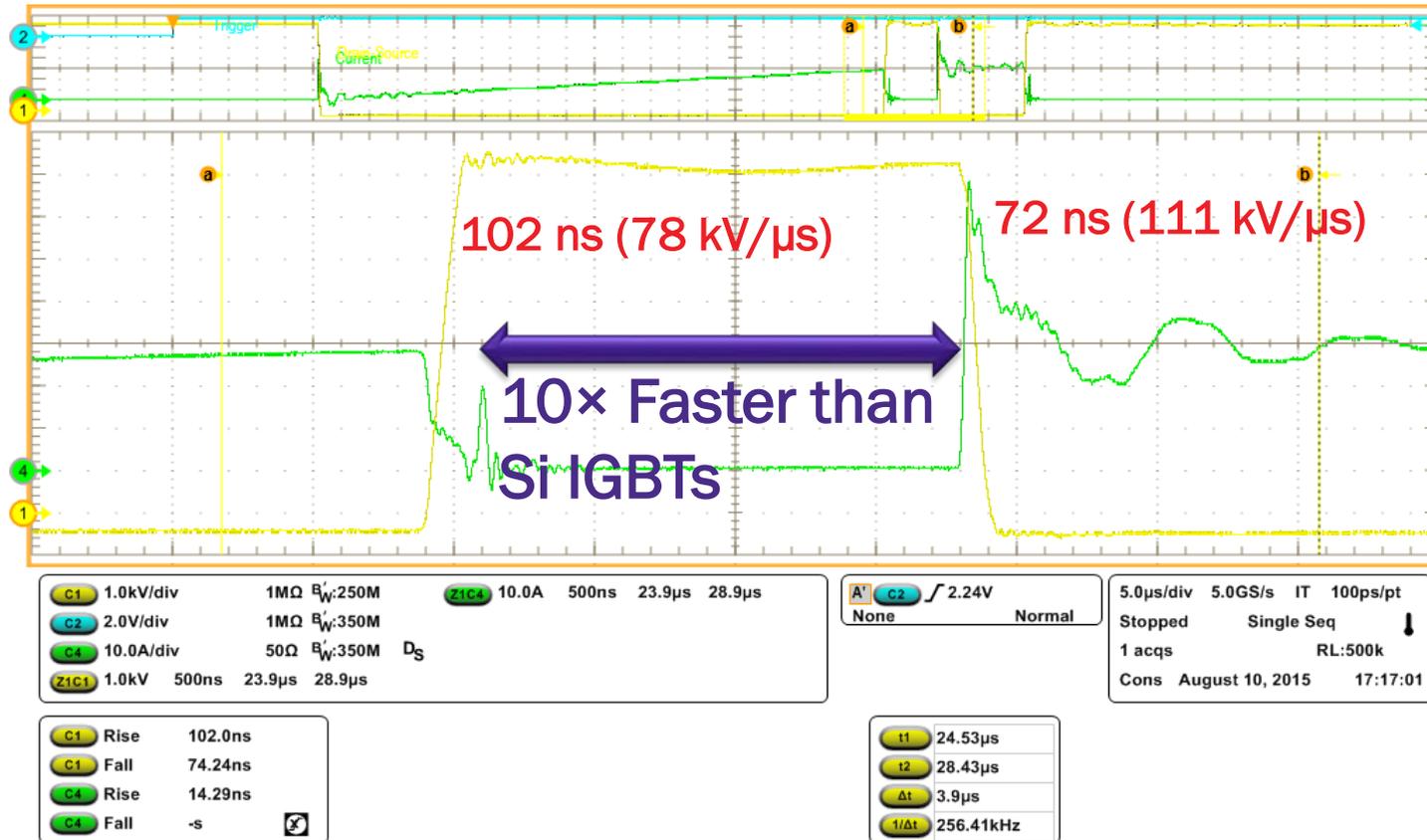
Dynamic Testing

Double Pulse Test Setup Utilizing a Clamped Inductive Load (CIL)

- Two controlled pulses turn DUT on and off
- Inductive load facilitates control of current through the DUT
- Allows for measurement of turn-on and turn-off switching losses at desired drain-to-source voltages and currents
- Gate Drive Circuit
 - 10 kV Isolation, 10 kV DC rail capable
 - Controllable gate output rails (Set at +20V / -5V)
 - Gate resistor was varied to control speed of switch: 2.5 Ω , 10 Ω , and 20 Ω
- Safety
 - Test Setup has multiple mechanical fail safes
 - Test Setup is completely controlled via wireless communication

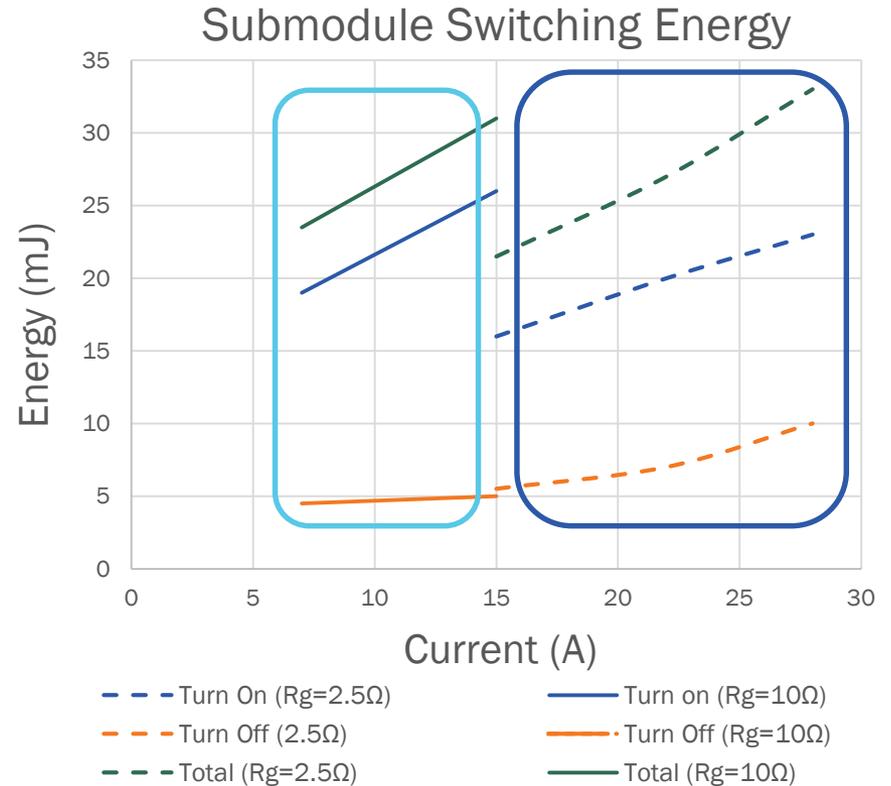
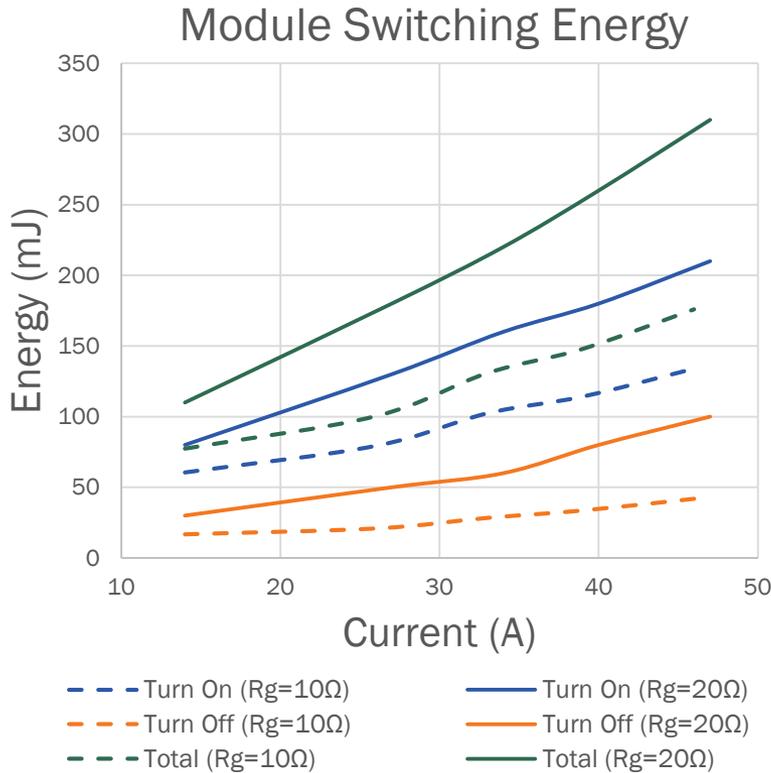


Switch Curves of Submodule



- $R_g=2.5$ Ohms, $I_{test} = 28$ A
- Voltage fall time (turn-on) has increased but not in the same amount
- Voltage Rise time (turn-off) has reduced to 100ns during turn off

Switching Losses vs. Current at 8 kV



- Total switching losses for a commercial Si 6.5 kV / 250 A module are ~ 2.6 J [3]
- **This higher power density SiC Module has over an order of magnitude lower losses**

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