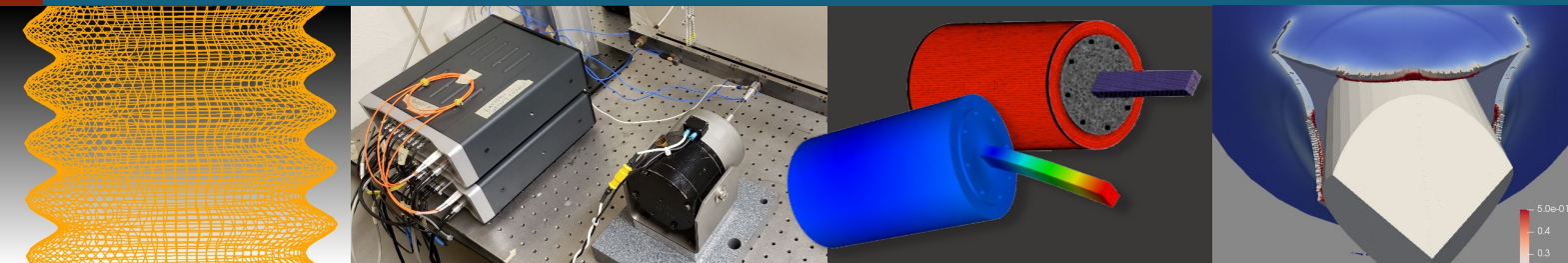


Empirical Model of Puncture Energy for Metals



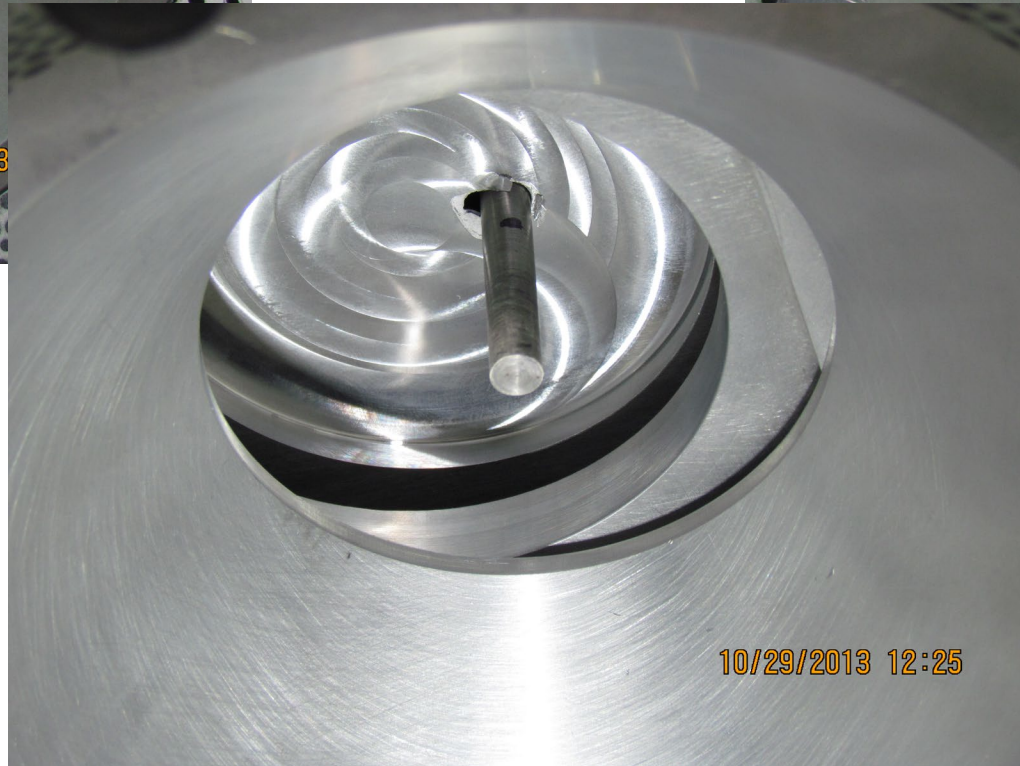
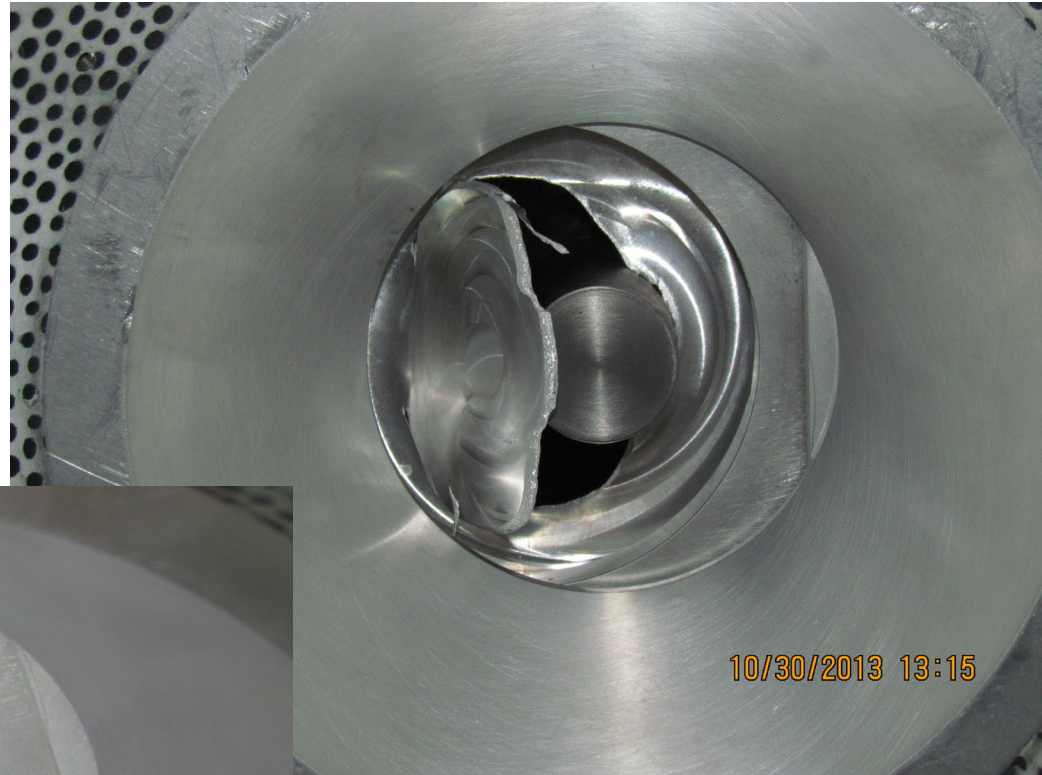
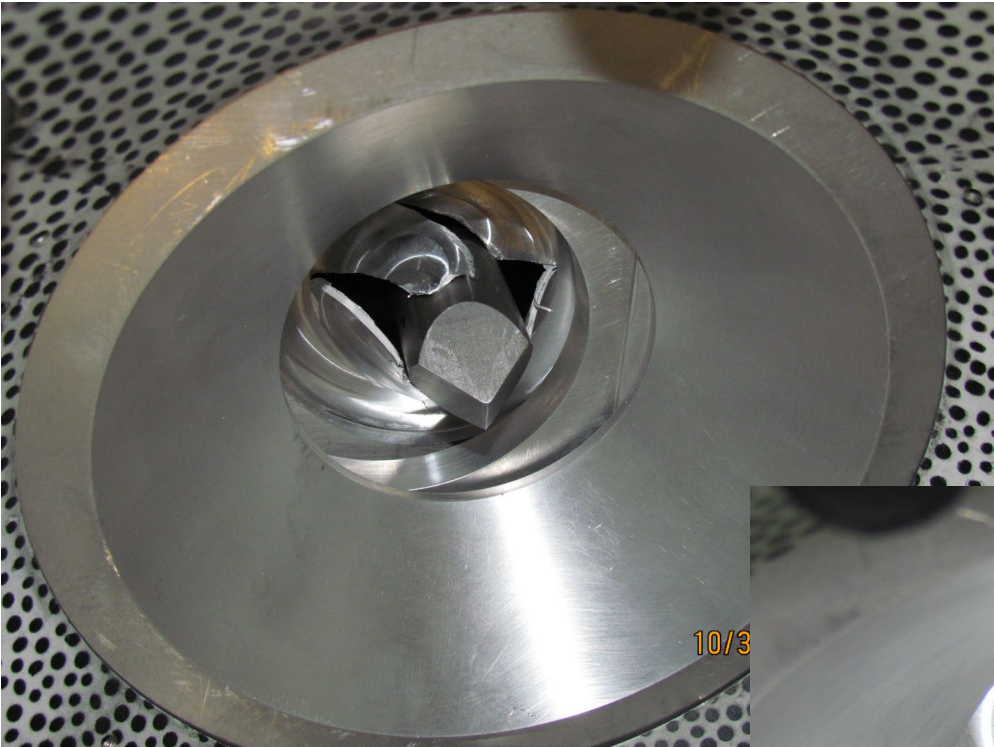
Students:

J. Albelo-Cortes (UTD), L. Alqawasmi (UNM),
J. Jacobowitz (CU)

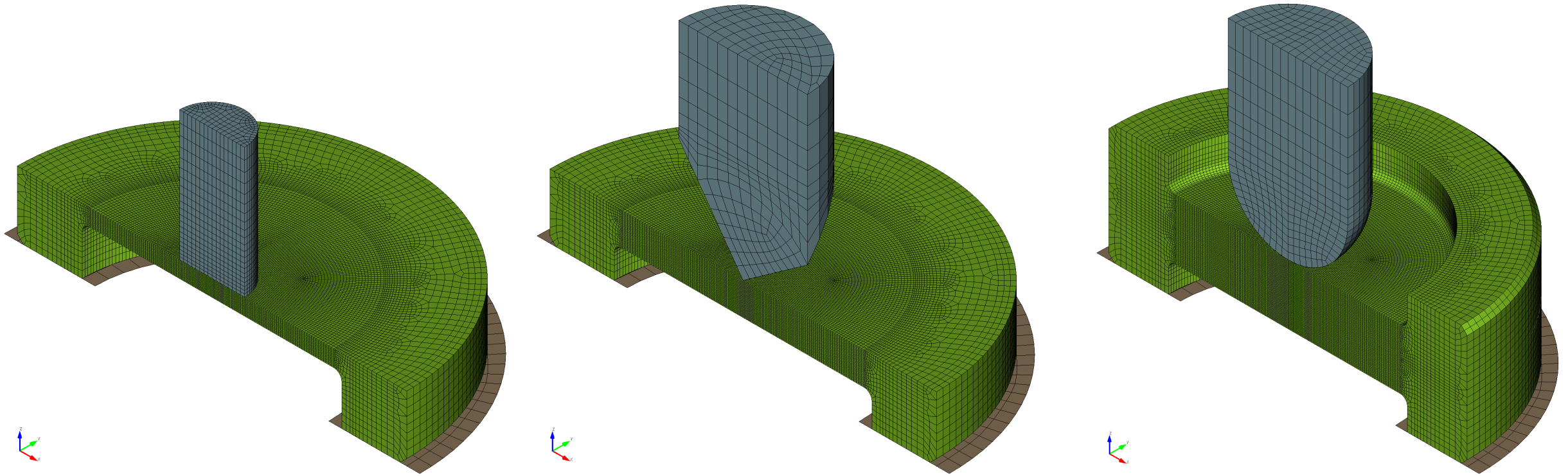
Mentors:

N. Hubbard, Dr. R. Kuether, Dr. T. Khraishi (UNM)

Motivation and Background

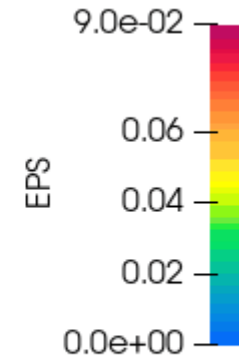


Multiple Probe Shapes and Coupon Thickness & Materials were Simulated



Flat : 0.25in Probe Through 0.125in 7075 Al

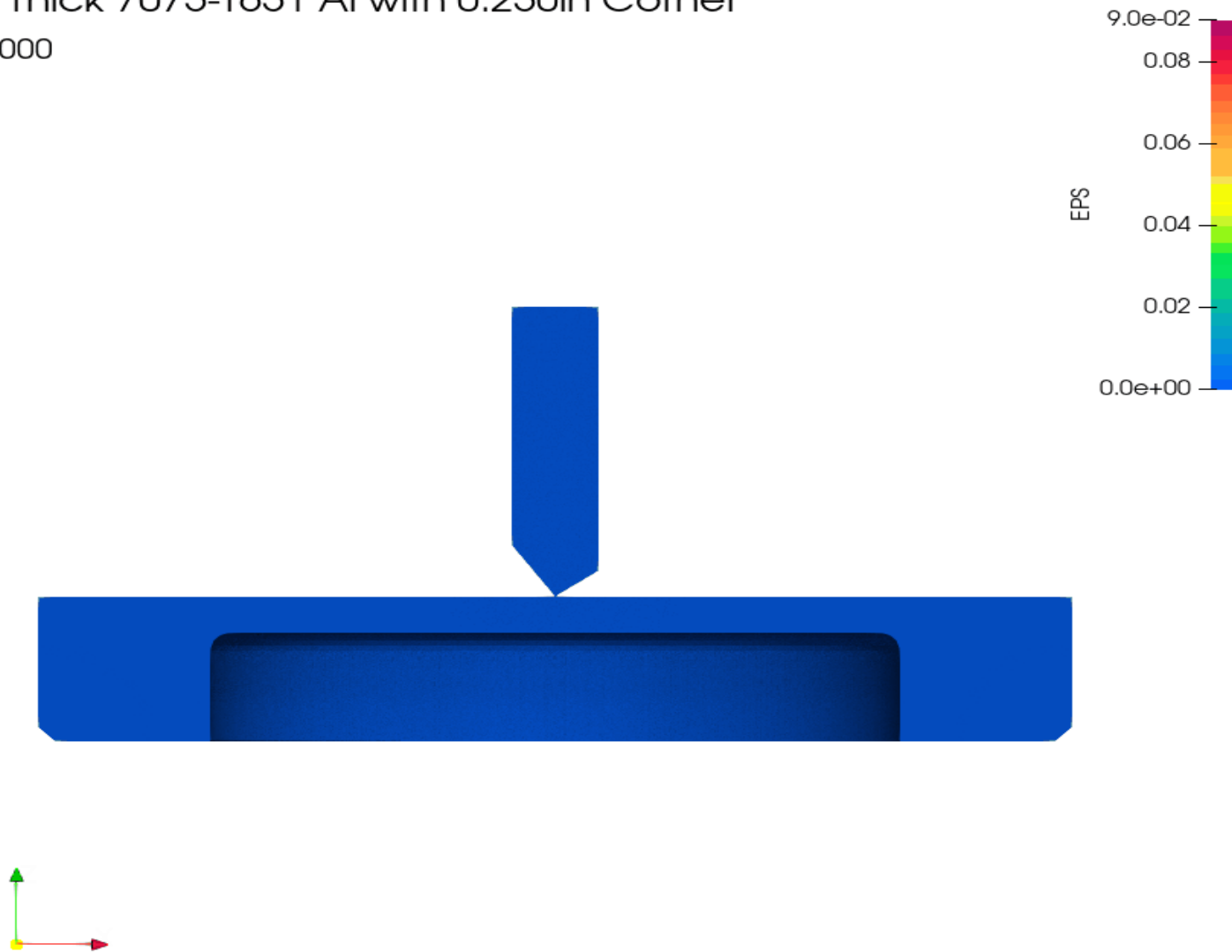
0.125in Thick 7075-T651 Al with 0.250in Flat
Time: 0.0000



Corner : 0.25in Probe Through 0.125in 7075 Al

0.125in Thick 7075-T651 Al with 0.250in Corner

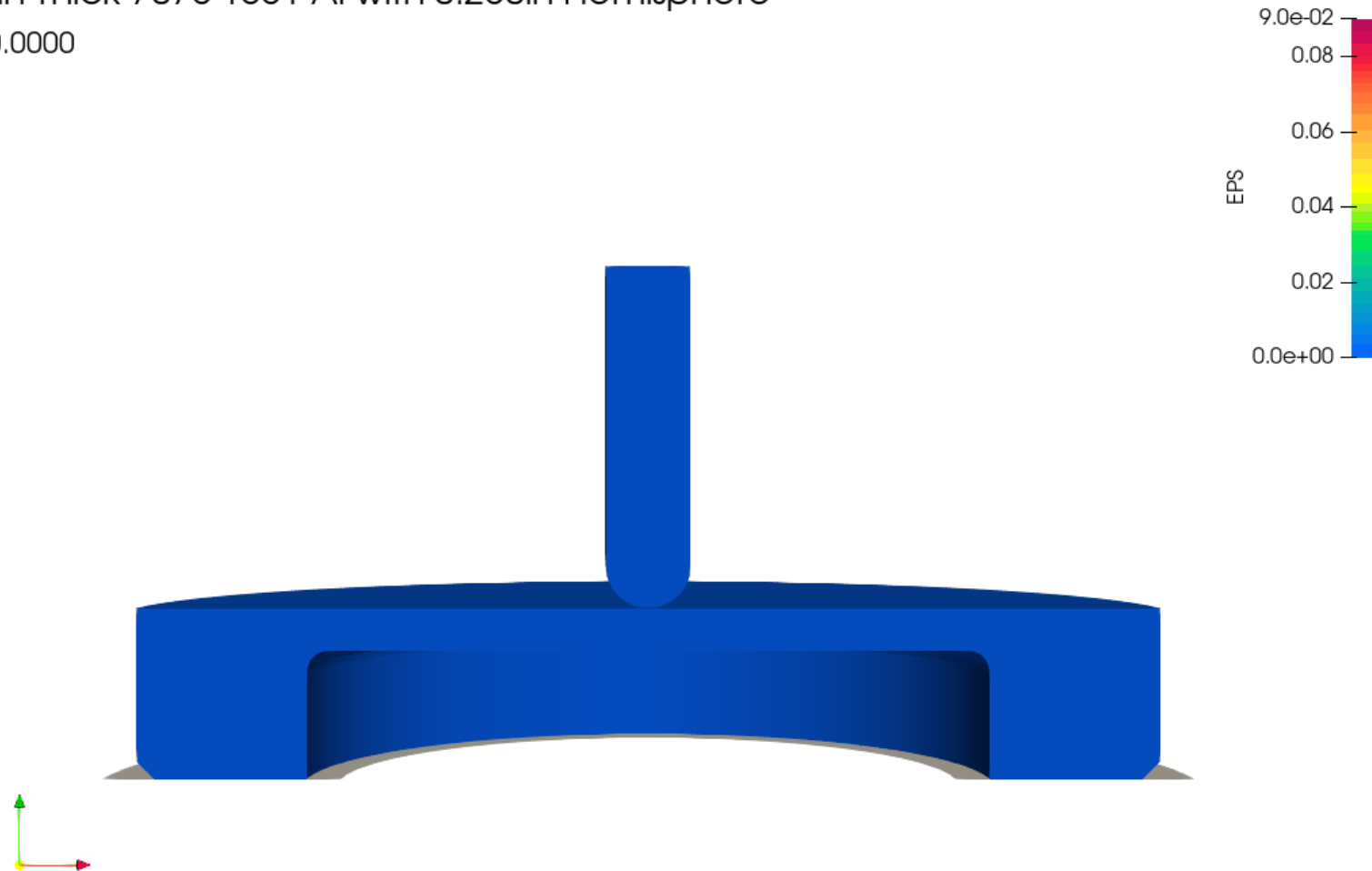
Time: 0.0000



Hemisphere : 0.25in Probe Through 0.125in 7075 Al

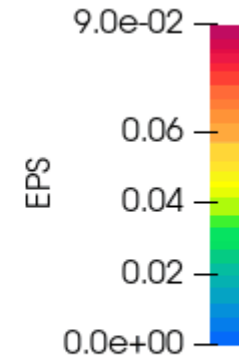
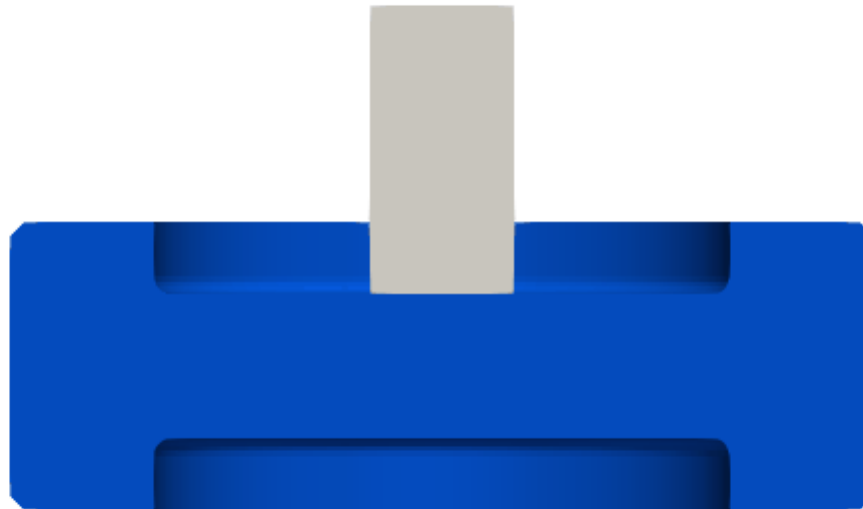
0.125in Thick 7075-T651 Al with 0.250in Hemisphere

Time: 0.0000



Flat : 0.50in Probe Through 0.50in 304L SS

0.500in Thick 304L VAR SS with 0.500in Flat
Time: 0.0000

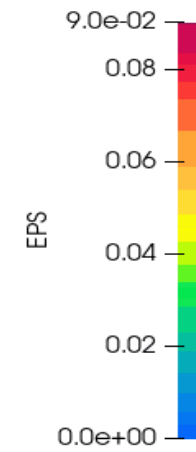


Note: The probe model was set to elastic and therefore does not show elastic plastic strain (EPS).

Corner : 0.50in Probe Through 0.50in 304L SS

0.500in Thick 304L VAR SS with 0.500in Corner

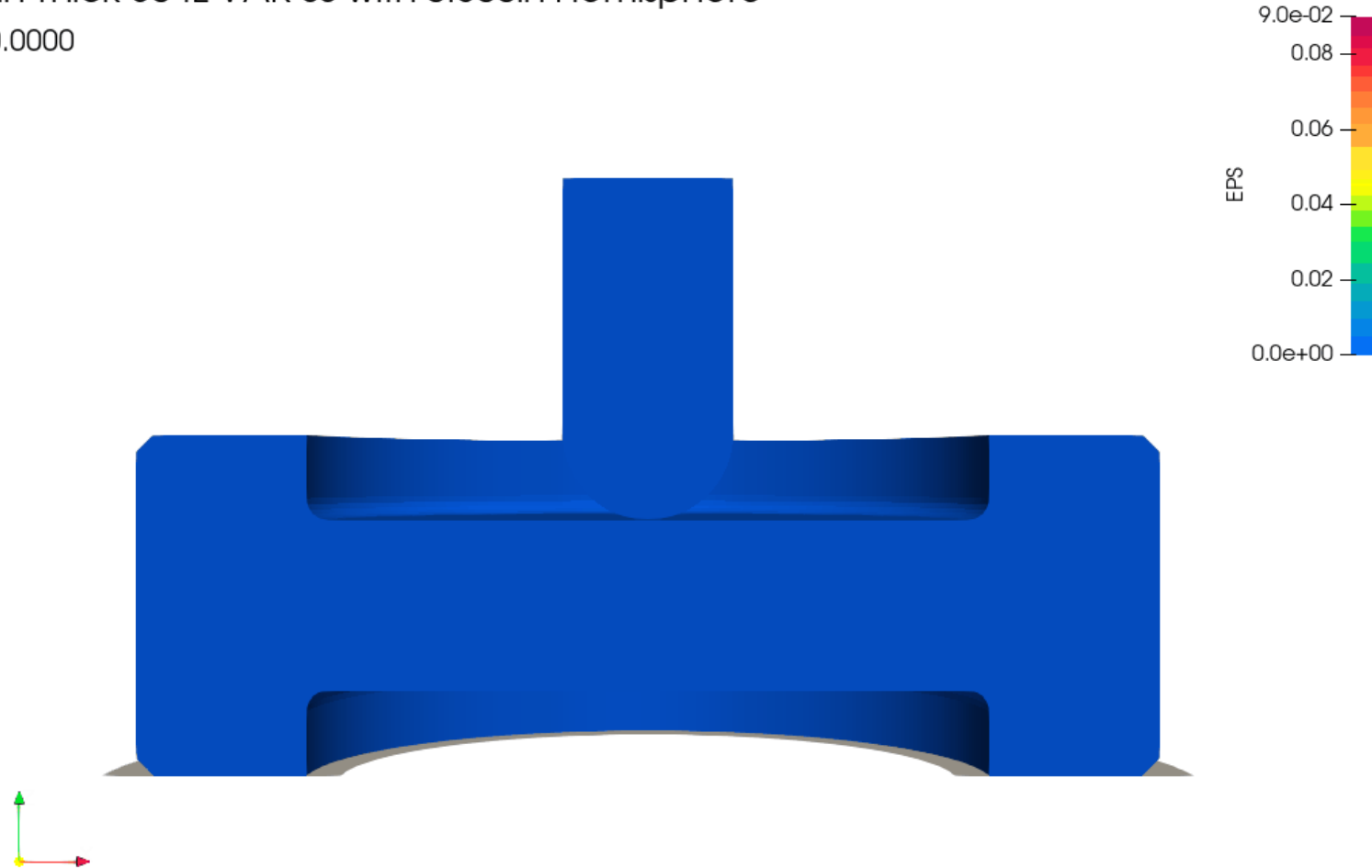
Time: 0.0000



Hemisphere : 0.50in Probe Through 0.50in 304L SS

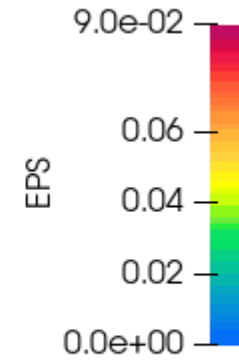
0.500in Thick 304L VAR SS with 0.500in Hemisphere

Time: 0.0000



The 6061 Material Model Can Fail Easily

0.125in Thick 6061-T651 Al with 1.000in Flat
Time: 0.0000

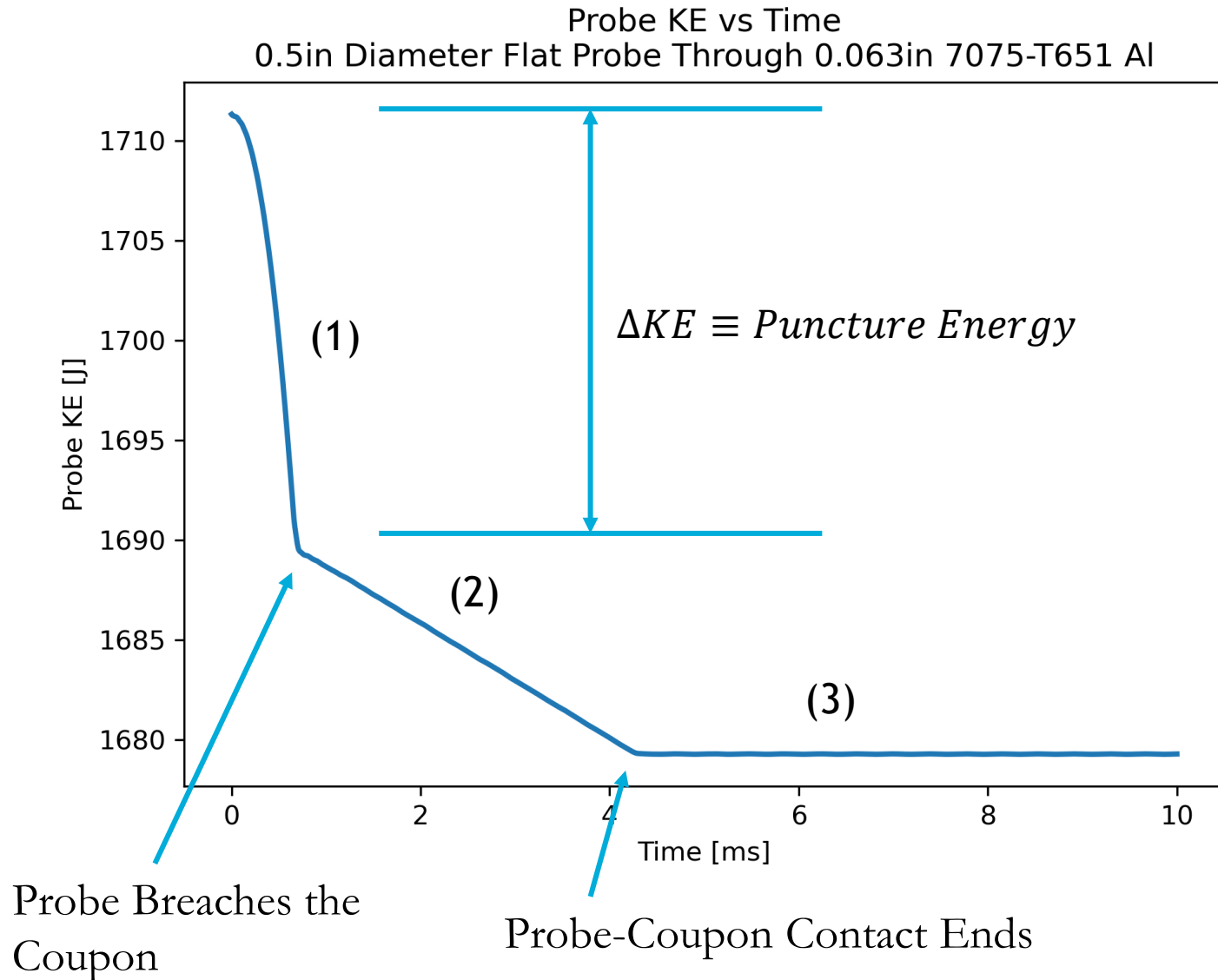


Probe Unique Aspects



- Flat : localizes stress at the circumference of the contact area
- Corner : acts like a wedge, cutting and spreading the coupon
- Hemispherical : the “smooth” probe shape induces the most plastic strain

Puncture Stages and Puncture Energy Determination



Stages of Puncture:

1. Probe contacts and deforms the coupon.
2. Probe scrapes the edge of the puncture hole.
3. Probe no longer in contact with the coupon.

Empirical Fit Equation by Corona (2020)



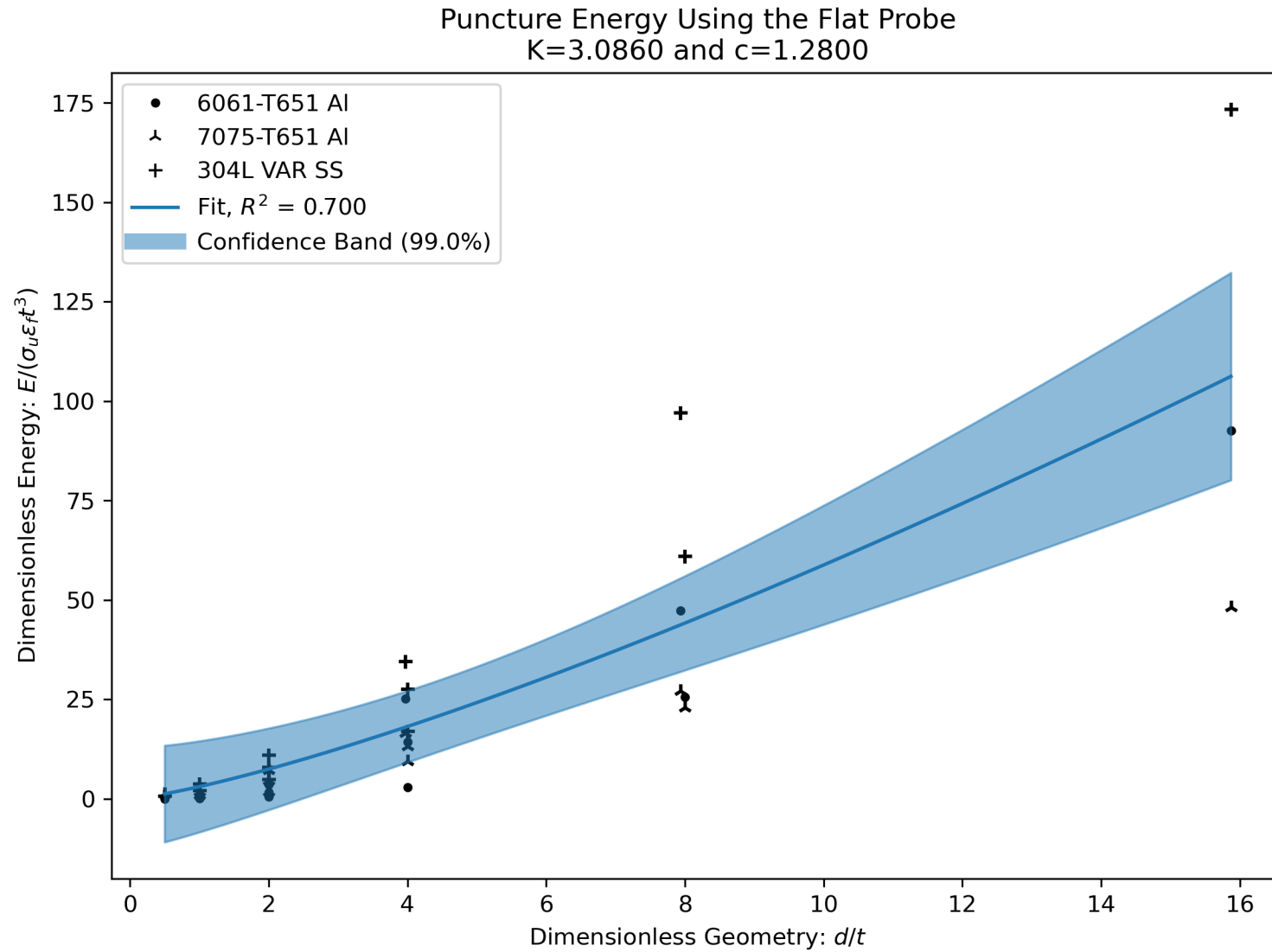
$$E = K \sigma_u \epsilon_f t^3 \left(\frac{d}{t}\right)^c$$

Puncture Energy [J] → E
 Constant 1 → K
 Ultimate Engineering Stress [Pa] → σ_u
 Ultimate Engineering Strain at Failure → ϵ_f
 Coupon Thickness [m] → t
 Probe Diameter [m] → d
 Constant 2 → c

$$\rightarrow \frac{E}{\sigma_u \epsilon_f t^3} = K \left(\frac{d}{t}\right)^c$$

dimensionless energy = dimensionless geometry

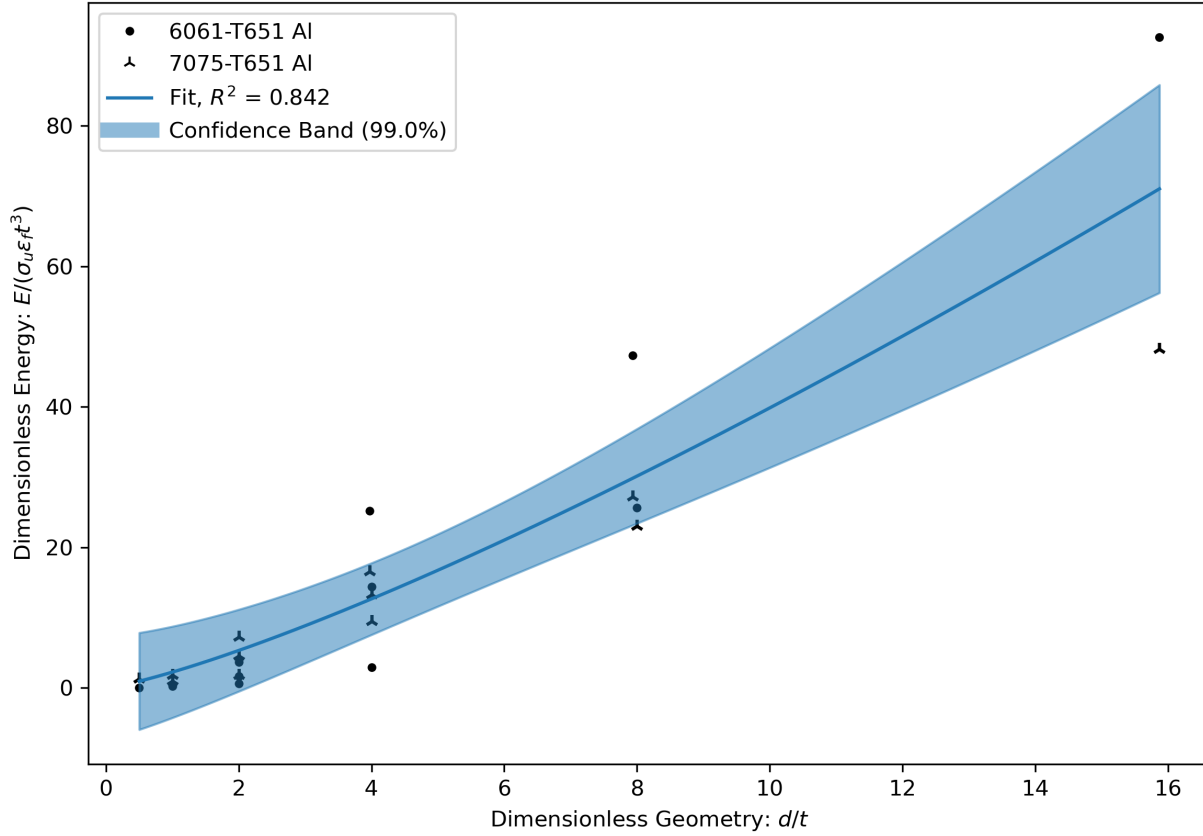
Flat Probe Fit Using All Materials



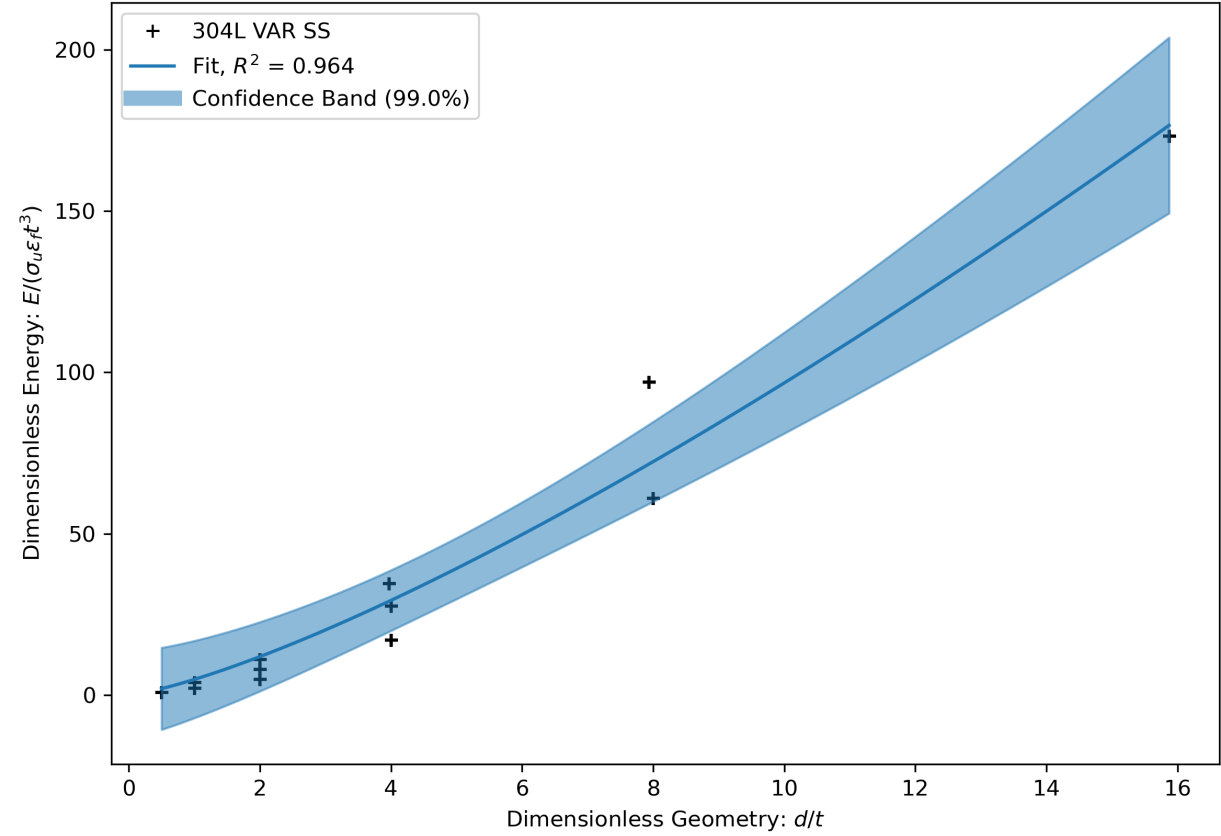
Flat Probe Fit Separating Materials



Puncture Energy Using the Flat Probe
K=2.2321 and c=1.2516



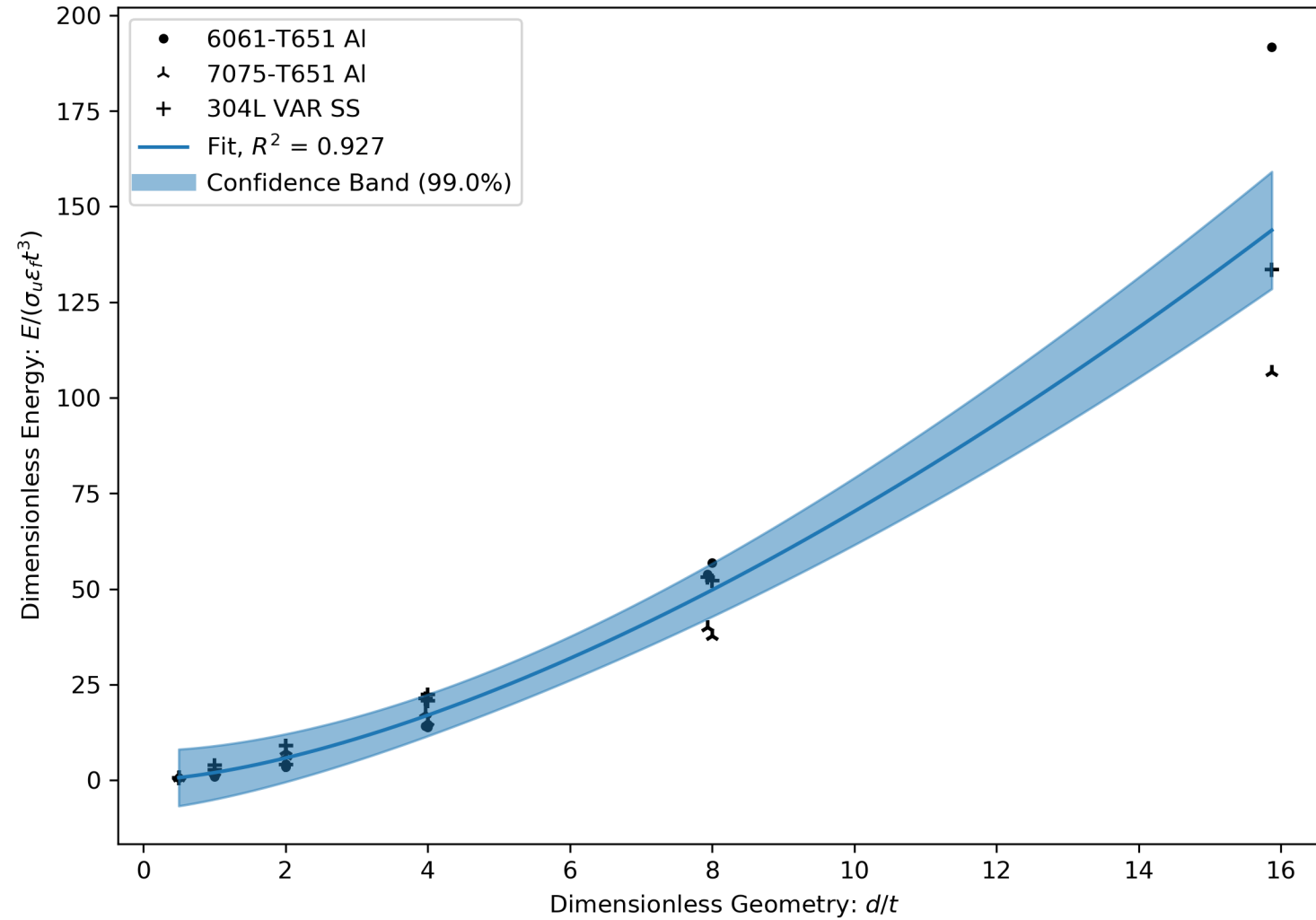
Puncture Energy Using the Flat Probe
K=4.8134 and c=1.3031



Corner Probe Fit Using All Materials



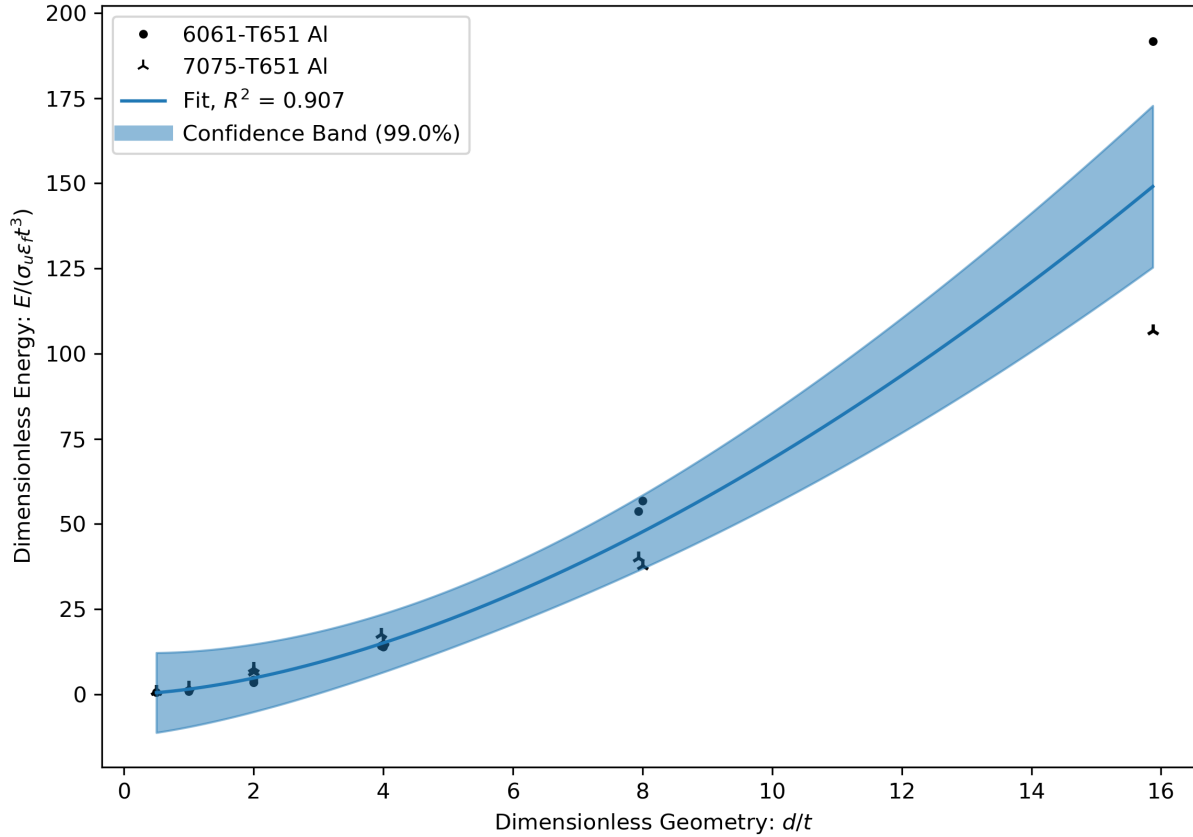
Puncture Energy Using the Corner Probe
 $K=1.9811$ and $c=1.5498$



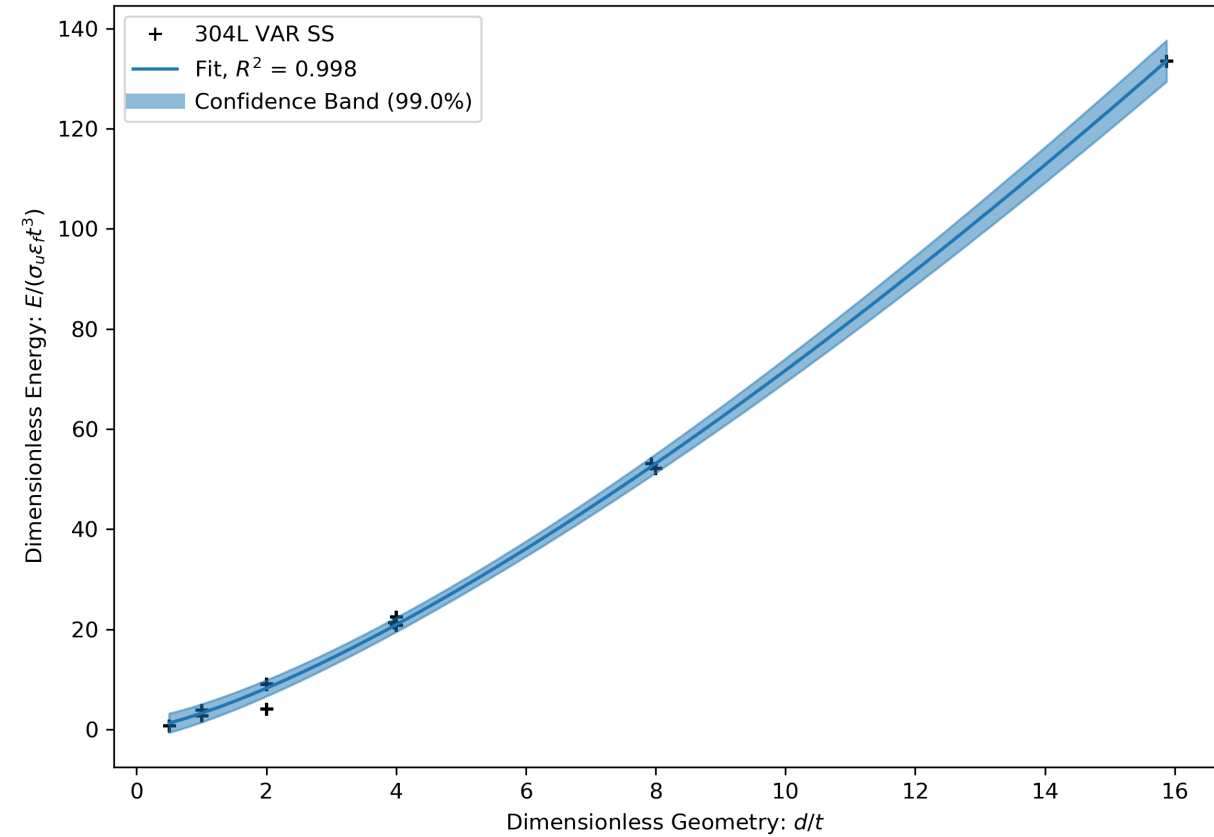
Corner Probe Fit Separating Materials



Puncture Energy Using the Corner Probe
 $K=1.5009$ and $c=1.6633$



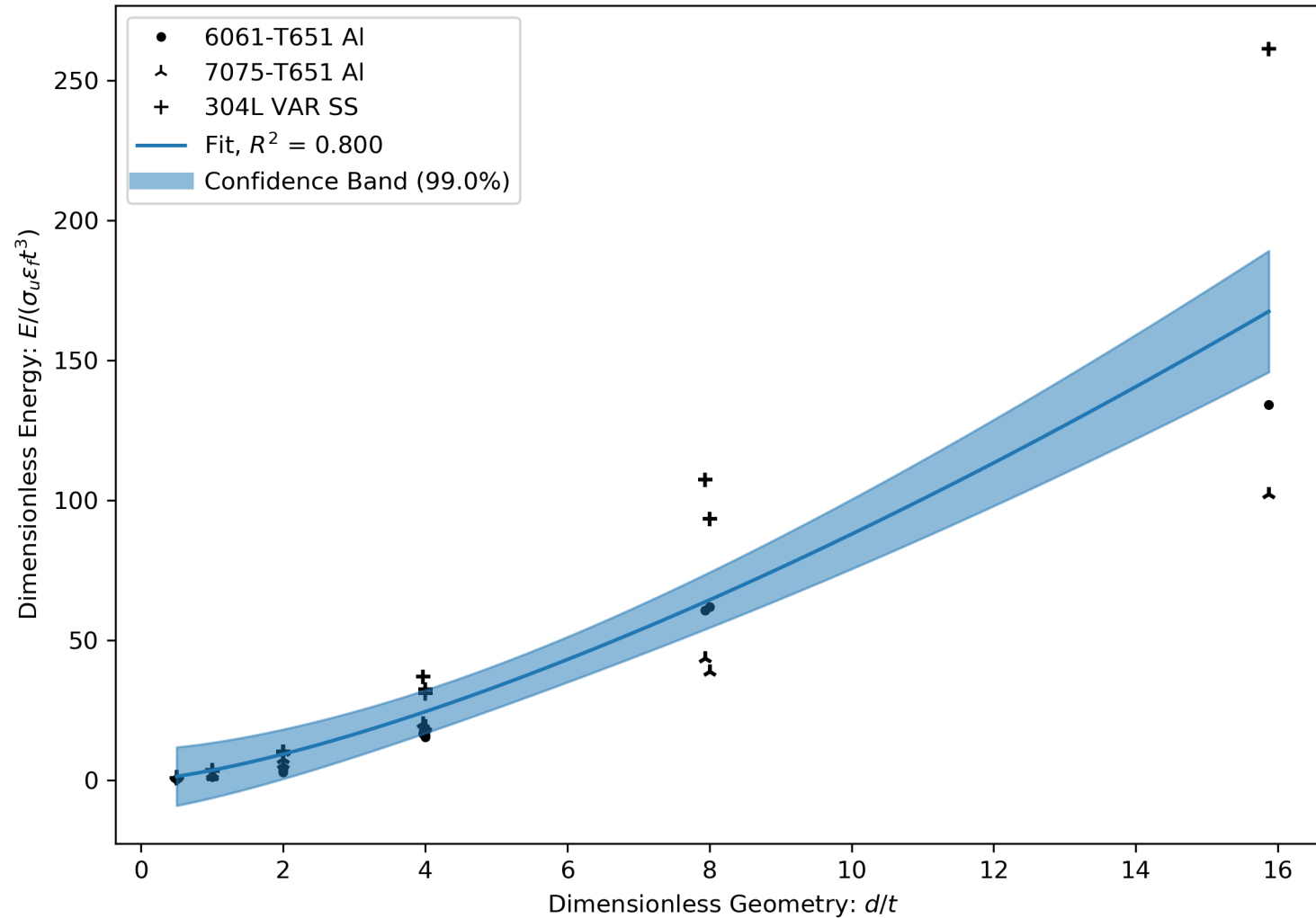
Puncture Energy Using the Corner Probe
 $K=3.2386$ and $c=1.3452$



Hemisphere Probe Fit Using All Materials



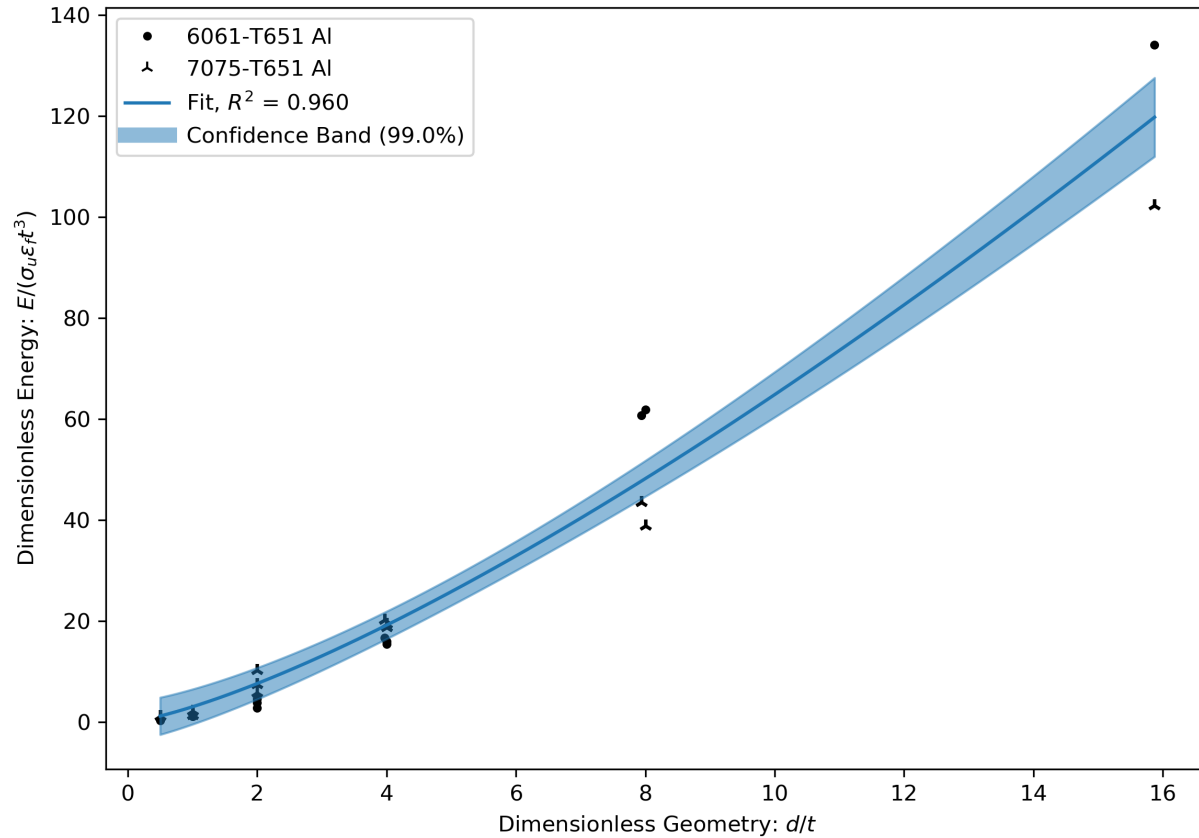
Puncture Energy Using the Hemisphere Probe
 $K=3.5375$ and $c=1.3953$



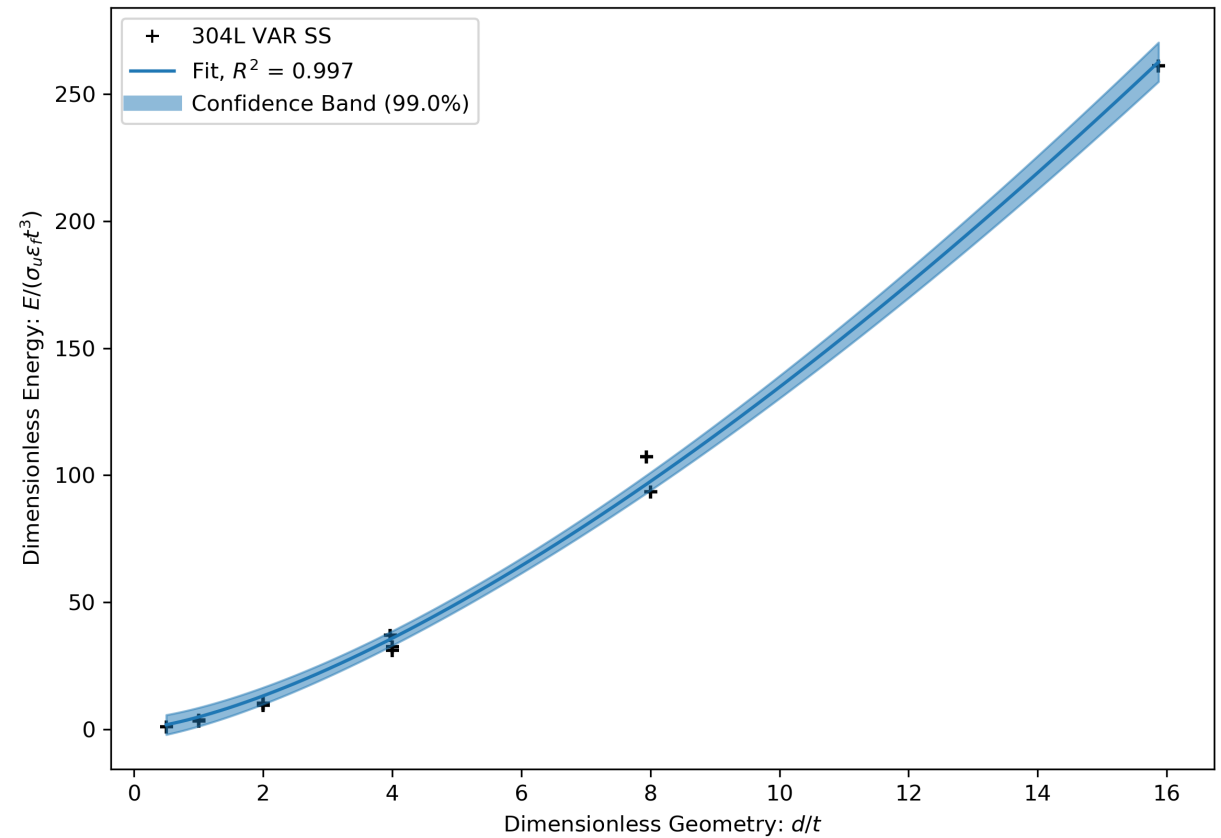
Hemisphere Probe Fit Separating Materials



Puncture Energy Using the Hemisphere Probe
K=3.0464 and c=1.3281



Puncture Energy Using the Hemisphere Probe
K=4.8230 and c=1.4460





R² Fit Summary

	Flat	Corner	Hemispherical
All data	0.700	0.927	0.800
Aluminum	0.842	0.907	0.960
Steel	0.964	0.998	0.997

The flat probe results were very scattered.

- Consequence: **lower quality fit** than the corner and hemisphere probes

Fits should be **separated by both material and probe shape**.



K and c Fit Summary

	Flat	Corner	Hemispherical
All data	K = 3.086 c = 1.280	K = 1.981 c = 1.550	K = 3.538 c = 1.395
Aluminum	K = 2.232 c = 1.252	K = 1.501 c = 1.663	K = 3.046 c = 1.328
Steel	K = 4.813 c = 1.303	K = 3.239 c = 1.345	K = 4.823 c = 1.446

Observed trend: Higher K for steel than aluminum



- **Simulate more alloys and dimensions** to ensure the fit stays statistically significant.
- Investigate the effects of **probe velocity**.
- Add **strain rate dependency** for all materials.
- **Increase the coupon puncture-area diameter** for thinner coupons.

Acknowledgements



Thank you to Neal Hubbard for teaching and guiding us through this project and answering all of our (many) questions. Thank you to Dr. Rob Kuether, Brooke Allensworth, Dr. Debby Fowler for organizing and running this summer research opportunity. Thank you to Dr. Tariq Kharishi (UNM) asking thoughtful questions to make us consider things more deeply. Thank you to Dr. Joe Bishop for checking in with us weekly and making sure we did not have any issues.

This research was conducted at the 2021 Nonlinear Mechanics and Dynamics Research Institute hosted by Sandia National Laboratories and the University of New Mexico.

Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.

Appendix: Confidence Band Calculation



$\alpha \equiv$ significance

$t \equiv$ student t distribution

$y_{fit} \equiv$ y as determined by regression

$n \equiv$ number of independent variables

$df \equiv$ degrees of freedom

$$s_x = (x - \bar{x})^2$$

$$SS_x = \sum_i (x - \bar{x})^2$$

$$SE = \sqrt{\frac{1}{df} \sum_i (y - y_{fit})^2}$$

$$\text{confidence interval} = t \cdot SE \cdot \sqrt{\frac{1}{n} + \frac{s_x}{SS_x}}$$

$$y_{conf} = y \pm \text{confidence interval}$$