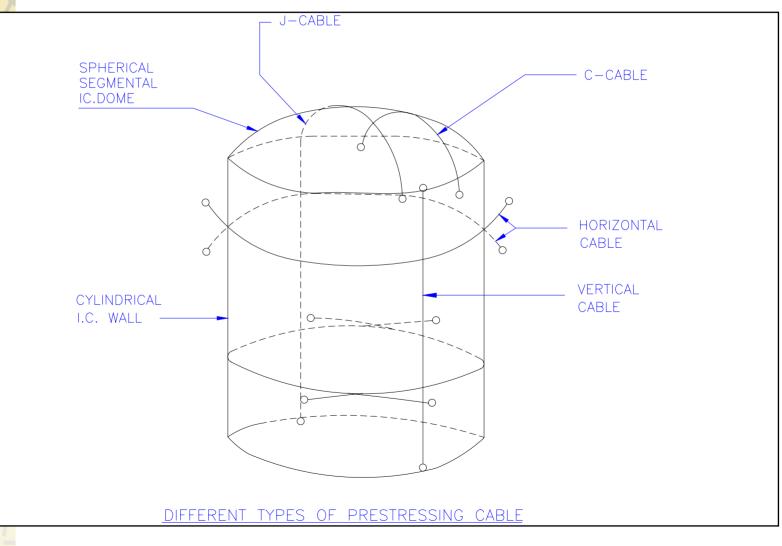
Estimation of Prestress Losses

U. S. P. Verma, Executive Director (Civil & Engg. Services) Raghupati Roy, Additional Chief Engineer (Civil) Indrajit Ray, Deputy Chief Engineer (Civil)

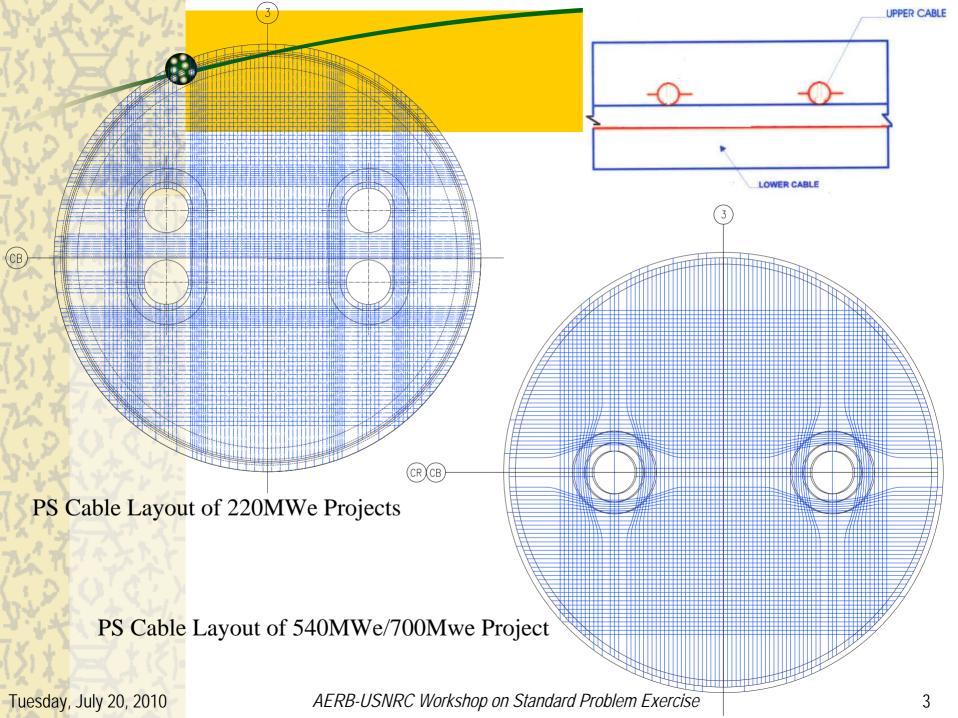
Nuclear Power Corporation of India Limited, Mumbai



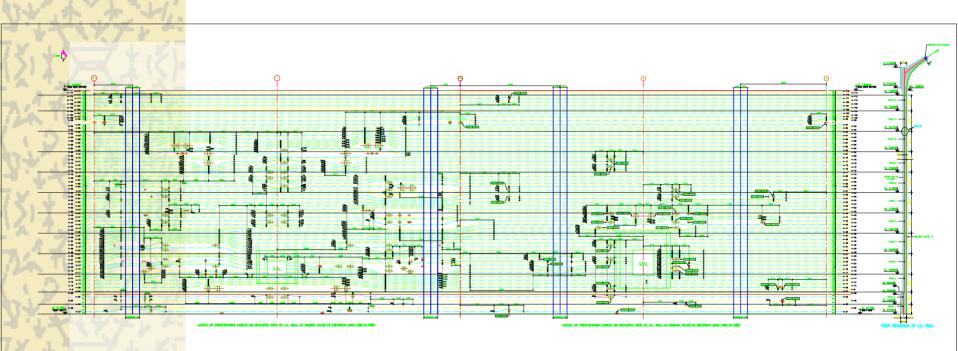
Types of Prestressing Cables Used in Indian Containments



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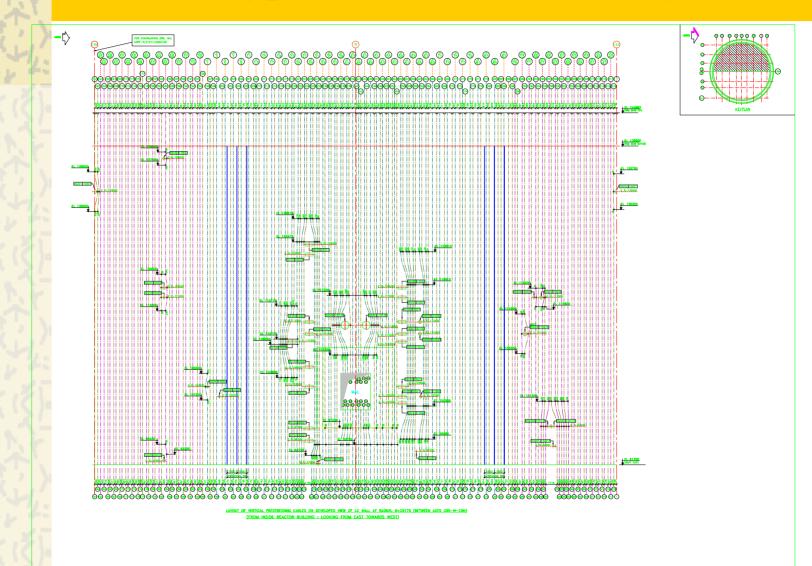


Typical Horizontal Cable Layout



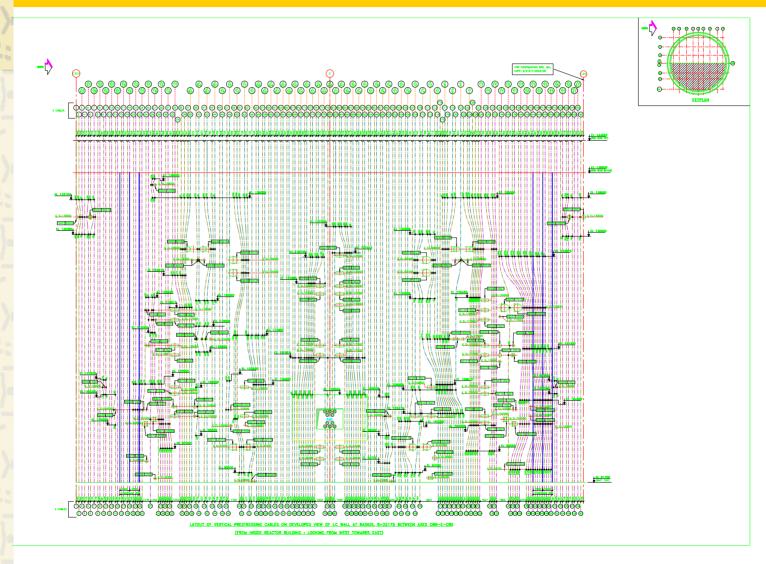
Tuesday, July 20, 2010

Typical Vertical Cable Layout



Tuesday, July 20, 2010

Typical Vertical Cable Layout



Tuesday, July 20, 2010

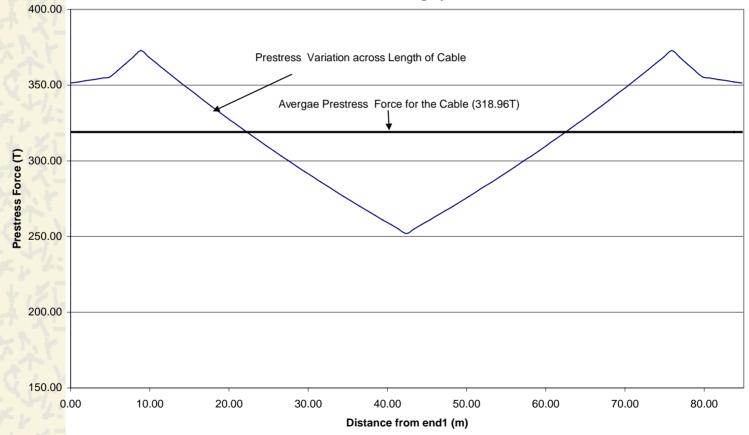
Short Term Losses

Initial (Short Term) Losses due to

- Wobble & Friction Loss
 - During Stressing
- Anchorage-draw-in (Slip Loss)
 - Due to Locking of Cables at Anchorage End
- Elastic Shortening
 - Due to stage wise Prestressing of Cables

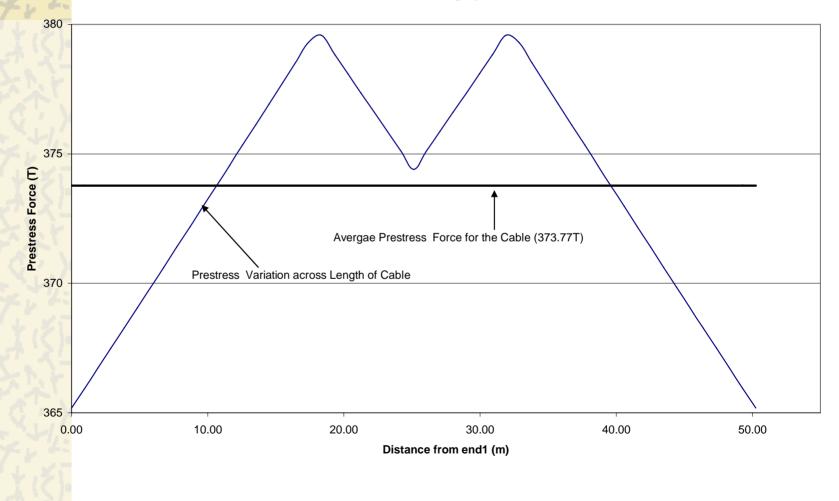
Typical Variation of Prestress After Initial Losses

Variation of Prestress Force after Initial Losses in Horizontal Cable in IC Wall 27K13 Prestressing System



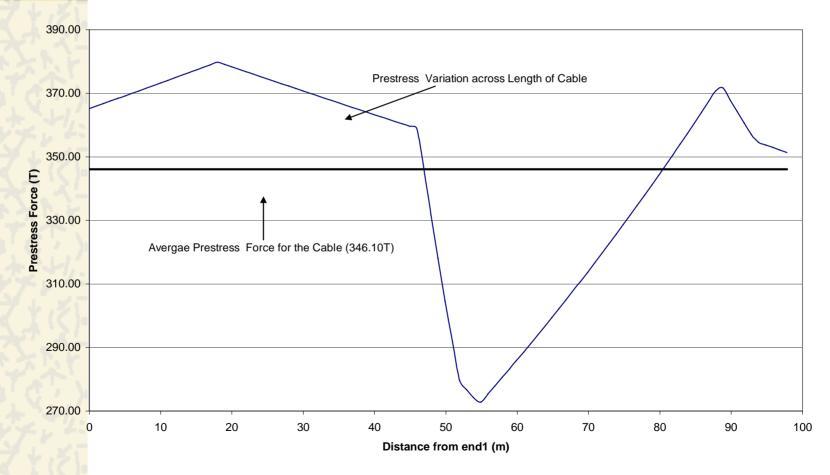
Typical Variation of Prestress After Initial Losses

Variation of Prestress Force after Initial Losses in Pure Vertical Cables in IC Wall 27K13 Prestressing System



Typical Variation of Prestress After Initial Losses

Variation of Prestress Force after Initial Losses for JO40 (type=1) 27K13 Prstressing System



Long Term Prestress Losses as per Different International Standards

Long Term Losses are Calculated with respect to Average Prestress Available in Cables after Initial Losses

Data Used for Calculation

Grade of Concrete (cube strength)	45 MPa			
Age of structure when long term losses are compared	40 years			
	i.e., 14600days			
Age of structure when drying started	7days			
Age of structure at load transfer	67days			
(Considering 7 days curing & 2 months of prestressing)				
Relative humidity	60%			
Volume to surface ratio = Effective thickness of structure	650mm			
Slump of concrete	120mm			
% of fine aggregate to total aggregate	40%			
Air content of concrete	2%			
% Reinforcement considered	1.3%			
with 2-25 ϕ at top & bot. of the cable & 1-25 ϕ @ top & bot. in betn. Cables, cable spacing = 500mm & considering 50% prestress steel participation				

Data Used for Calculation

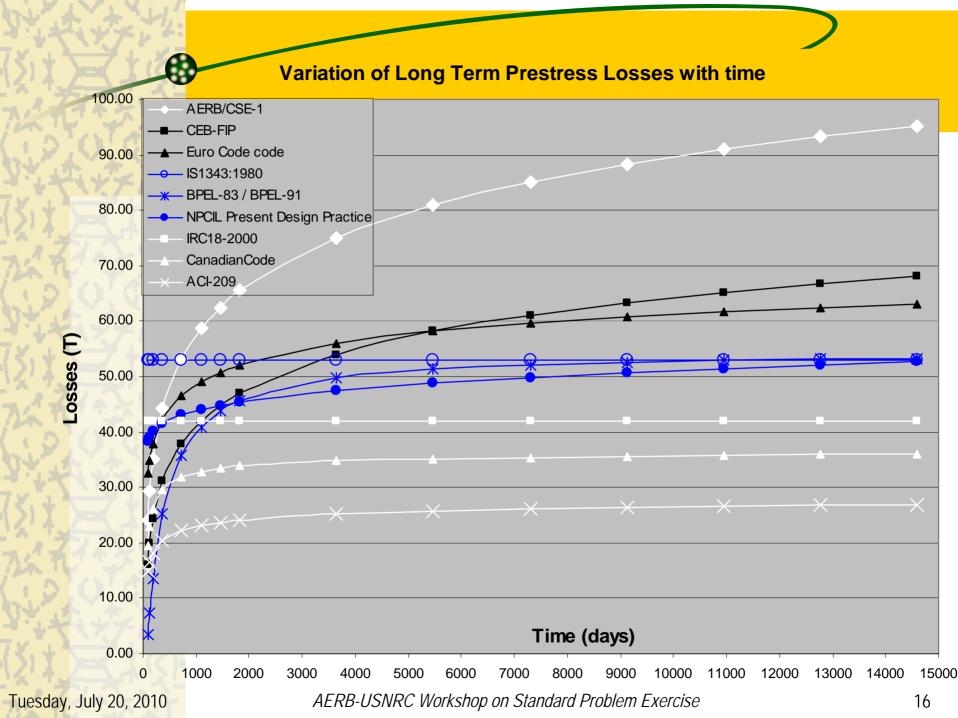
Modulus of Elasticity of Prestressing steel	1.95E+05MPa			
Modulus of Elasticity of Concrete	As per codal requirement 12 MPa			
Stress in concrete section due to prestress				
Stress in concrete section due to dead load	1 MPa			
Prestressing system	27K13 with low relaxation steel			
C/s area of prestressing steel	2664.90 mm ²			
Guaranteed ultimate tensile strength of the system	500 T			
Prestress force after initial losses	340 T			
1000 hour relaxation (ρ1000)	2.5 %			

Long Term Losses (Shrinkage + Creep + Relaxation)

- AERB Containment Code (AERB/SS/CSE-1)
 CEB-FIP Model Code 1990
- 🕁 Euro Code ENV 1992-1-1 EC 2
- ≽ IS: 1343-1980
- ≽ BPEL-91
- Present design practice of NPCIL
- ≽ IRC: 18-2000
- Canadian Code CAN3-A23.3-M84
- American code (ACI 209R)

Total Long-term Losses

N I	Code	Long Term Prestress Losses (T)				
ł	Code	Shrinkage	Cree	p Re	laxation	Total
	AERB/SS/CSE-1	15.79	27.79	9	51.71	95.29
	CEB-FIP MODEL CODE	15.79	26.46	6	25.85	68.10
X	Eurocode	Computation thru' common expression				63.06
	<mark>IS 134</mark> 3 : 1980	5.65	28.67	7	18.65	52.98
Ŷ	BPEL-83 / BPEL-91	8.81	34.08	3	10.42 ►	51.57
	Practice Followed by NPCIL	5.65	28.67	7	18.33	52.66
	IRC 18 2000	8.57	24.94	4	8.50	42.01
	CAN3-A23.3-M84	Computation thru' common expression ►				36.07
*	ACI 209R - 92	0.60		16.85	9.42	26.87



CONCLUSION OF THE STUDY

The predictions by NPCIL present practice, IS:1343-1980, IRC:18-2000 and BPEL match very closely

CEB-FIP and EURO code predict long-term losses very closely

Long term pre-stress losses show signs of stabilisation in around 20 years

Thank You