



Standard Problem Exercise No. 3

Phase 2 Results

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Model 4 Case 1 Presentation



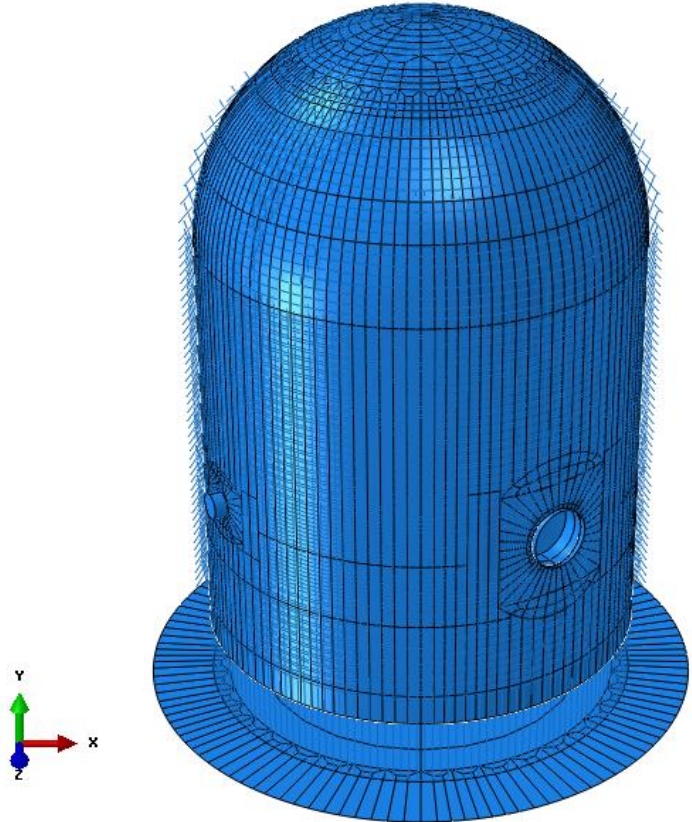


Model Geometry and Initial Conditions

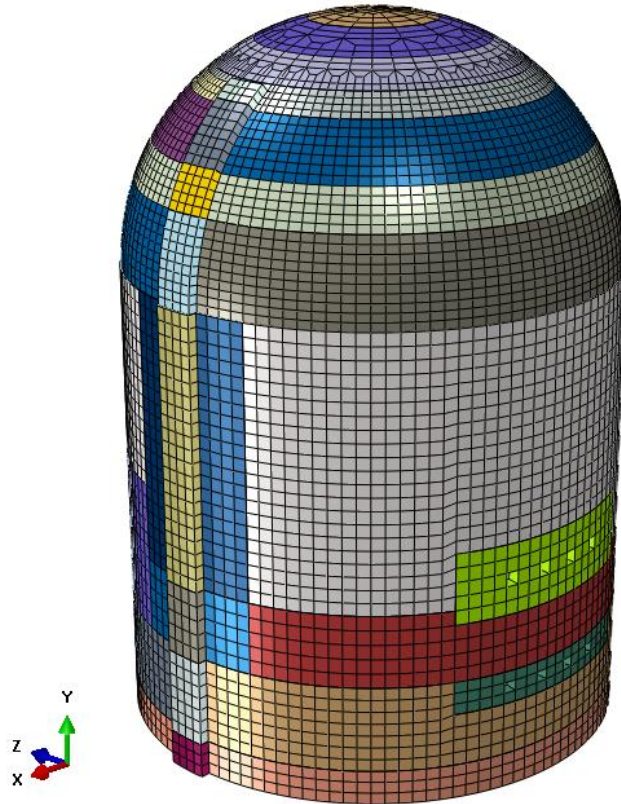
- **Model 3 includes concrete, all tendons, rebar, and liner. Shear reinforcement not included, since structure wall represented by shell elements.**
 - Concrete modeled with 4-node shell elements
 - Rebar with embedded subelements
 - tendons with two-node beam elements
 - liner with 4-node shell elements, overlain onto same nodes as concrete shell nodes, but offset by appropriate eccentricity
- **Representation of losses by FE Model's simulation of friction**
- **Every tendon was modeled, and each tendon had a "jacking element" protruding from the tendon end zone**



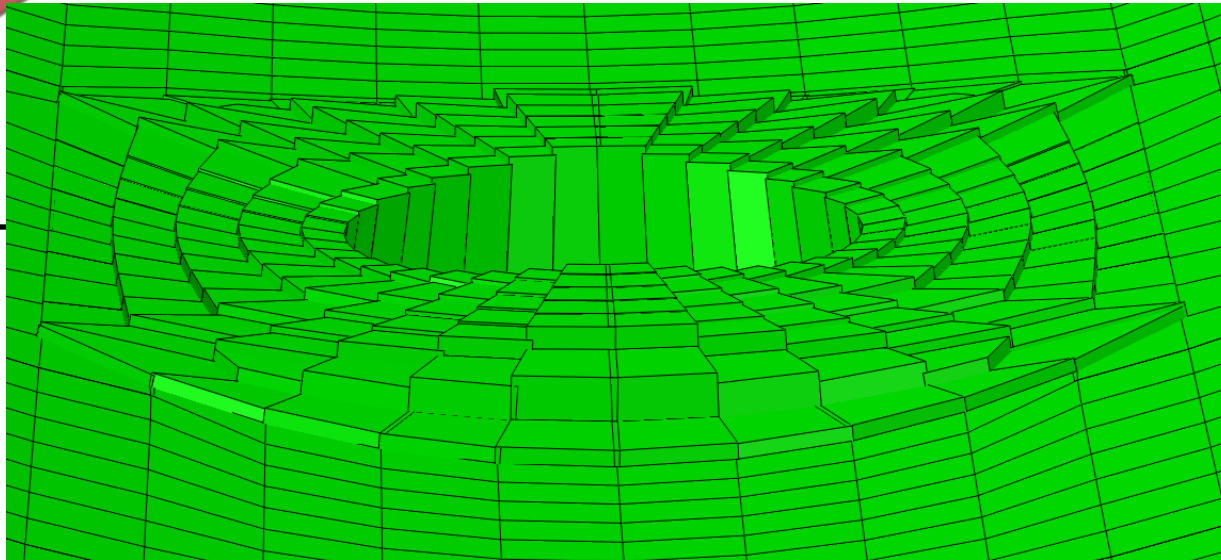
Model 4 Overview



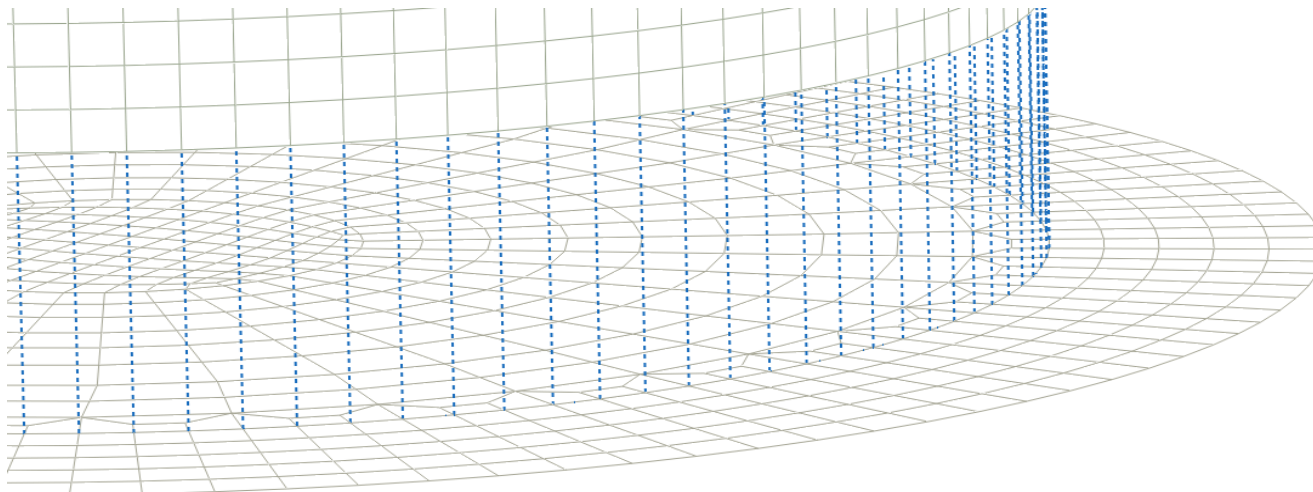
Meshed Concrete Vessel with Various Section Assignments



View of M/S and F/W



EH Thickness Assigned to Center of Each Element. Air-Lock Similar

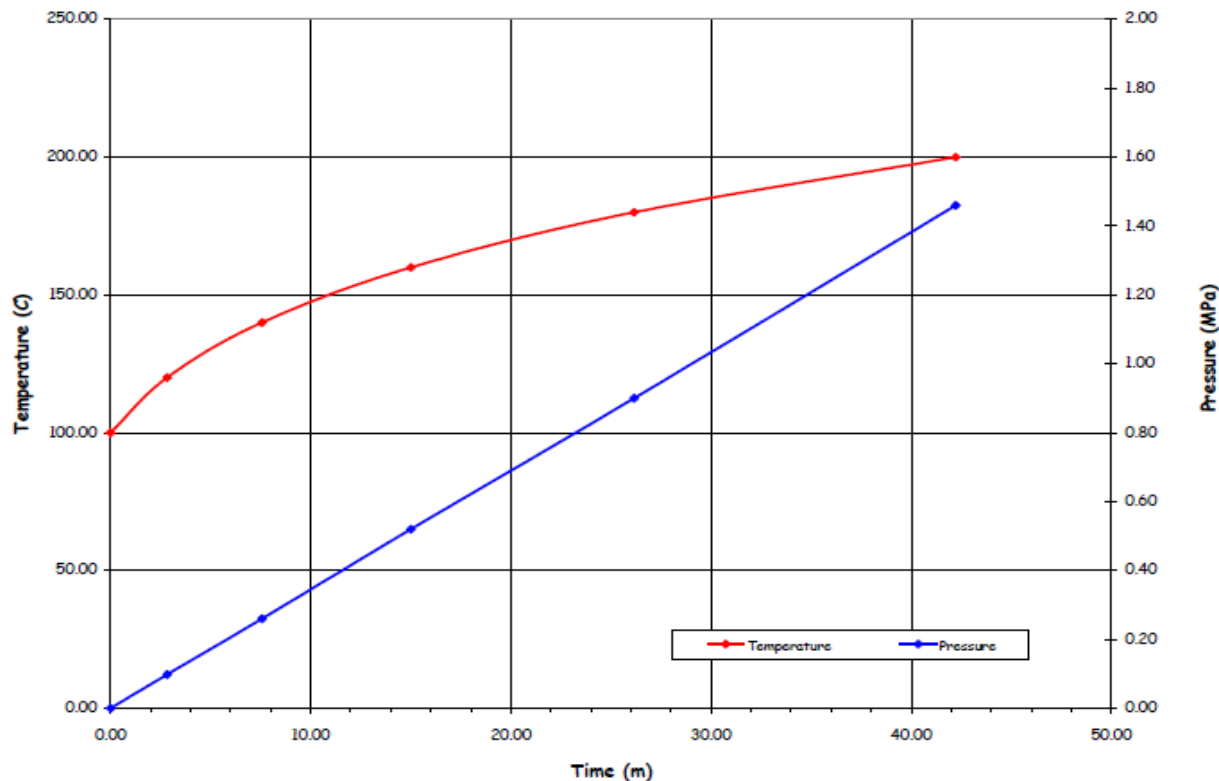


Rigid Links from Bottom of Vessel to Basemat Elements

Model 4 Problem Definition

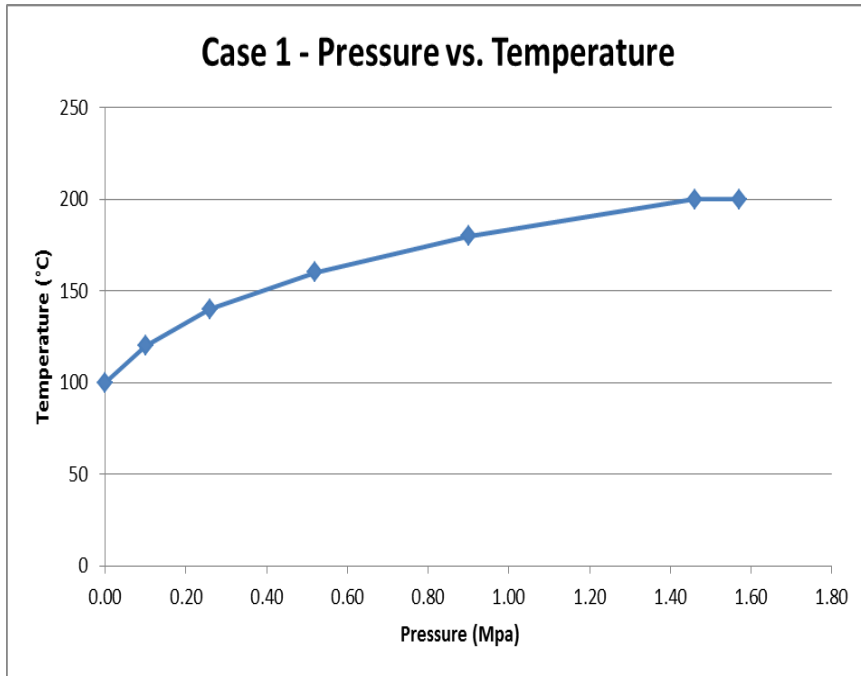
Case 1 – Saturated Steam

- Considers monotonically increasing pressure and temperature based on pseudo-time history of 1:4 Scale PCCV Model SFMT pressurization rate (5 psi/min)

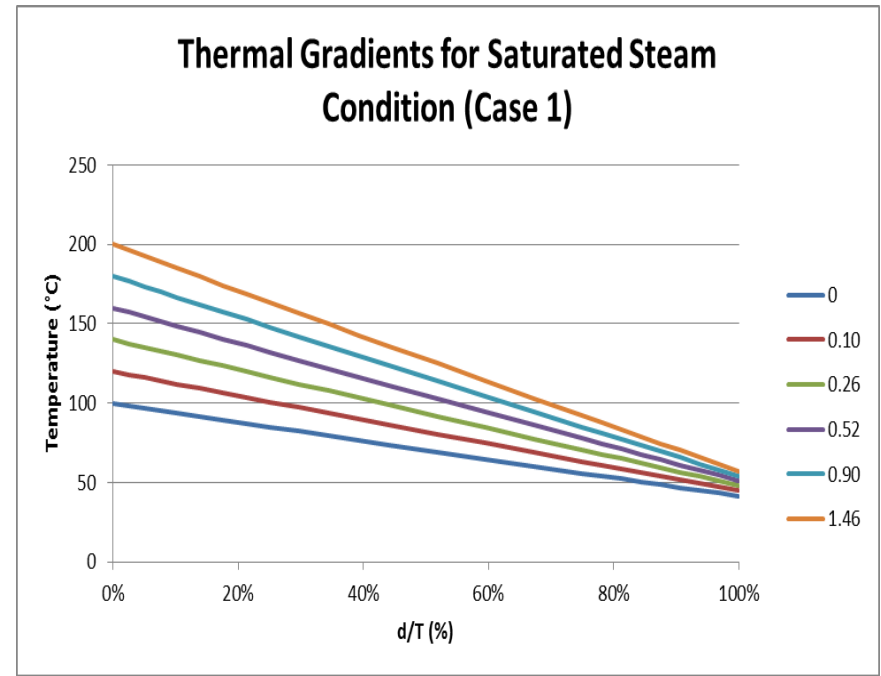


Predefined Temperature Case 1

Temperature solution varies linearly through thickness of PCCV wall



Temperature at inside face of vessel at corresponding pressure



Temperature variation through thickness at pressure milestones



Material Modeling

- **Concrete was simulated using ABAQUS concrete “Damaged Plasticity” constitutive model that utilizes a smeared-cracking formulation in tension and a compressive plasticity theory**
- **Steel elements were simulated using ABAQUS “Standard Plasticity”**
- **Stress-strain curves consist of effective stress (Mises) and effective strain**





Implementing Temperature Dependent Property Degradation

- **concrete and steel material strengths degrade with temp**
- **In the last 10 years, the effect of temperature on strength is better known (especially for concrete)**
- **Material stress-strain curves defined and implemented for fully-coupled temperature degradation - adopted based on the 2005 Euro-code**



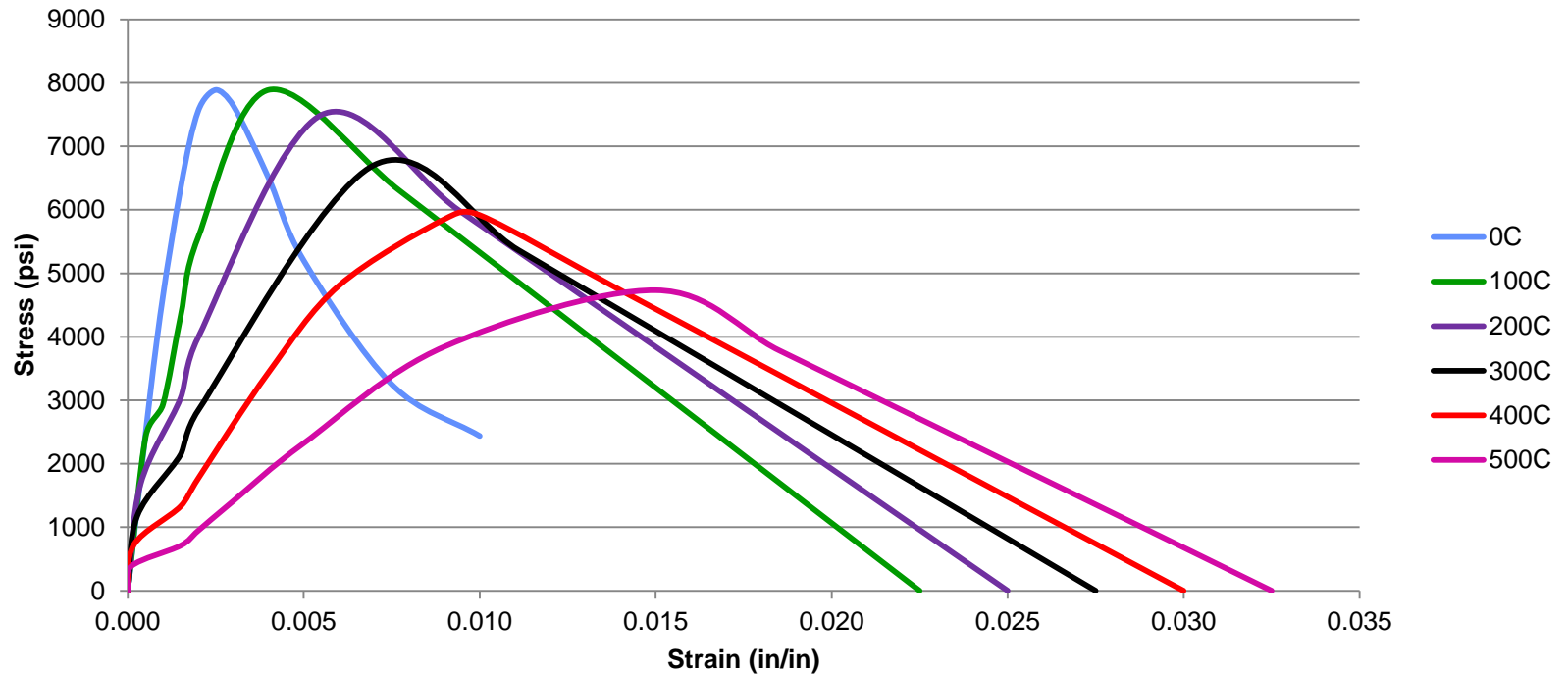
Concrete Degradation Properties at Elevated Temperatures per Eurocode

Concrete temp. θ [°C]	Siliceous aggregates			Calcareous aggregates		
	$f_{c,\theta} / f_{ck}$ [-]	$\epsilon_{c1,\theta}$ [-]	$\epsilon_{cu1,\theta}$ [-]	$f_{c,\theta} / f_{ck}$ [-]	$\epsilon_{c1,\theta}$ [-]	$\epsilon_{cu1,\theta}$ [-]
1	2	3	4	5	6	7
20	1,00	0,0025	0,0200	1,00	0,0025	0,0200
100	1,00	0,0040	0,0225	1,00	0,0040	0,0225
200	0,95	0,0055	0,0250	0,97	0,0055	0,0250
300	0,85	0,0070	0,0275	0,91	0,0070	0,0275
400	0,75	0,0100	0,0300	0,85	0,0100	0,0300
500	0,60	0,0150	0,0325	0,74	0,0150	0,0325
600	0,45	0,0250	0,0350	0,60	0,0250	0,0350
700	0,30	0,0250	0,0375	0,43	0,0250	0,0375
800	0,15	0,0250	0,0400	0,27	0,0250	0,0400
900	0,08	0,0250	0,0425	0,15	0,0250	0,0425
1000	0,04	0,0250	0,0450	0,06	0,0250	0,0450
1100	0,01	0,0250	0,0475	0,02	0,0250	0,0475
1200	0,00	-	-	0,00	-	-



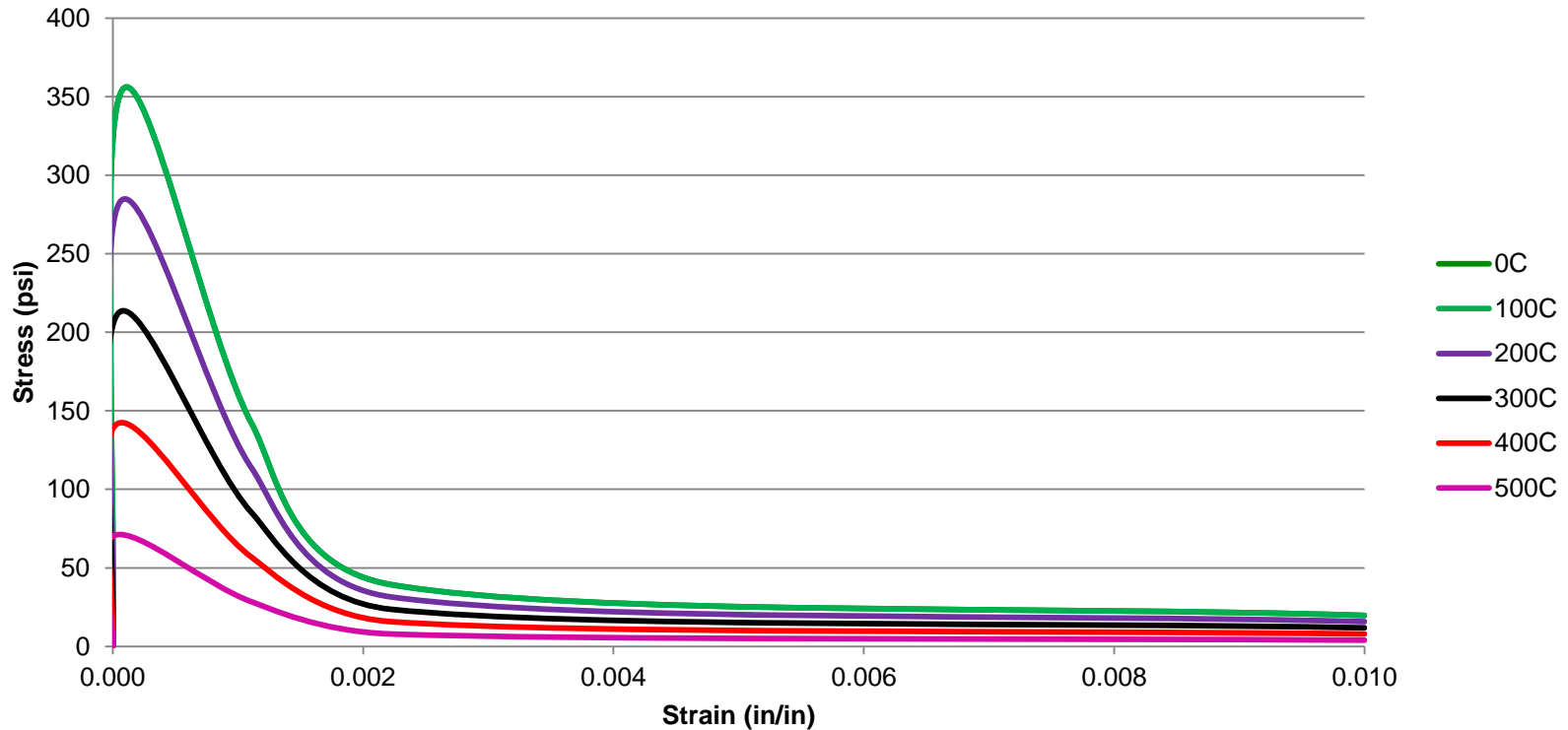
Concrete Compressive Stress-Strain Curves

Concrete Compressive Strength at Elevated Temperatures



Concrete Tensile Stress-Strain Curves

Concrete Tensile Strength at Elevated Temperatures



Steel Degradation Properties at Elevated Temperatures per Eurocode

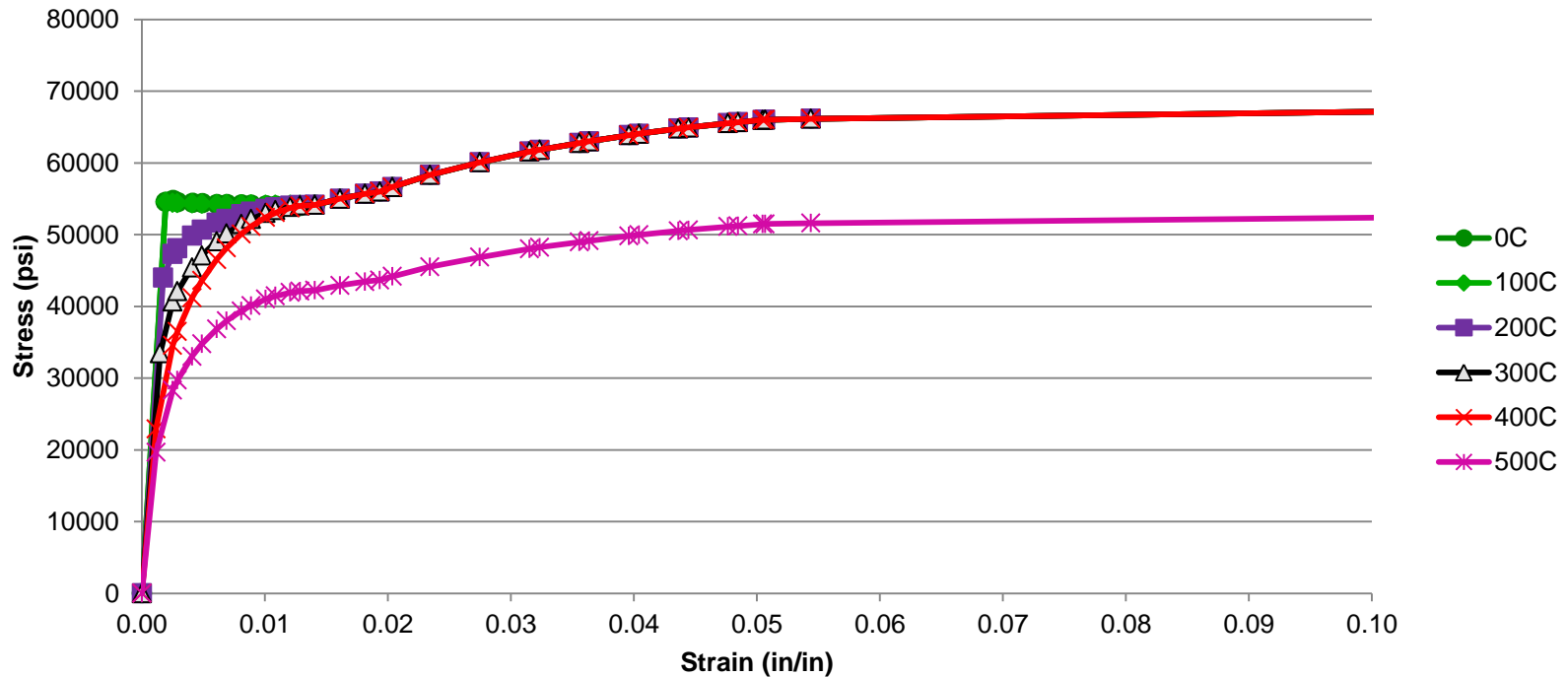
Steel Temperature θ_a	Reduction factors at temperature θ_a relative to the value of f_y or E_a at 20°C		
	Reduction factor (relative to f_y) for effective yield strength $k_{y,\theta} = f_{y\theta}/f_y$	Reduction factor (relative to f_y) for proportional limit $k_{p,\theta} = f_{p\theta}/f_y$	Reduction factor (relative to E_a) for the slope of the linear elastic range $k_{E,\theta} = E_{a\theta}/E_a$
20°C	1,000	1,000	1,000
100°C	1,000	1,000	1,000
200°C	1,000	0,807	0,900
300°C	1,000	0,613	0,800
400°C	1,000	0,420	0,700
500°C	0,780	0,360	0,600
600°C	0,470	0,180	0,310
700°C	0,230	0,075	0,130
800°C	0,110	0,050	0,090
900°C	0,060	0,0375	0,0675
1000°C	0,040	0,0250	0,0450
1100°C	0,020	0,0125	0,0225
1200°C	0,000	0,0000	0,0000

NOTE: For intermediate values of the steel temperature, linear interpolation may be used.



Liner Stress-strain curves

Figure 3-12: Liner Stress-Strain Curves at Elevated Temperatures





Analysis Results

Required Output/Results for Model 4:

1. **Description of Failure Prediction Model or Criteria**
2. **Geometric Modeling, and Model Description**
3. **Subset of response information defined by “55 standard output locations” of 1:4 Scale PCCV round-robin;**
4. **Contour Plot of Peak Strains in Liner During LST at pressure milestones: $P = 0$ (prestress applied); $1 \times P_d$; $1.5 P_d$; $2 P_d$; $2.5 P_d$; $3 P_d$; $3.3 P_d$; $3.4 P_d$; Ultimate Pressure**
5. **Average Strains over 450.45 mm Regions as shown in Figure 11, locations 3, 4, 5, but with similar locations adjacent to other penetrations, plotted vs. Pressure. (The intent is for these strains to be over a standardized gage length, which is defined by the spacing between liner anchors.)**





For direct comparison amongst participants, also requested to plot (Using Excel)

- **Liner Strain Magnitudes (Hoop Direction) at Locations Indicated in Figure 11 (of SPE problem statement), versus pressure**
 - **Tendon stress distribution at $P = 0$ (prestress applied); $1 \times P_d$; $1.5 P_d$; $2 P_d$; $2.5 P_d$; $3 P_d$; $3.3 P_d$; $3.4 P_d$; Ultimate Pressure for**
 - **Hoop Tendons # H35, H53, H68**
 - **Vertical Tendon # V37 and V46**
 - **Plots of response versus pressure for Standard Output Locations:**
 - **1-15 (displacements)**
 - **22-29 (rebar strains)**
 - **36-42 (liner strains)**
 - **48-55 (tendon strains and stresses)**
- (see Table 4-1 in NUREG/CR-6809 for locations of SOL's)**

Model 4 Results by Pressure Milestones at 6.2 m

Case 1 Results by Pressure Milestones at 6.2 m

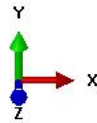
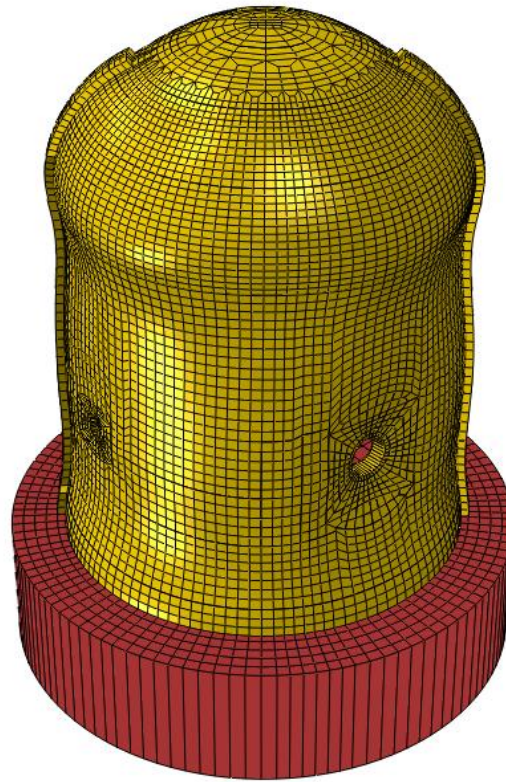
Milestone	Pressure (MPa)	x Pd
Zero Concrete Hoop Stress (at 0° azimuth)	0.78	2.00
Concrete Hoop Cracking Occurs (at 0° azimuth)	0.80	2.04
Tendon A Reach approx. 1% Strain (at 0° azimuth)	1.23	3.13
Tendon B Reach approx. 1% Strain (at 0° azimuth)	1.18	3.00

Case 2 Results by Pressure Milestones at 6.2 m

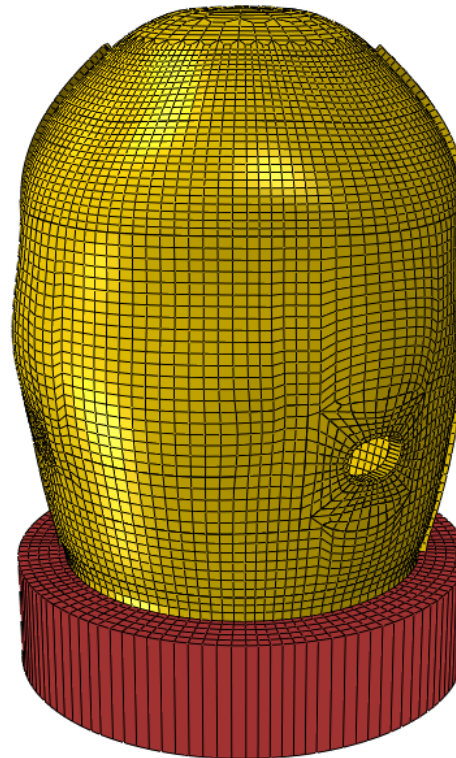
Milestone	Pressure (MPa)	x Pd
Zero Concrete Hoop Stress (at 0° azimuth)	0.74	1.89
Concrete Hoop Cracking Occurs (at 0° azimuth)	0.77	1.95
Tendon A Reach approx. 1% Strain (at 0° azimuth)	1.20	3.06
Tendon B Reach approx. 1% Strain (at 0° azimuth)	1.24	3.16



Case 1 Deformed Shape after Tendon Anchorage. Deformation Scale x 500



Case 1 Deformed Shape at 3.6 x Pd. Deformation Scale x 20

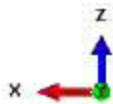


Step: Pressure_Temp_5
Increment 42: Step Time = 0.3274

Deformed Var: U Deformation Scale Factor: +2.000e+01

Case 1 Animation of a “Plan-View” Slice at a Model Elevation of 4.68m

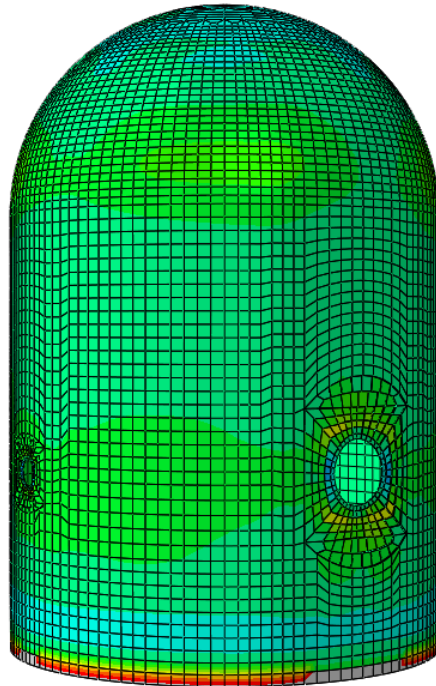
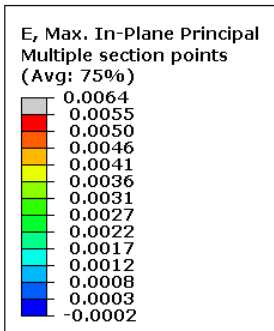
Step: Pressure_Frame: 0
Total Time: 3.000000



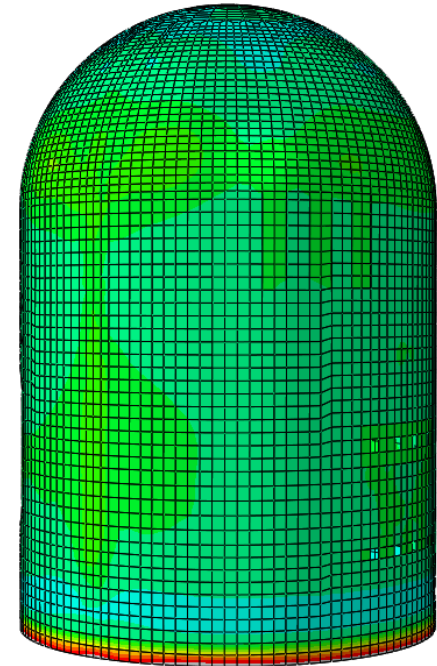
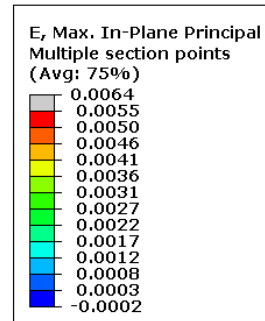
Step: Pressure_Temp_1
Increment: 0; Step Time = 0.000
Deformed Var: U; Deformation Scale Factor: +3.000e+01



Case 1 Max Principal Strain in Liner at 2.0 x Pd

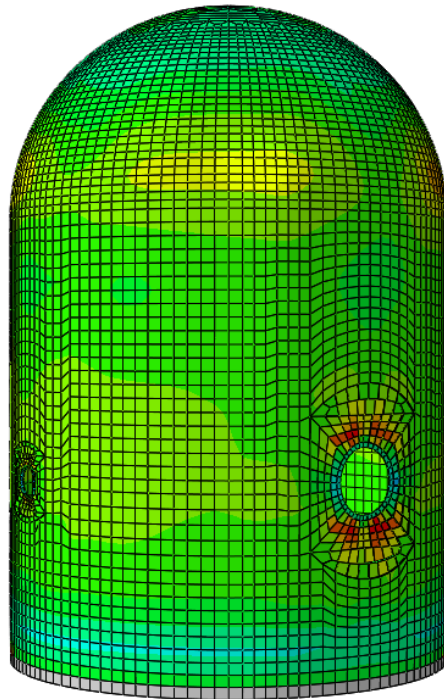
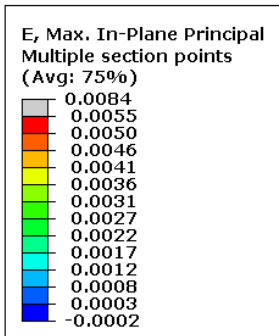


Step: Pressure_Temp_4
Increment 10: Step Time = 0.1683
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

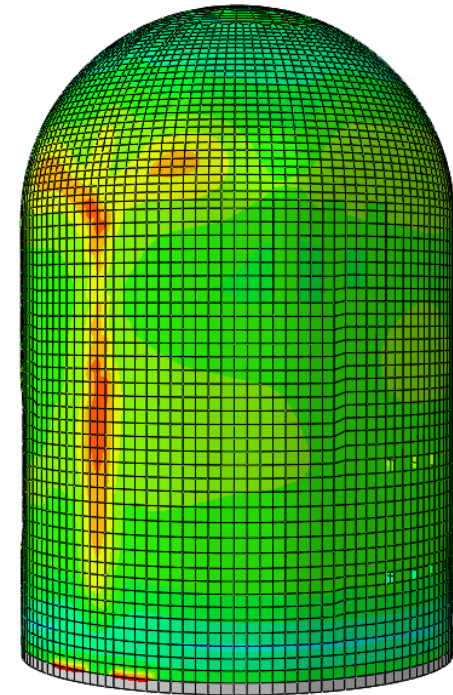
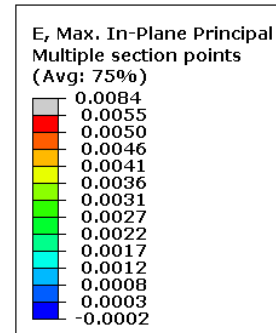


Step: Pressure_Temp_4
Increment 10: Step Time = 0.1683
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Strain in Liner at 2.5 x Pd

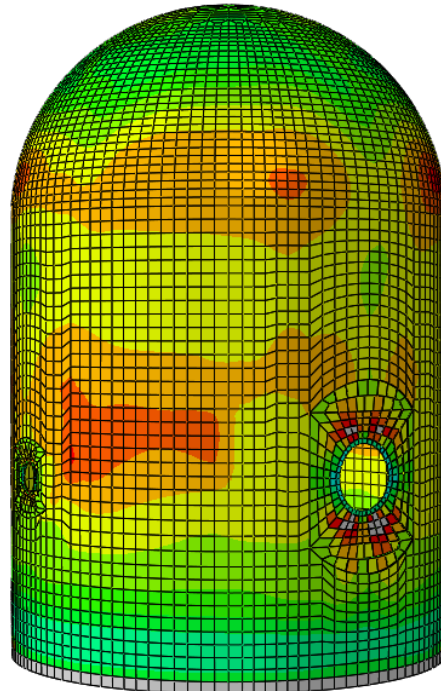
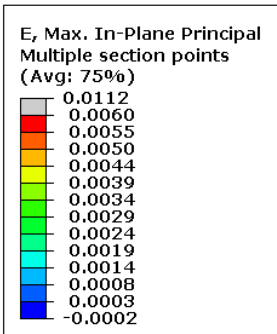


Step: Pressure_Temp_5
Increment 6: Step Time = 5.0625E-02
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

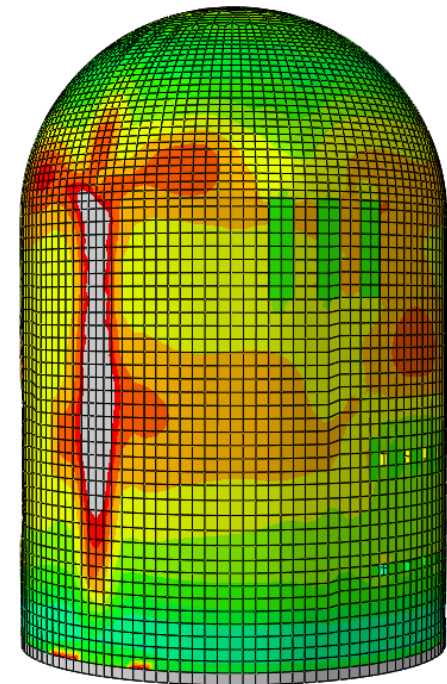
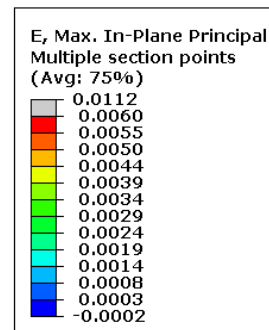


Step: Pressure_Temp_5
Increment 6: Step Time = 5.0625E-02
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Strain in Liner at 3.0 x Pd

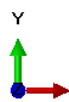
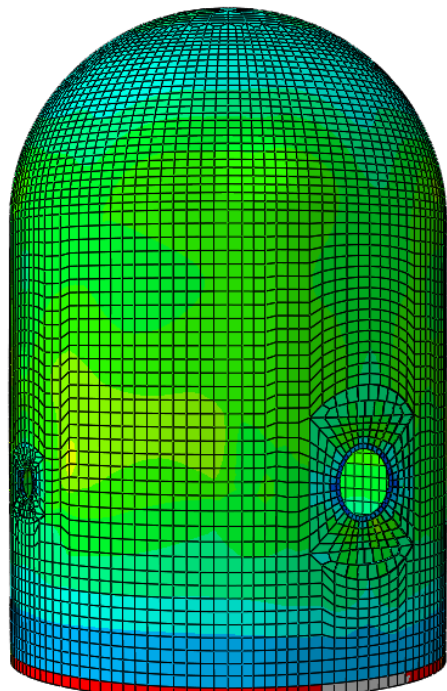
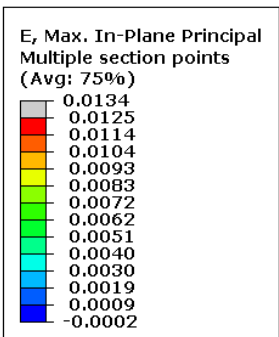


Step: Pressure_Temp_5
Increment 19; Step Time = 0.1781
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

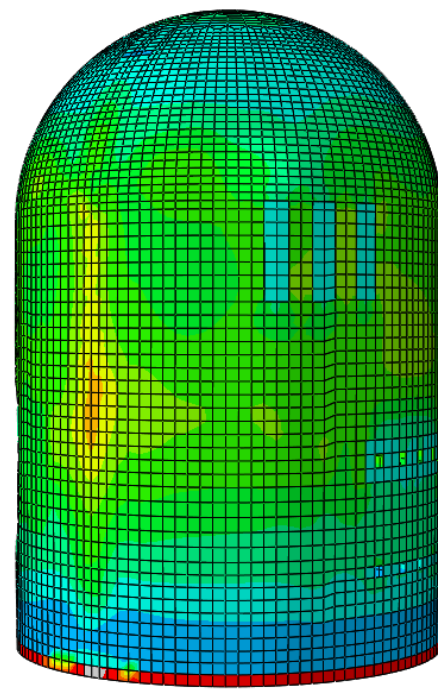
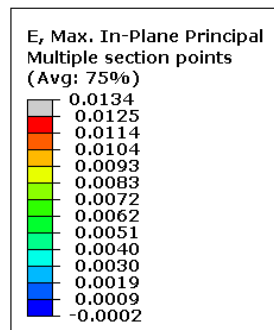


Step: Pressure_Temp_5
Increment 19; Step Time = 0.1781
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Strain in Liner at 3.3 x Pd. (Higher Contour Color Limits)

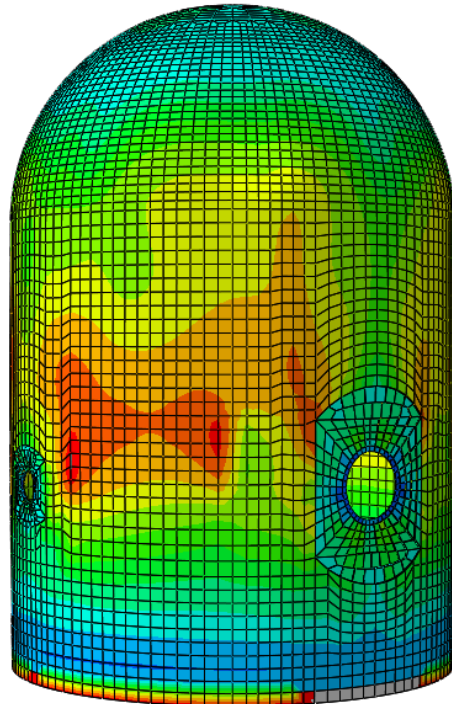
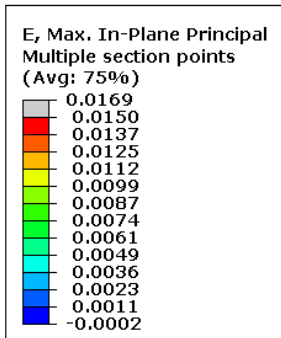


Step: Pressure_Temp_5
Increment 29: Step Time = 0.2520
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

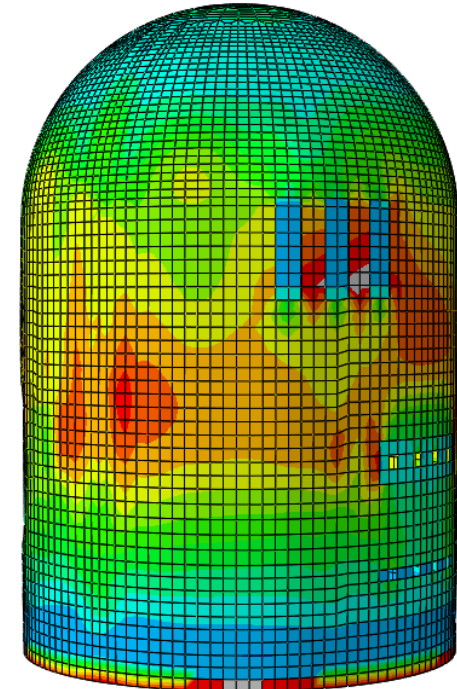
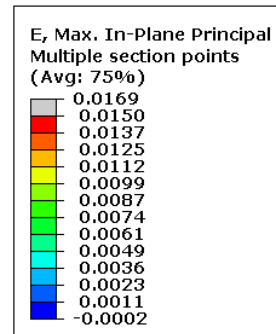


Step: Pressure_Temp_5
Increment 29: Step Time = 0.2520
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Strain in Liner at 3.6 x Pd

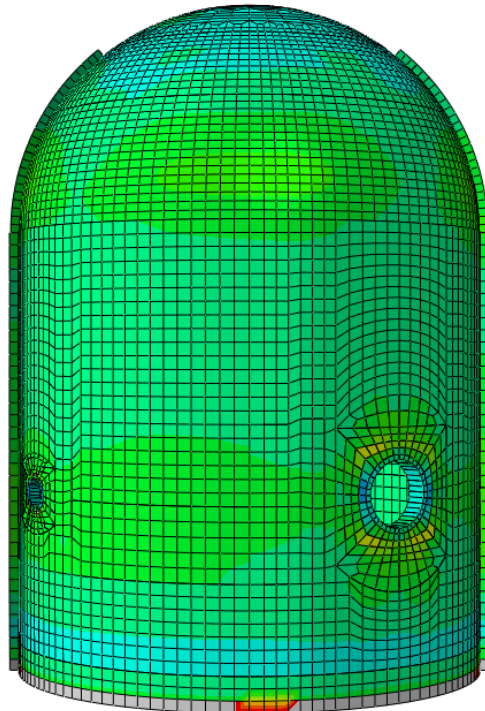
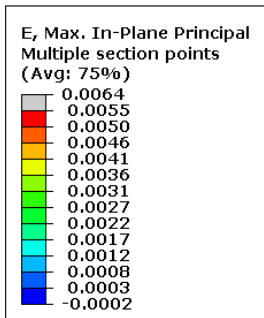


Step: Pressure_Temp_5
Increment 42: Step Time = 0.3274
Primary Var: E_r Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

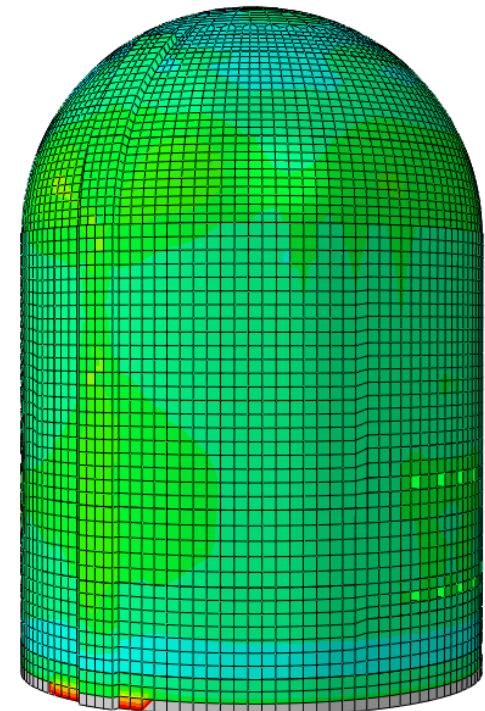
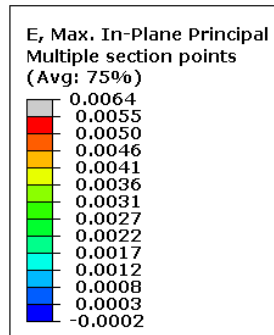


Step: Pressure_Temp_5
Increment 42: Step Time = 0.3274
Primary Var: E_r Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Membrane Strain in Concrete at 2.0 x Pd

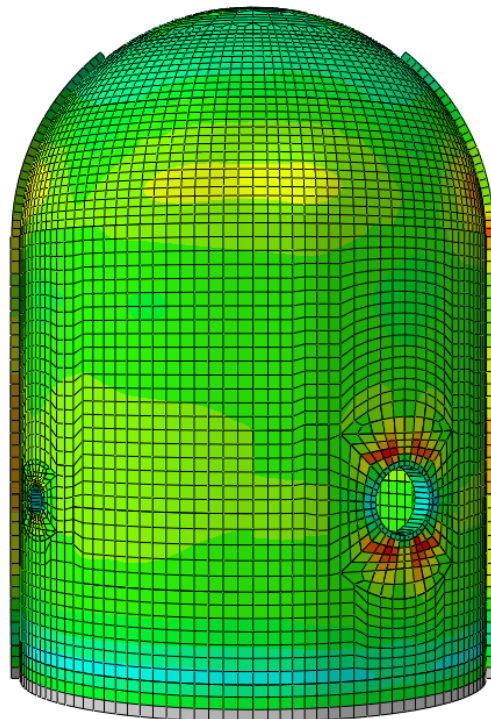
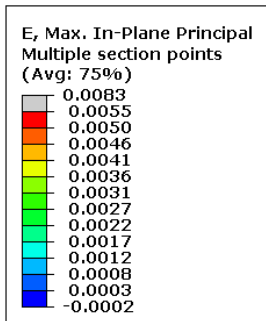


Step: Pressure_Temp_4
Increment 10: Step Time = 0.1683
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

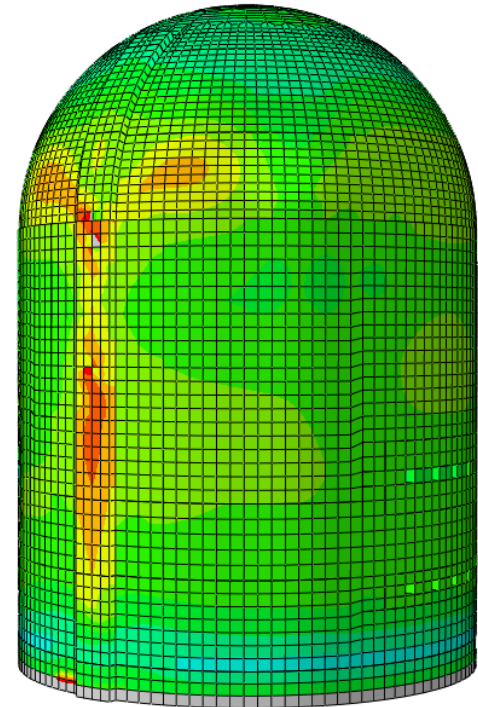
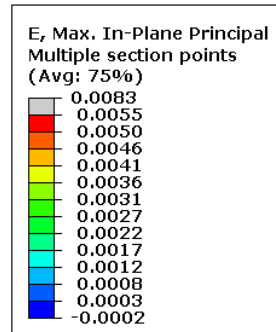


Step: Pressure_Temp_4
Increment 10: Step Time = 0.1683
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Membrane Strain in Concrete at 2.5 x Pd

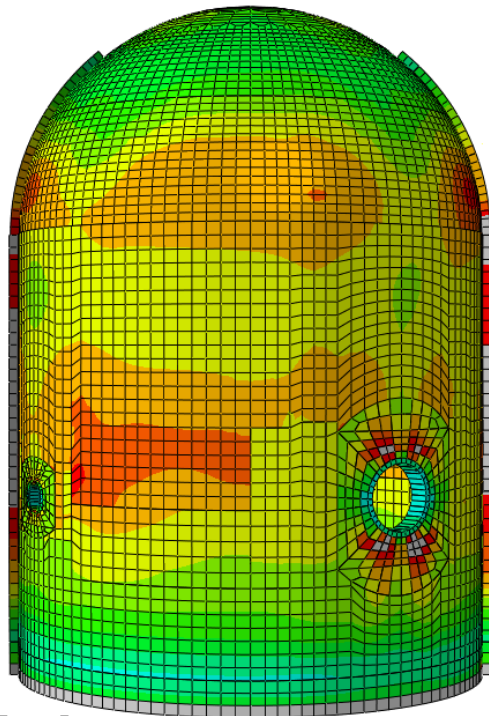
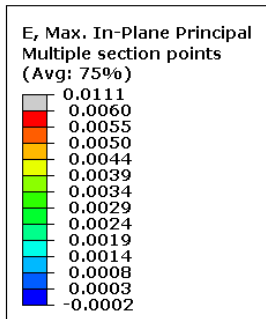


Step: Pressure_Temp_5
Increment 6: Step Time = 5.0625E-02
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

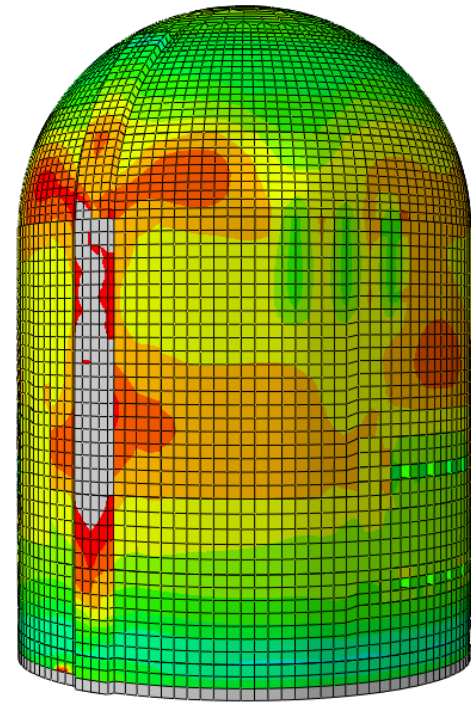
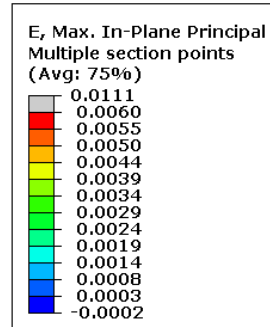


Step: Pressure_Temp_5
Increment 6: Step Time = 5.0625E-02
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Membrane Strain in Concrete at 3.0 x Pd

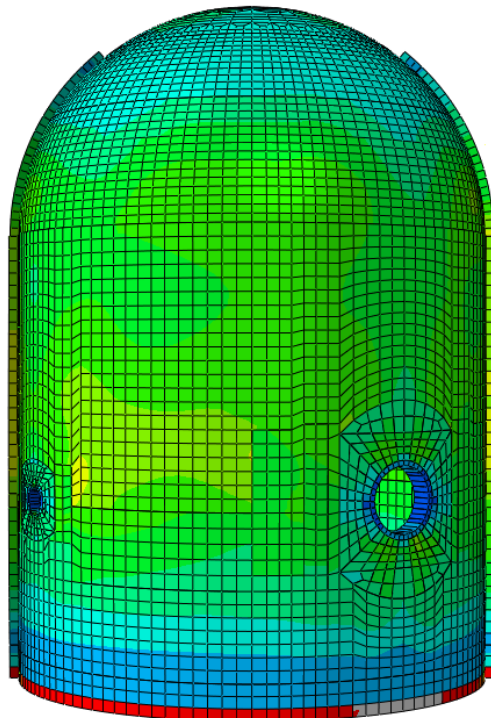
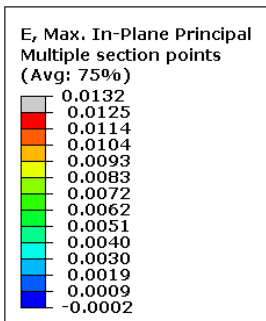


Step: Pressure_Temp_5
Increment 19: Step Time = 0.1781
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

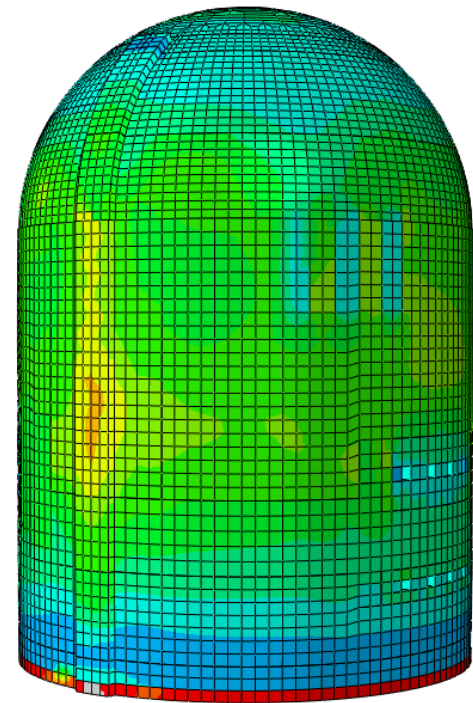
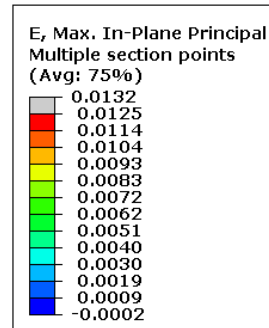


Step: Pressure_Temp_5
Increment 19: Step Time = 0.1781
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Membrane Strain in Concrete at 3.3 x Pd

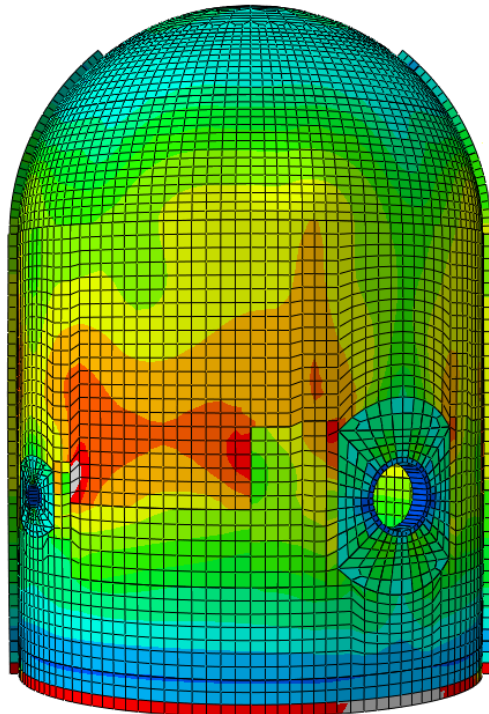
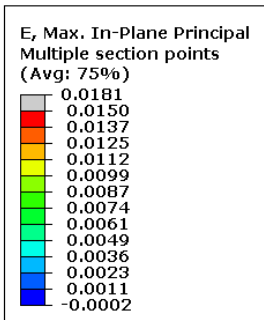


Step: Pressure_Temp_5
Increment 29; Step Time = 0.2520
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

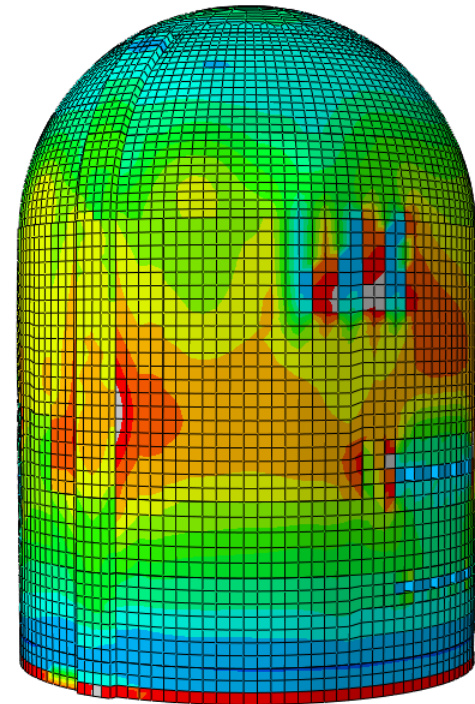
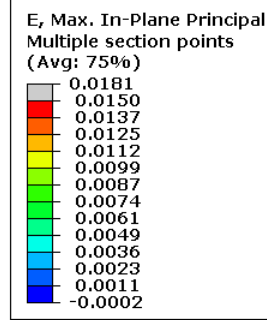


Step: Pressure_Temp_5
Increment 29; Step Time = 0.2520
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 1 Max Principal Membrane Strain in Concrete at 3.6 x Pd

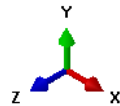
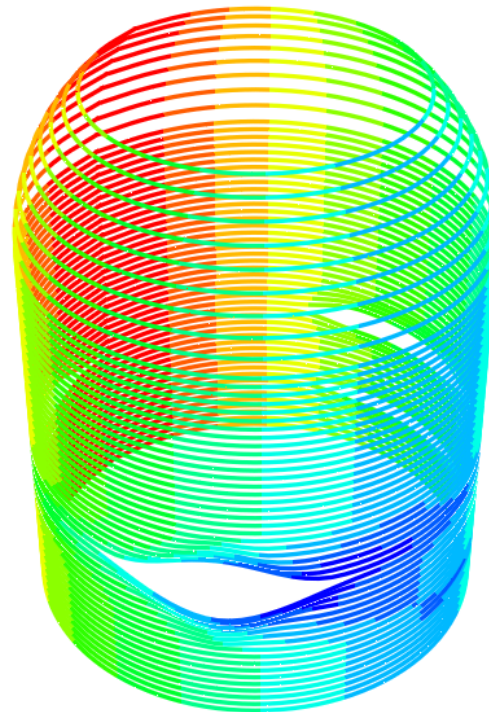
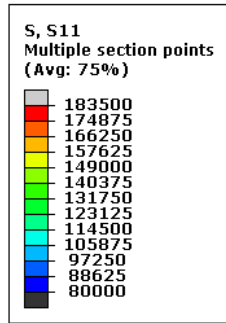


Step: Pressure_Temp_5
Increment 42; Step Time = 0.3274
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00



Step: Pressure_Temp_5
Increment 42; Step Time = 0.3274
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

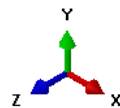
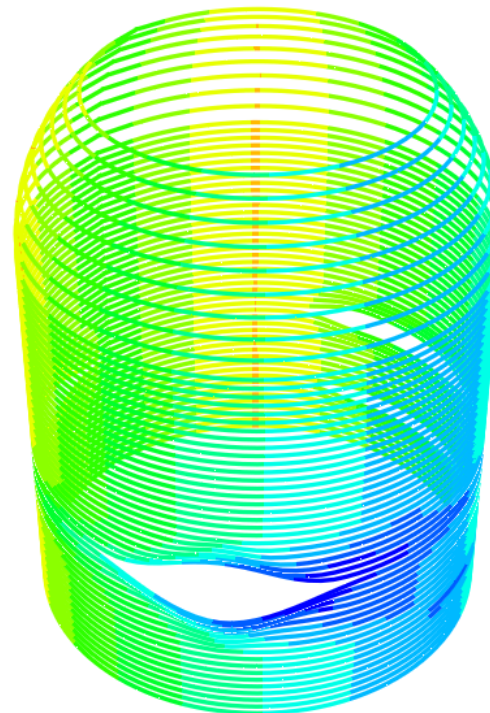
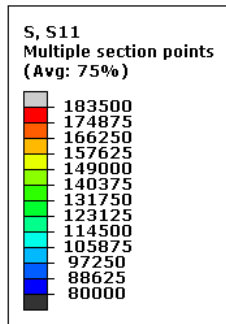
Case 1 Stress in Hoop Tendons Anchored at 90° after Jacking before Anchorage



Step: Jacking-finish
Increment 24: Step Time = 1.000
Primary Var: S, S11
Deformed Var: U Deformation Scale Factor: +1e+00



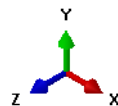
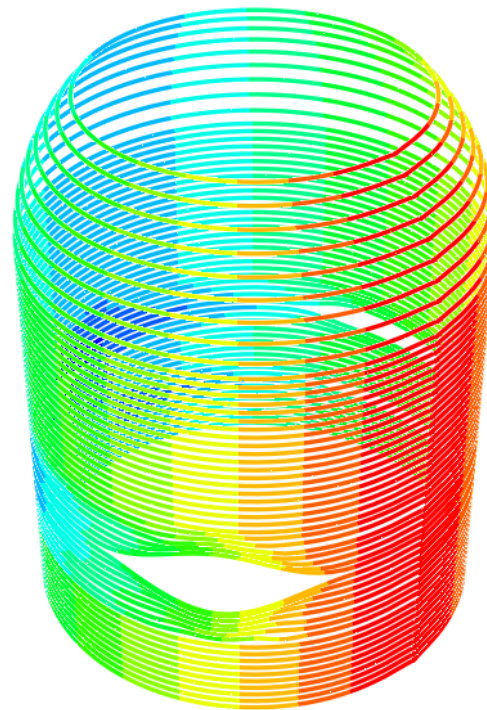
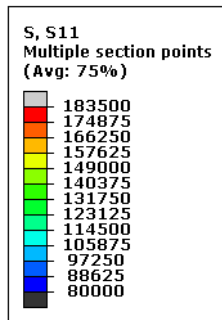
Case 1 Stress in Hoop Tendons Anchored at 90° after Anchorage



Step: Anchor
Increment 15: Step Time = 1.000
Primary Var: S, S11
Deformed Var: U Deformation Scale Factor: +1e+00



Case 1 Stress in Hoop Tendons Anchored at 270° after Jacking before Anchorage

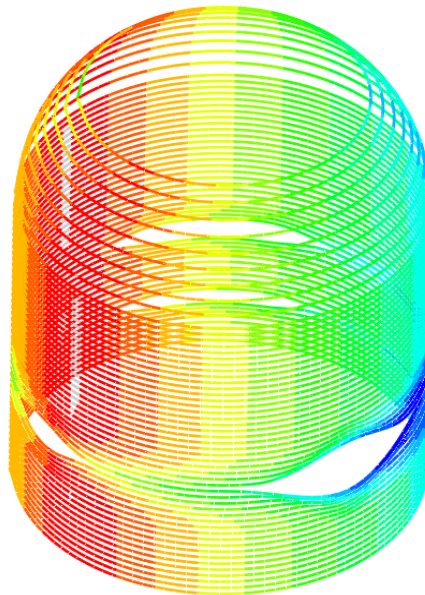
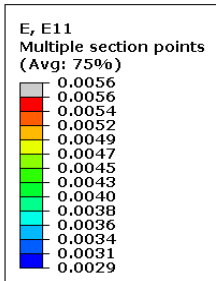


Step: Jacking-finish
Increment 24: Step Time = 1.000
Primary Var: S, S11
Deformed Var: U Deformation Scale Factor: +1e+00



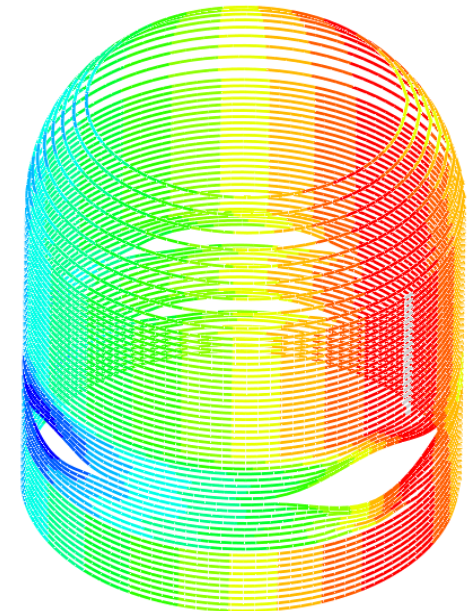
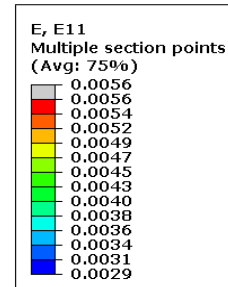
Case 1 Strain in Hoop Tendons

Anchored at 90° after Anchorage



Y
Z
Step: Anchor
Increment 33: Step Time = 1.000
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

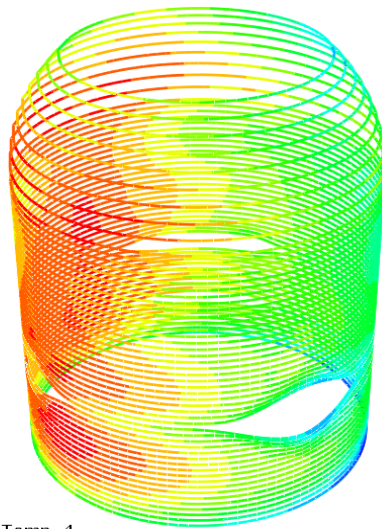
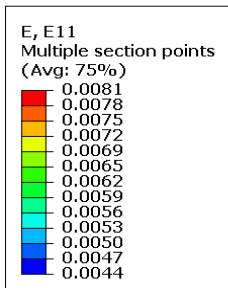
Anchored at 270° after Anchorage



Y
Z
Step: Anchor
Increment 33: Step Time = 1.000
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

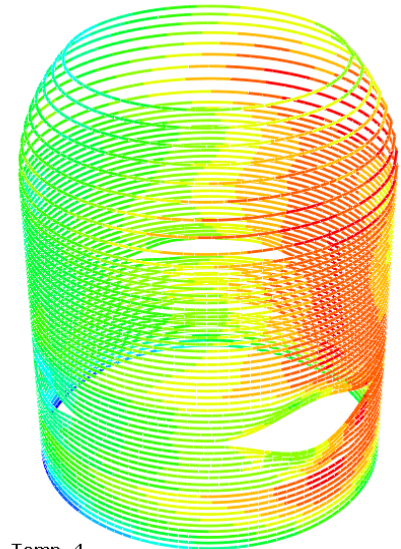
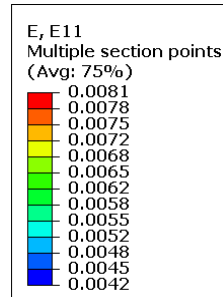
Case 1 Strain in Hoop Tendons

Anchored at 90° at 2.0 x Pd



Y
Z
Step: Pressure_Temp_4
Increment 10: Step Time = 0.1683
Primary Var: E, E11

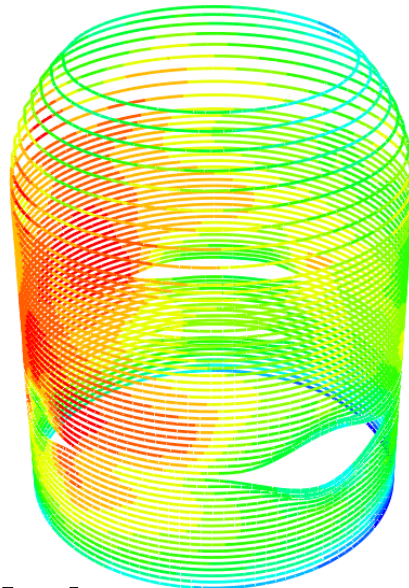
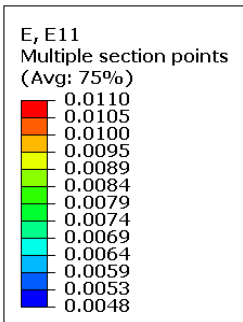
Anchored at 270° at 2.0 x Pd



Y
Z
Step: Pressure_Temp_4
Increment 10: Step Time = 0.1683
Primary Var: E, E11

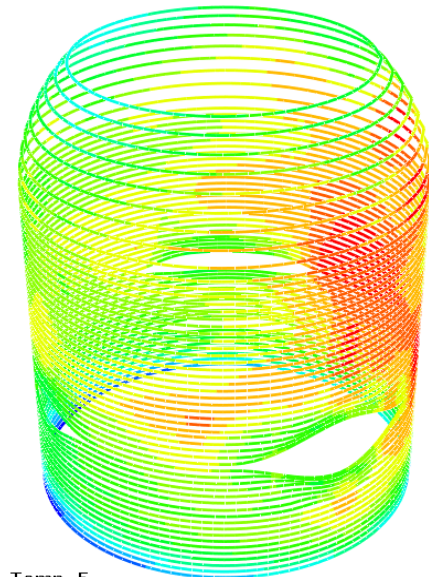
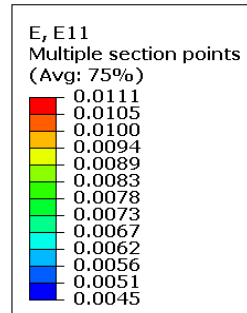
Case 1 Strain in Hoop Tendons

Anchored at 90° at 3.0 x Pd



Step: Pressure_Temp_5
Increment 19; Step Time = 0.1781
Primary Var: E, E11

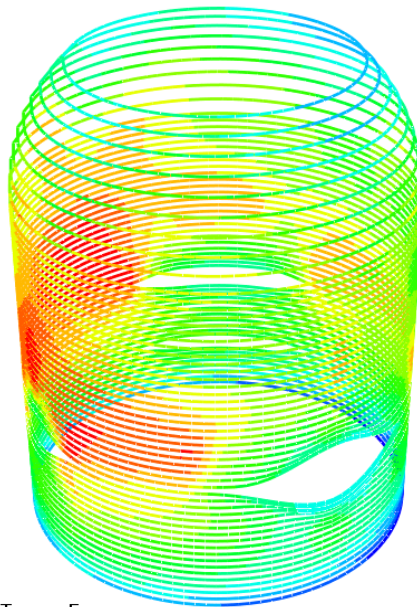
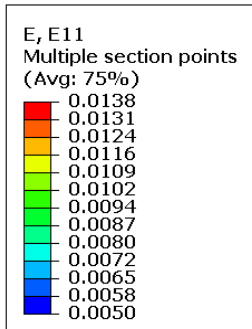
Anchored at 270° at 3.0 x Pd



Step: Pressure_Temp_5
Increment 19; Step Time = 0.1781
Primary Var: E, E11

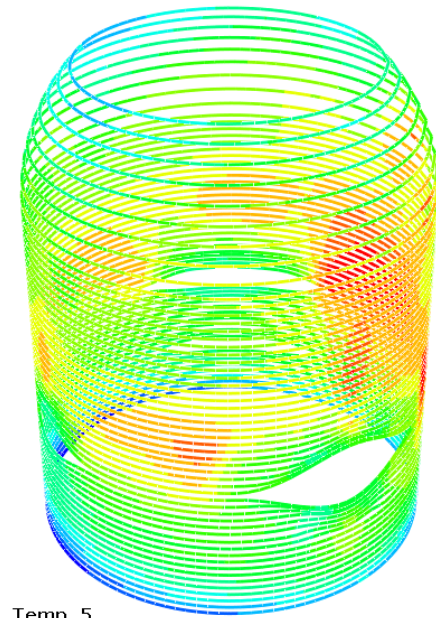
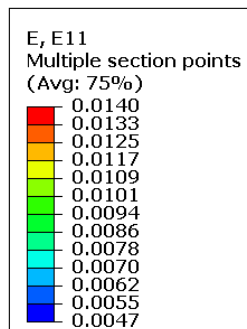
Case 1 Strain in Hoop Tendons

Anchored at 90° at 3.3 x Pd



Y
Z
Step: Pressure_Temp_5
Increment 29; Step Time = 0.2520
Primary Var: E, E11

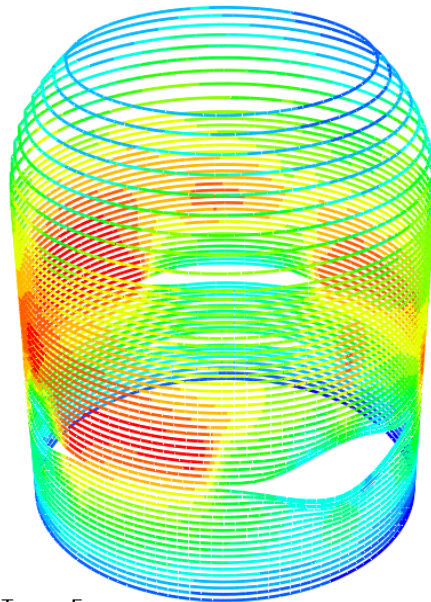
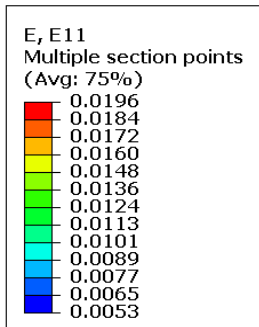
Anchored at 270° at 3.3 x Pd



Y
Z
Step: Pressure_Temp_5
Increment 29; Step Time = 0.2520
Primary Var: E, E11

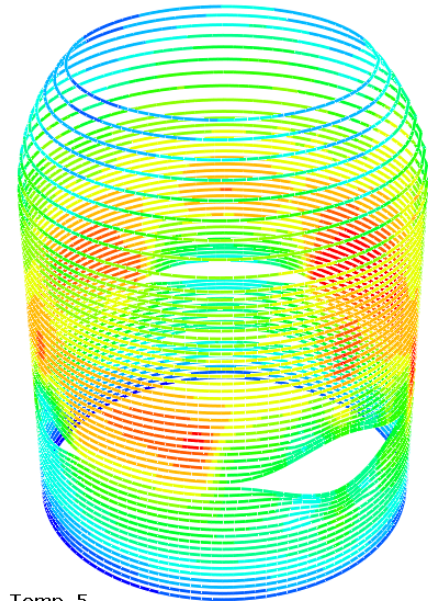
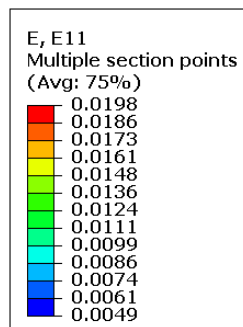
Case 1 Strain in Hoop Tendons

Anchored at 90° at 3.6 x Pd



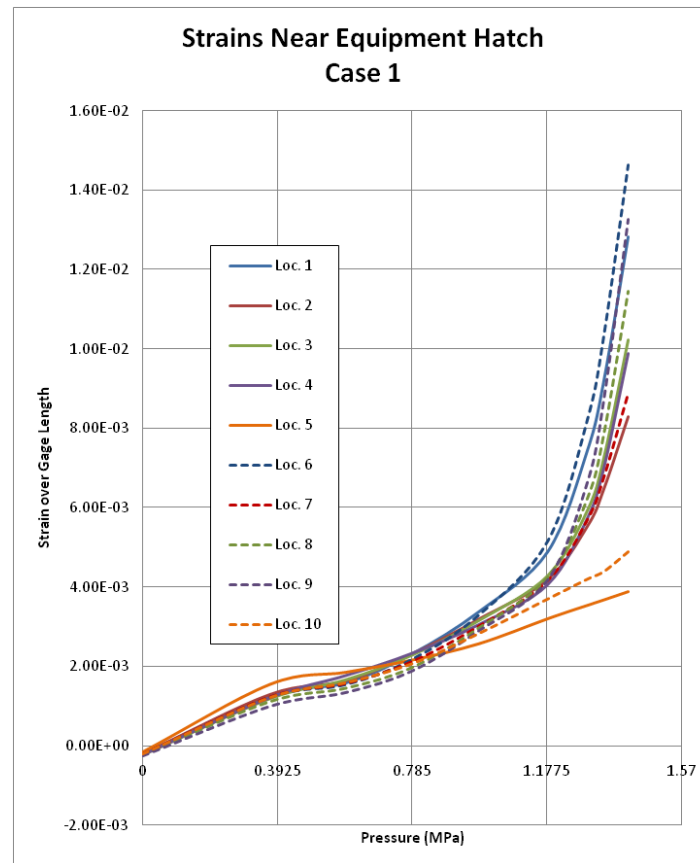
Step: Pressure_Temp_5
Increment 42: Step Time = 0.3274
Primary Var: E, E11

Anchored at 270° at 3.6 x Pd



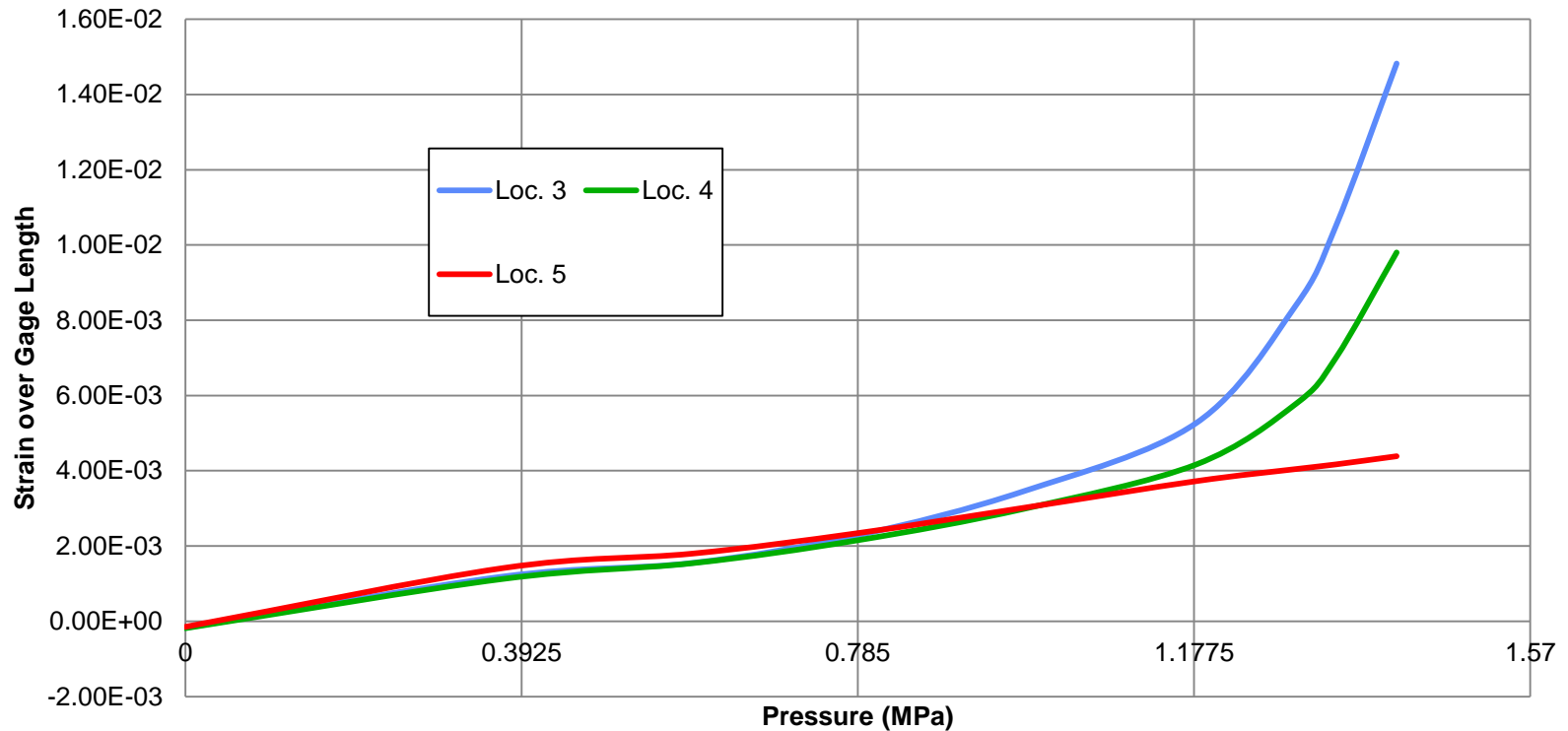
Step: Pressure_Temp_5
Increment 42: Step Time = 0.3274
Primary Var: E, E11

Case 1 Strains over Selected Gage Length Near E/H



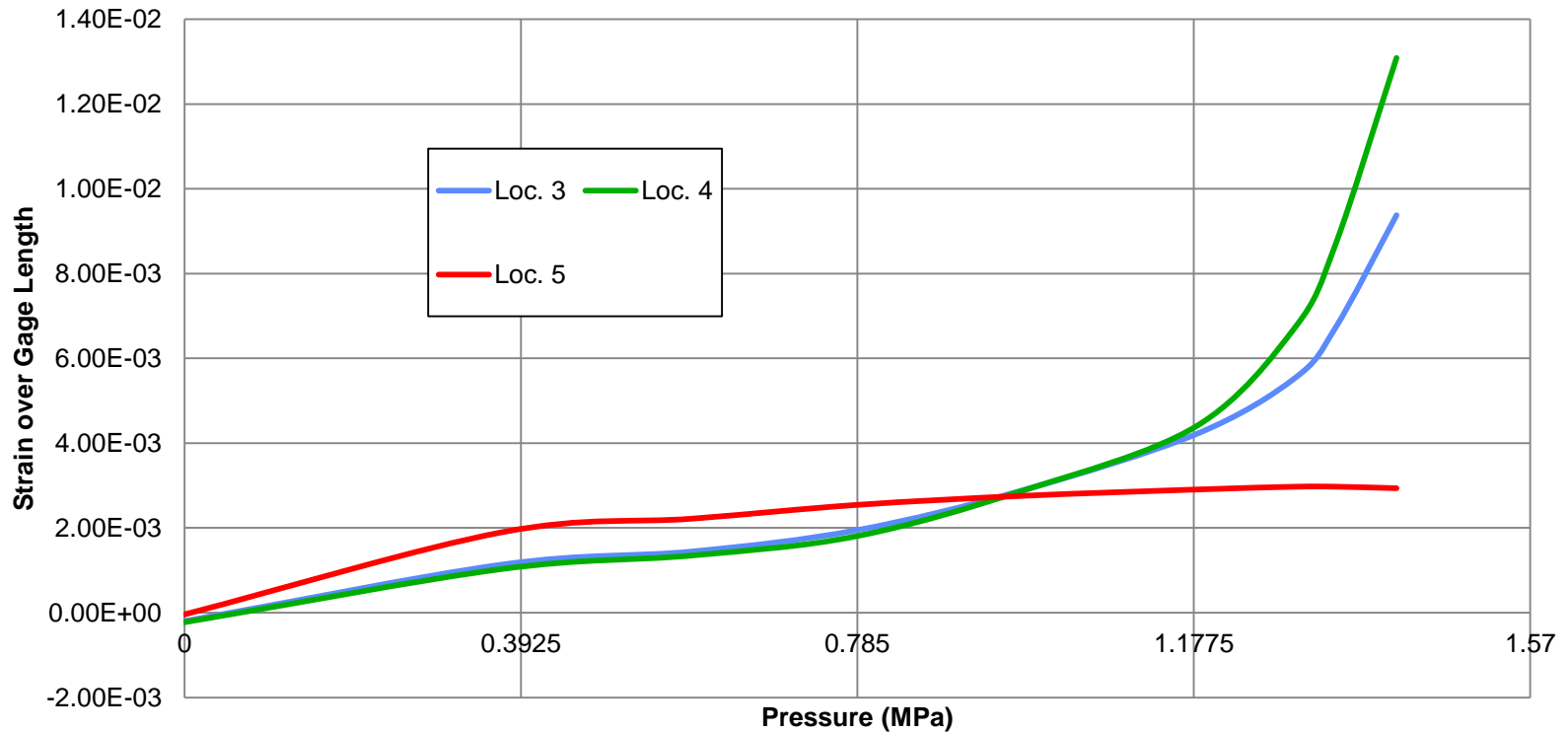
Case 1 Strains over Selected Gage Length Near A/L

Strains Near Air Lock



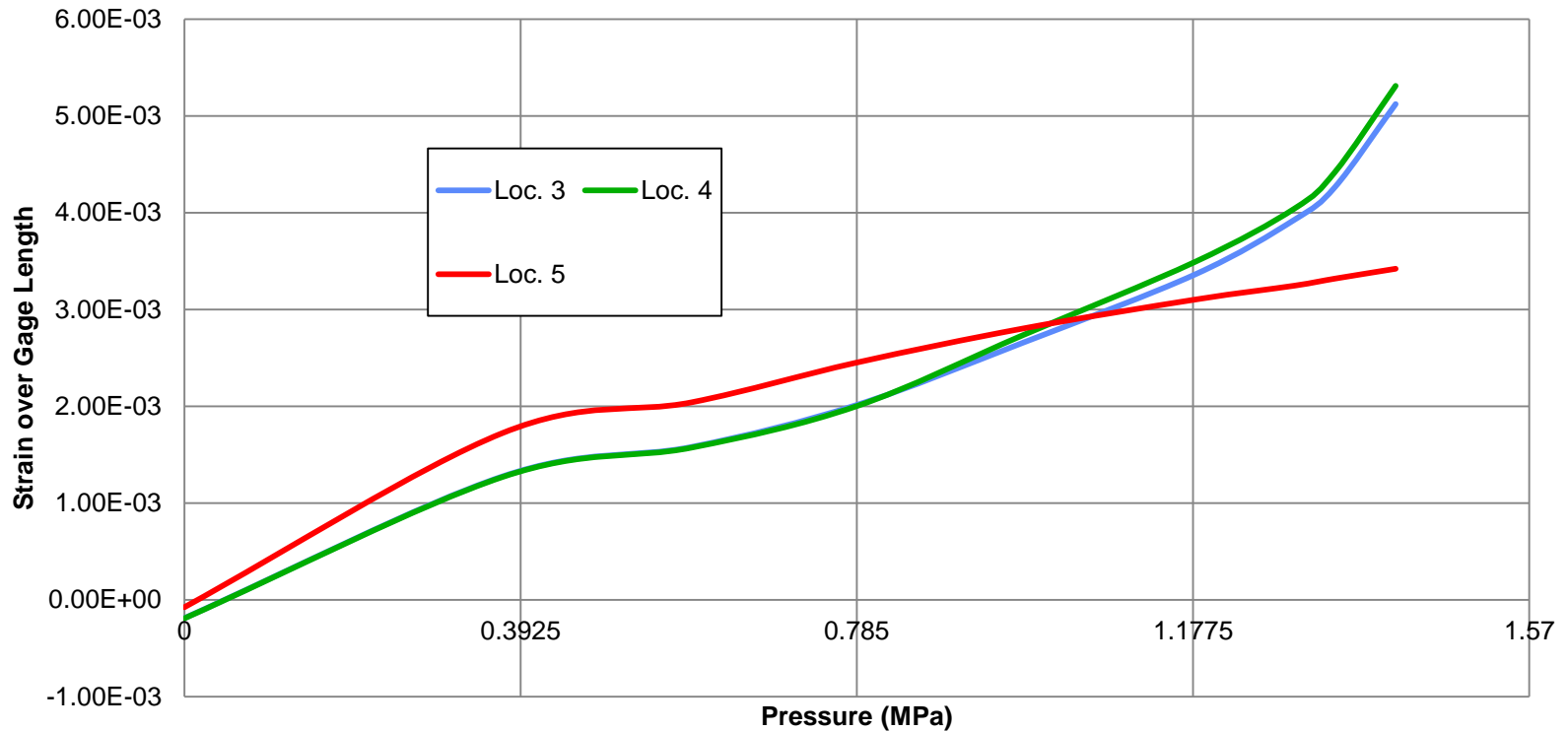
Case 1 Strains over Selected Gage Length Near M/S

Strains Near Mainsteam

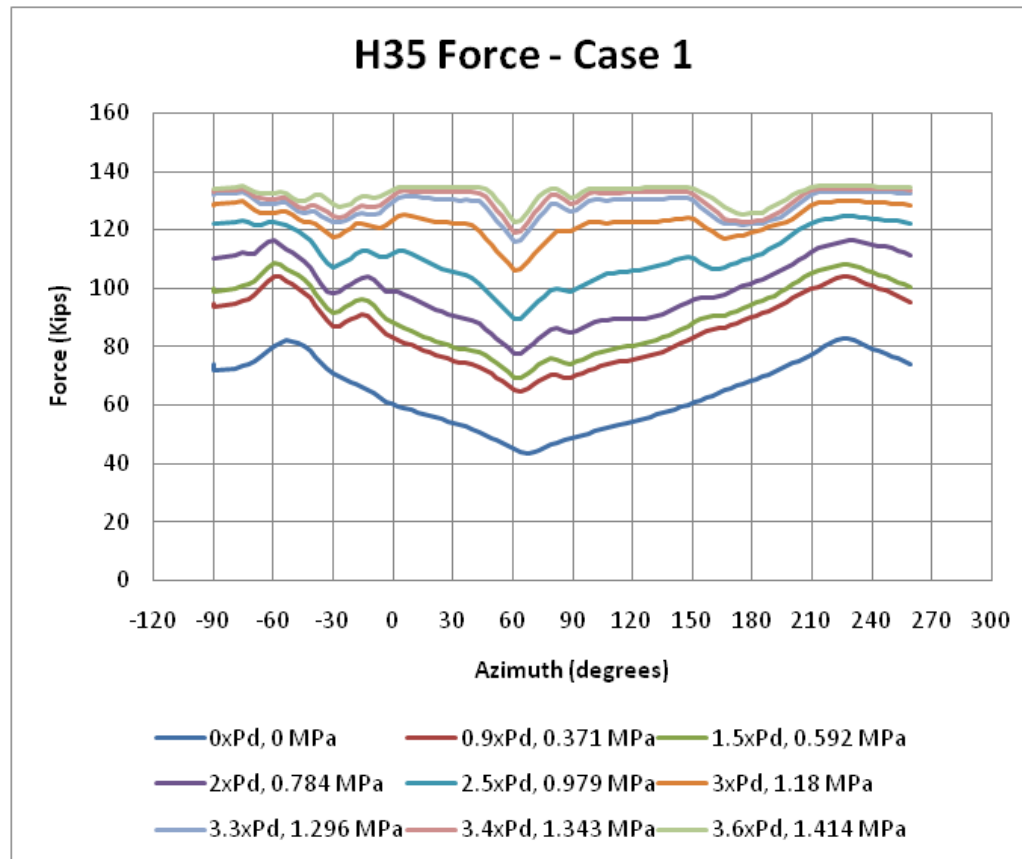


Case 1 Strains over Selected Gage Length Near F/W

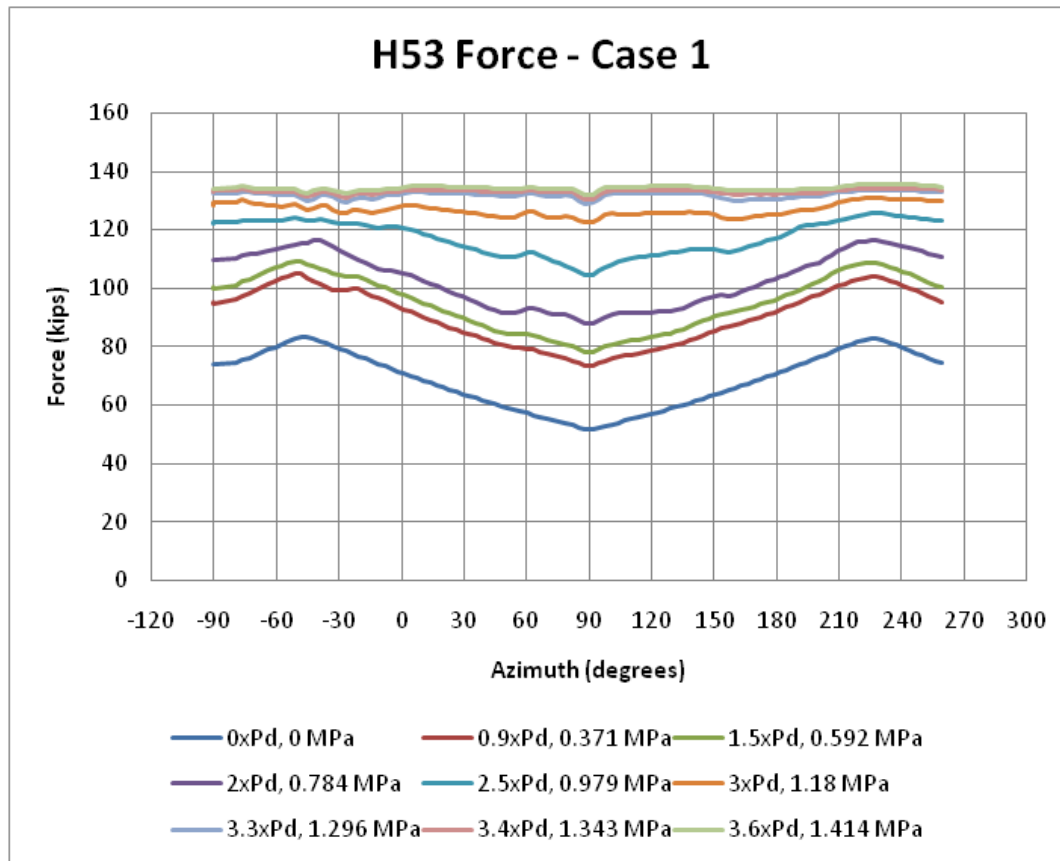
Strains Near Feed Water



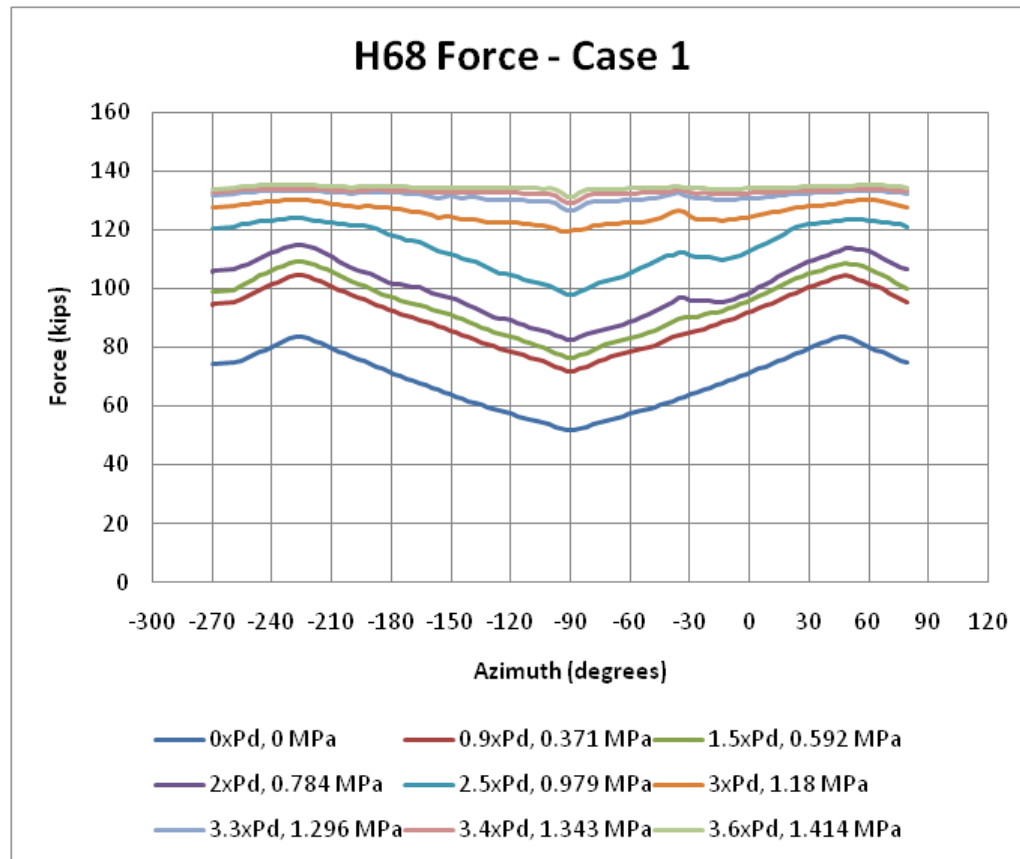
Case 1 Abaqus Analysis – Hoop Tendon H35 Force



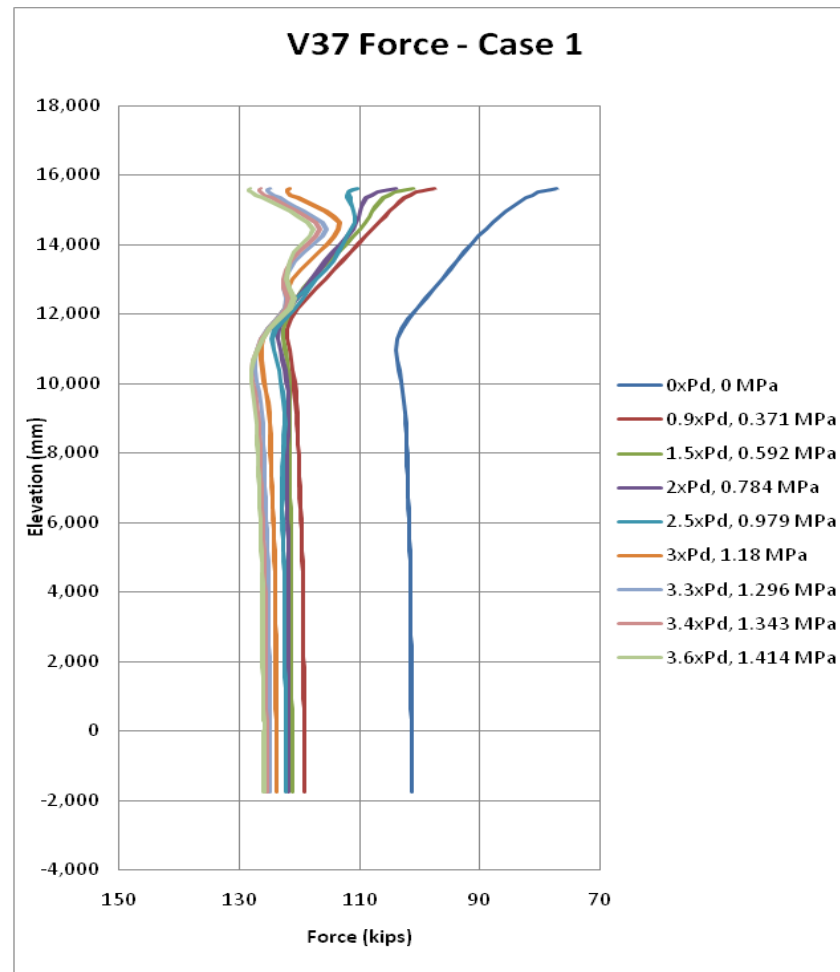
Case 1 Abaqus Analysis – Hoop Tendon H53 Force



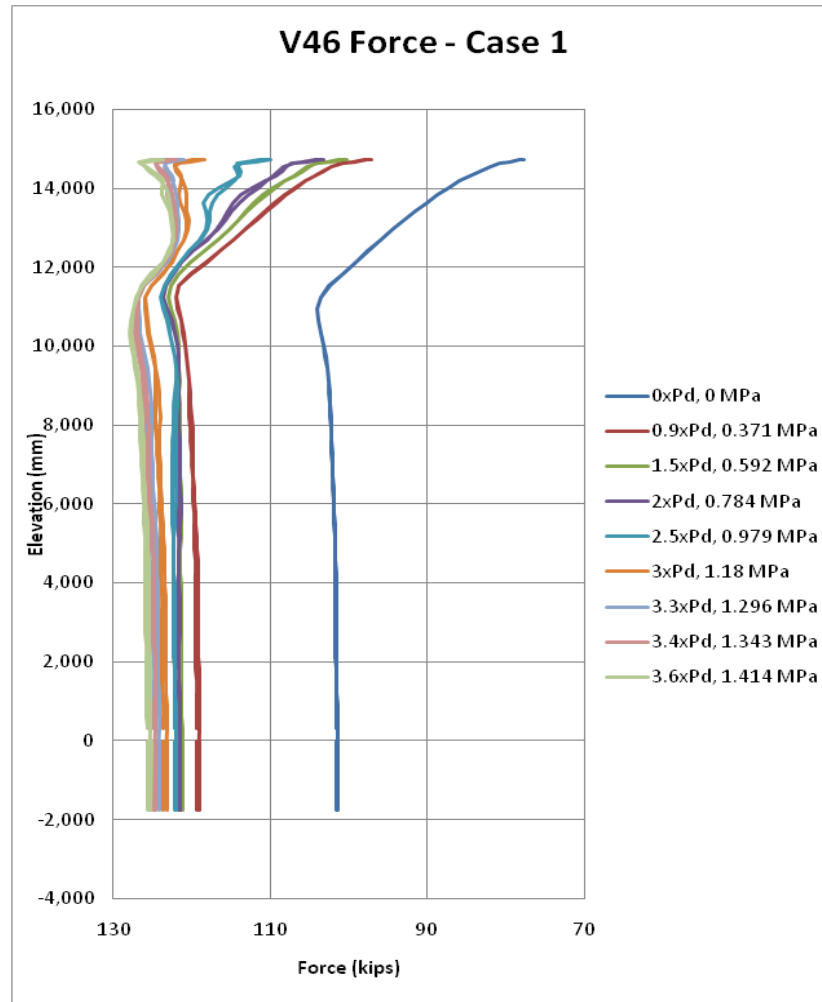
Case 1 Abaqus Analysis – Hoop Tendon H68 Force



Case 1 Abaqus Analysis – Hairpin Tendon V37 Force



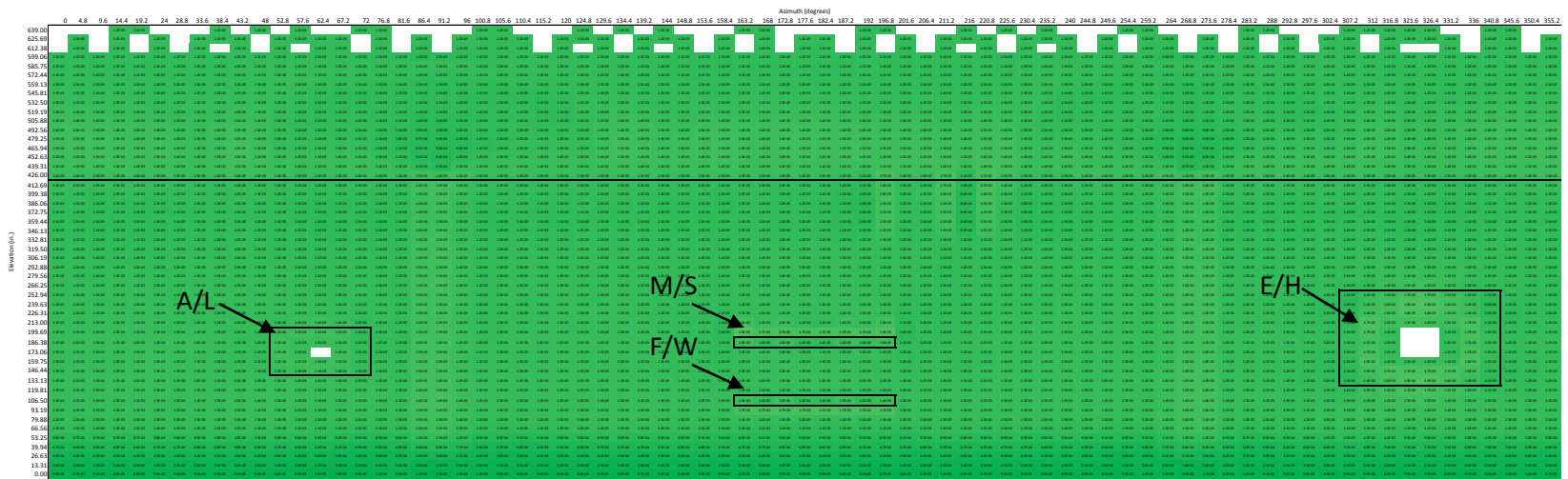
Case 1 Abaqus Analysis – Hairpin Tendon V46 Force



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



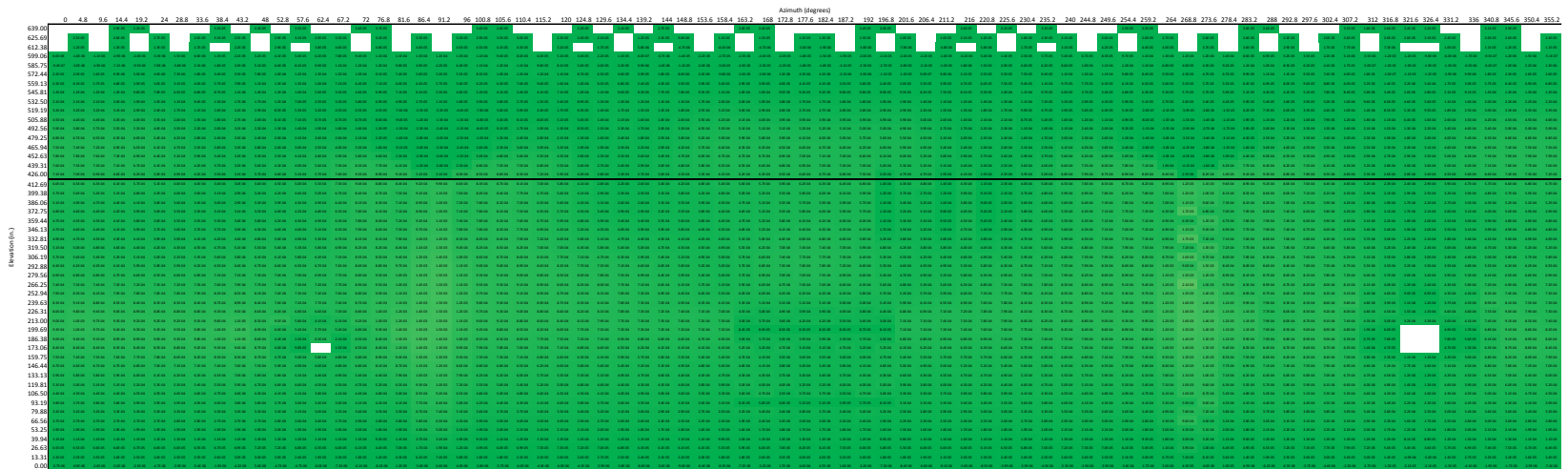
Strain Map of Entire Liner Surface at 1.0xPd



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



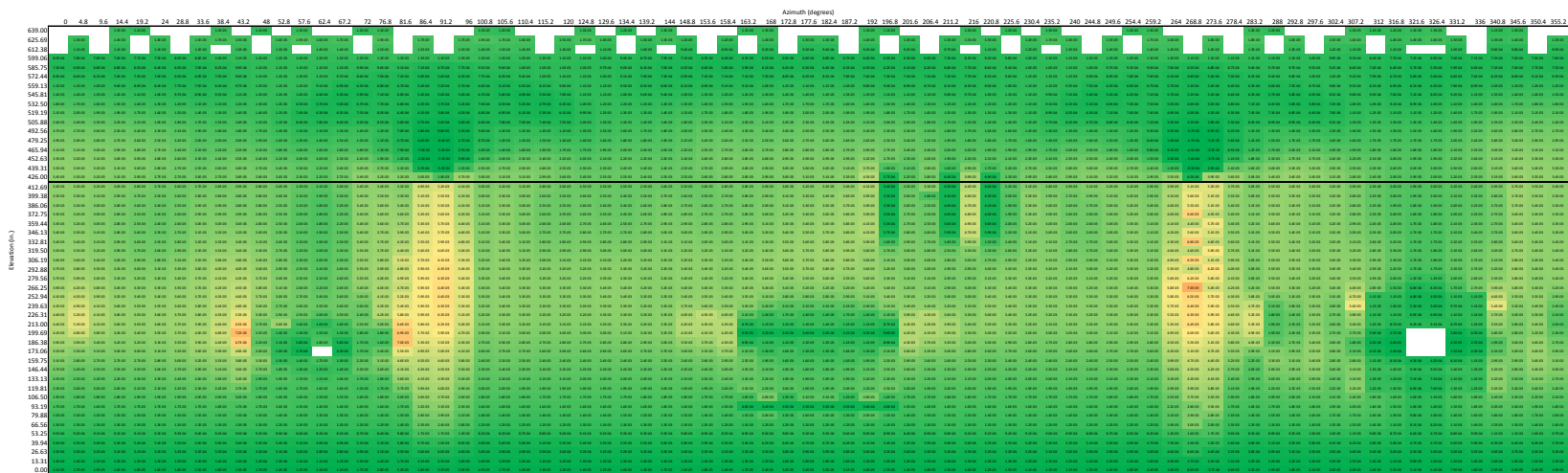
Strain Map of Entire Liner Surface at 2.0xPd



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red

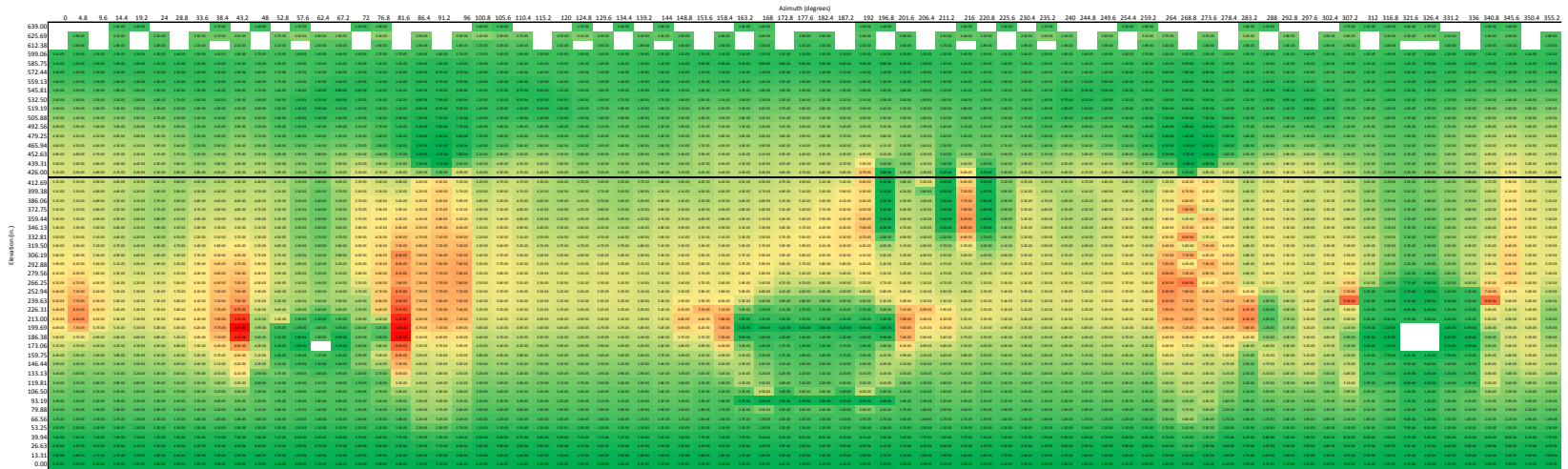


Strain Map of Entire Liner Surface at 3.0xPd



Liner Strain Mapping Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red

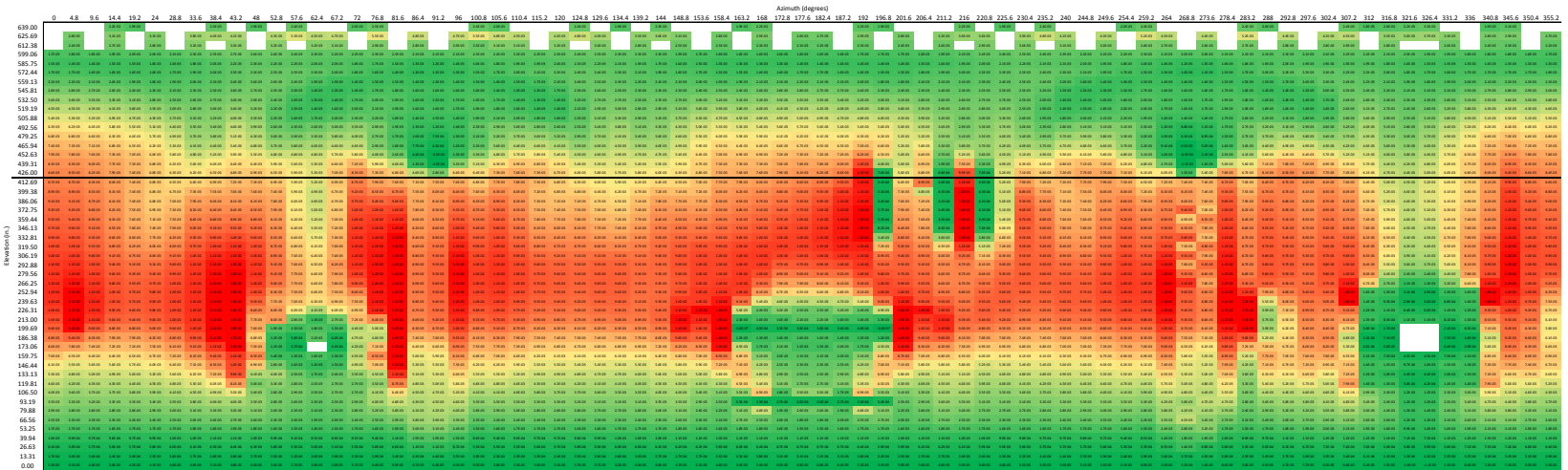


Strain Map of Entire Liner Surface at 3.3xPd



Liner Strain Mapping Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



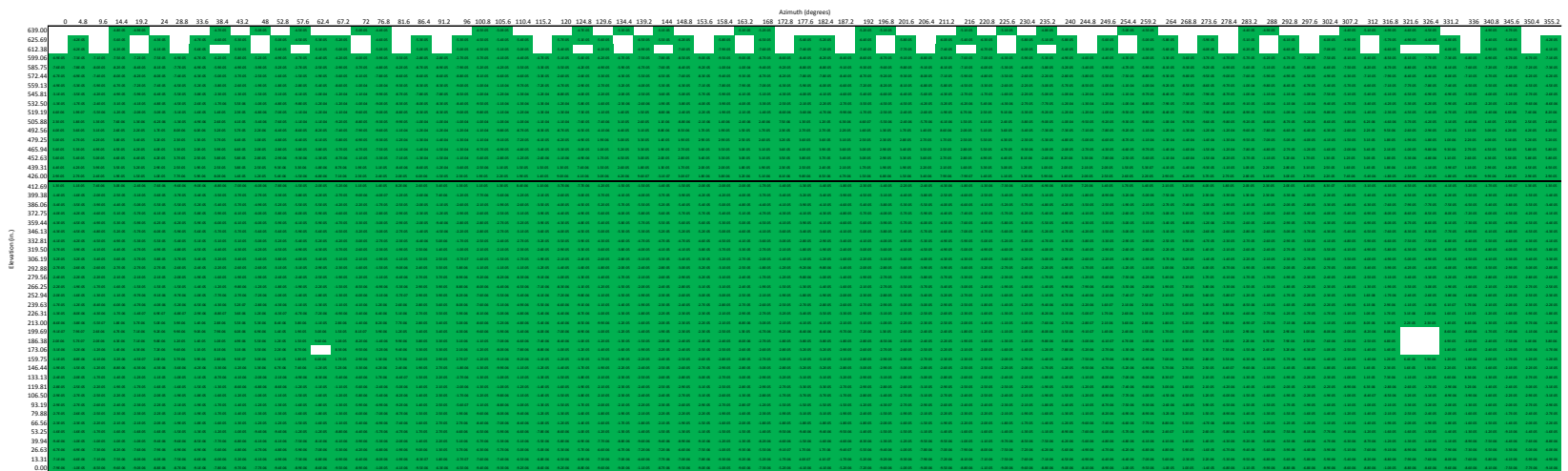
Strain Map of Entire Liner Surface at 3.6xPd



Liner Strain Mapping

Case 1 – Saturated Steam Condition

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



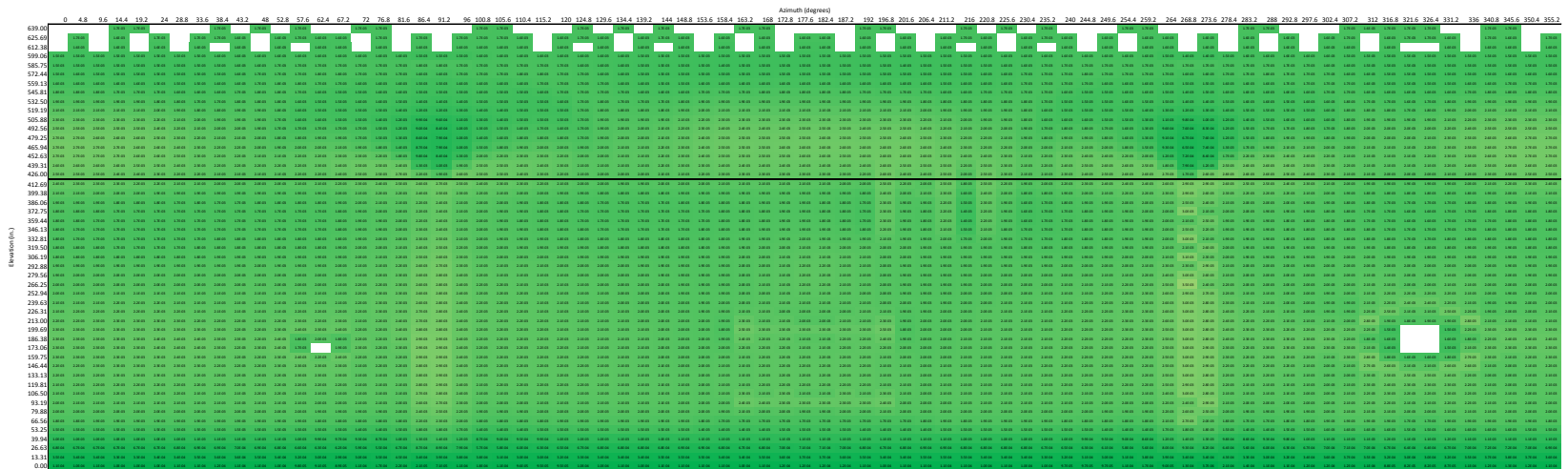
Strain Map of Entire Liner Surface at 1.0xPd



Liner Strain Mapping

Case 1 – Saturated Steam Condition

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



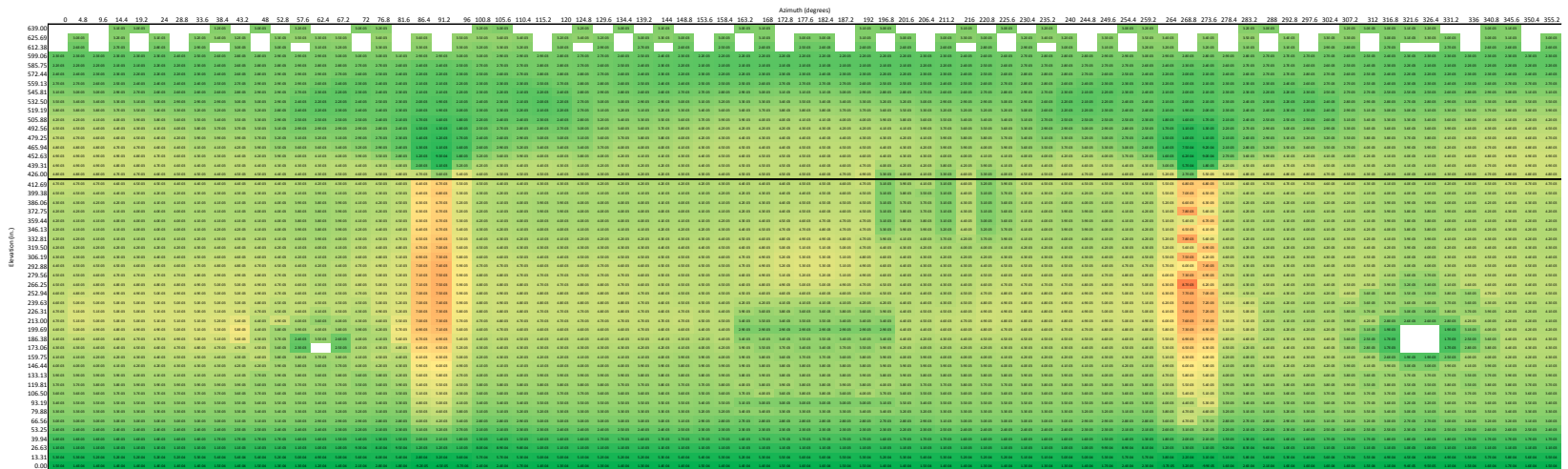
Strain Map of Entire Liner Surface at 2.0xPd



Liner Strain Mapping

Case 1 – Saturated Steam Condition

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



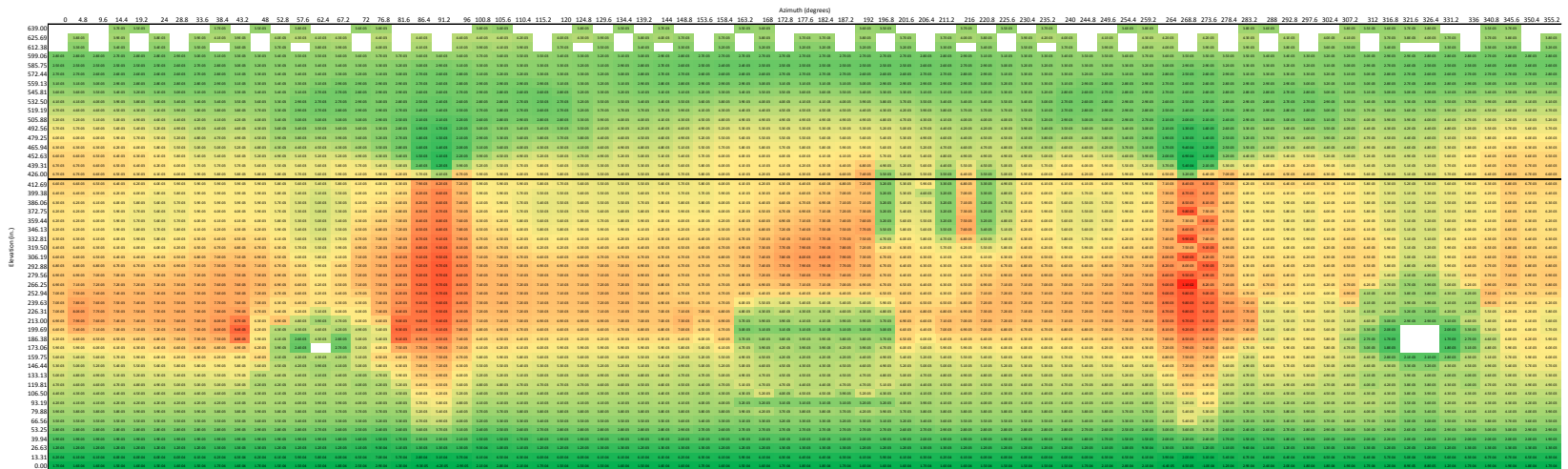
Strain Map of Entire Liner Surface at 3.0xPd



Liner Strain Mapping

Case 1 – Saturated Steam Condition

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



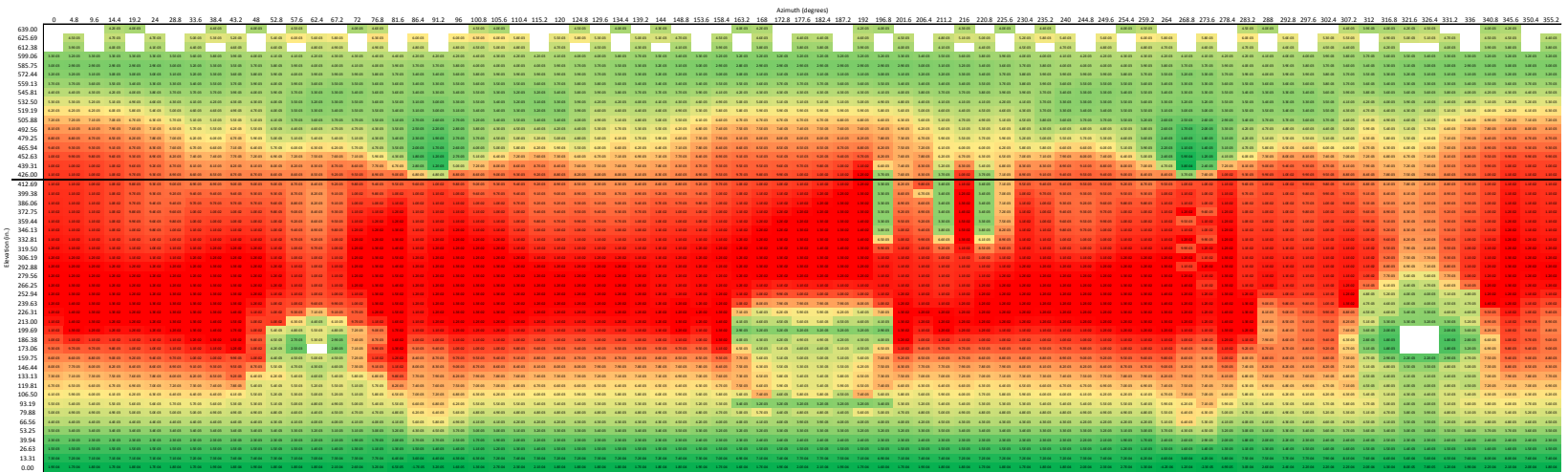
Strain Map of Entire Liner Surface at 3.3xPd



Liner Strain Mapping

Case 1 – Saturated Steam Condition

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



Strain Map of Entire Liner Surface at 3.6xPd





Model 4 Case 2 Presentation

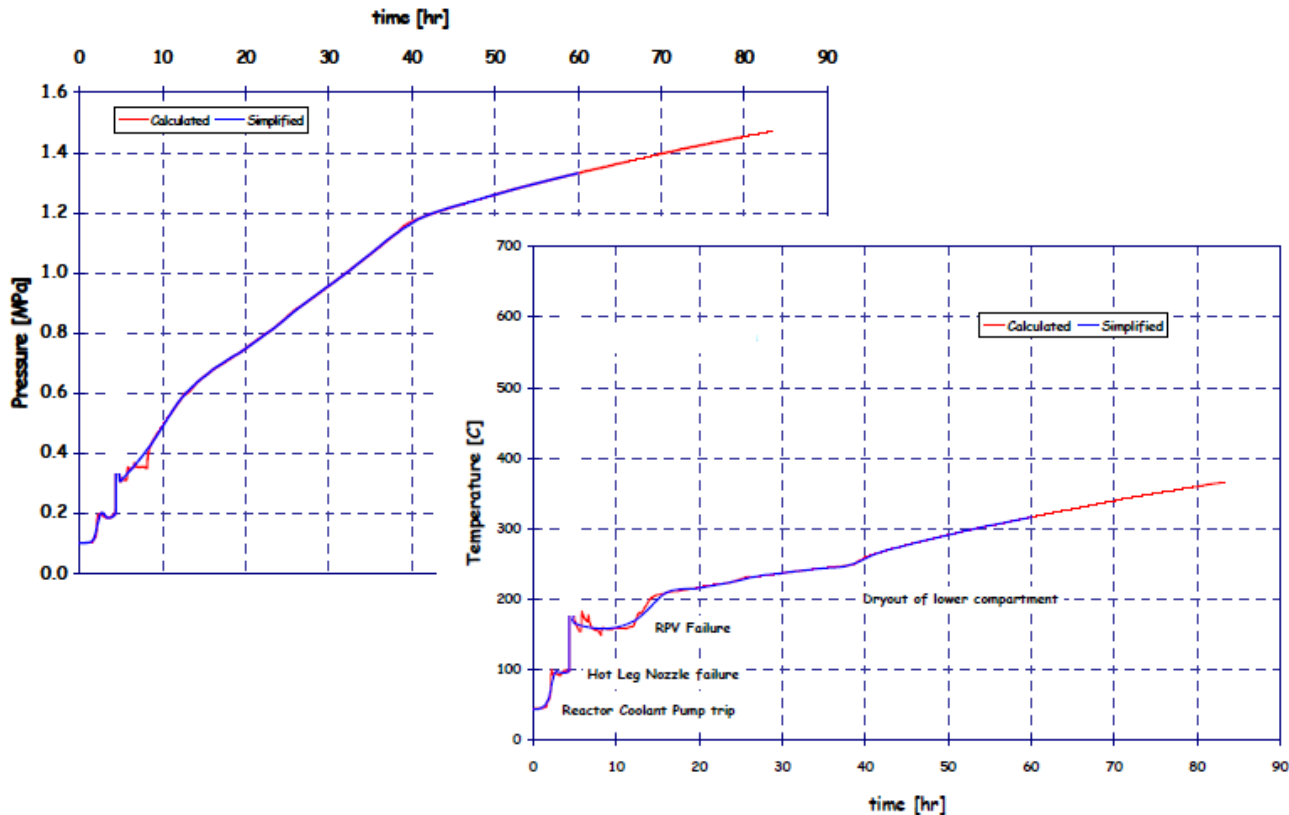




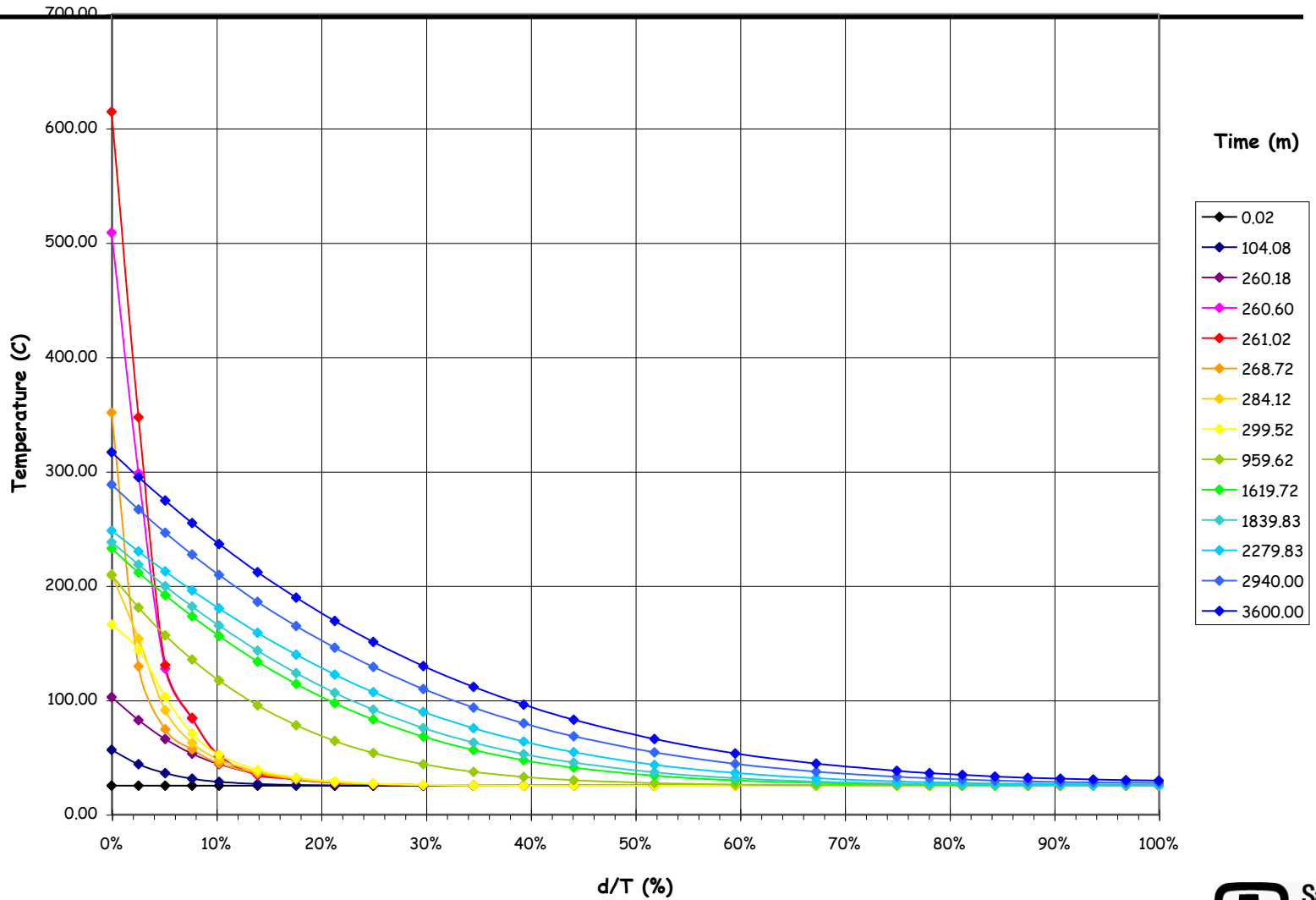
Model 4

Case 2 – Blackout Station

- An accident safety case (large dry PWR), ignoring hydrogen burn at approx. 4-1/2 hrs due to general consensus on its lack of effect on leak rate



Case 2 Gradients @ Section 2

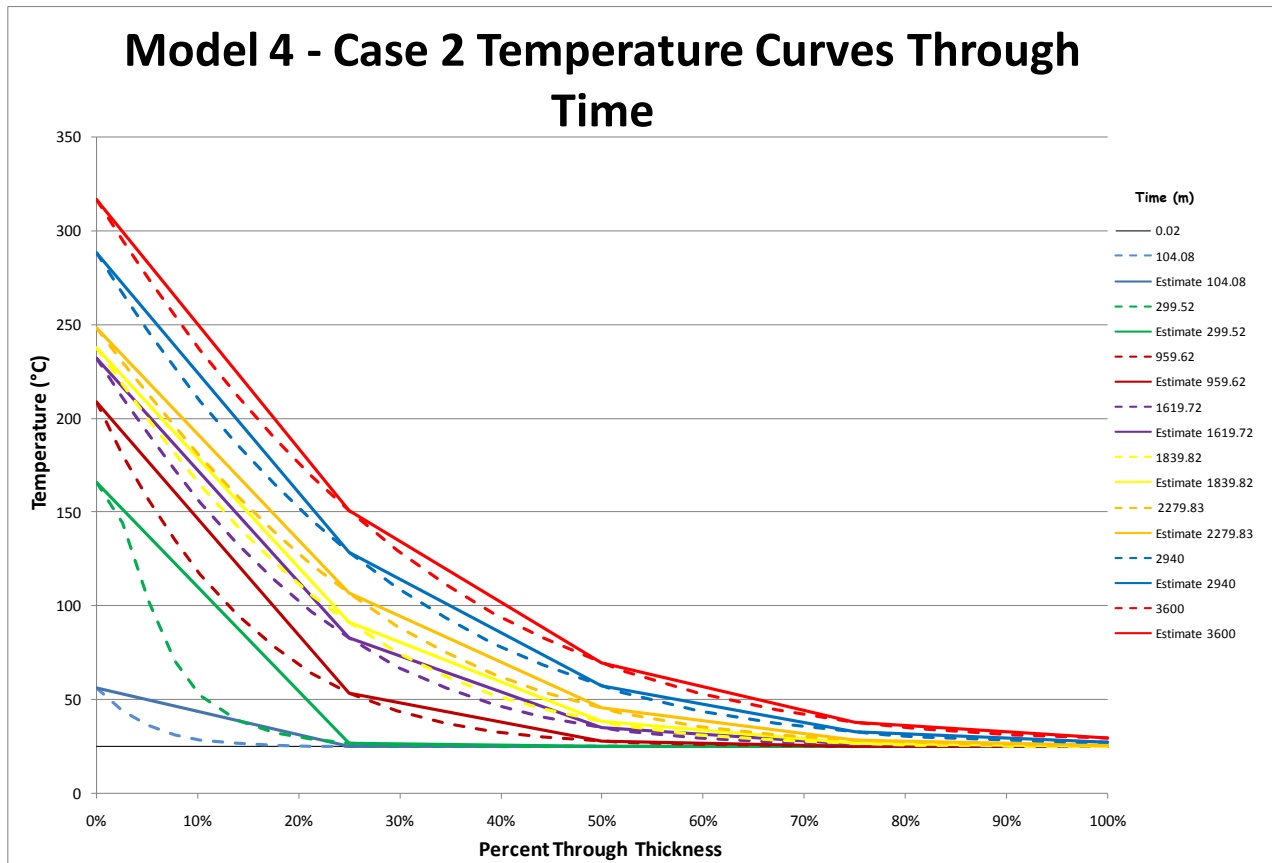




Predefined Temperature Case 2

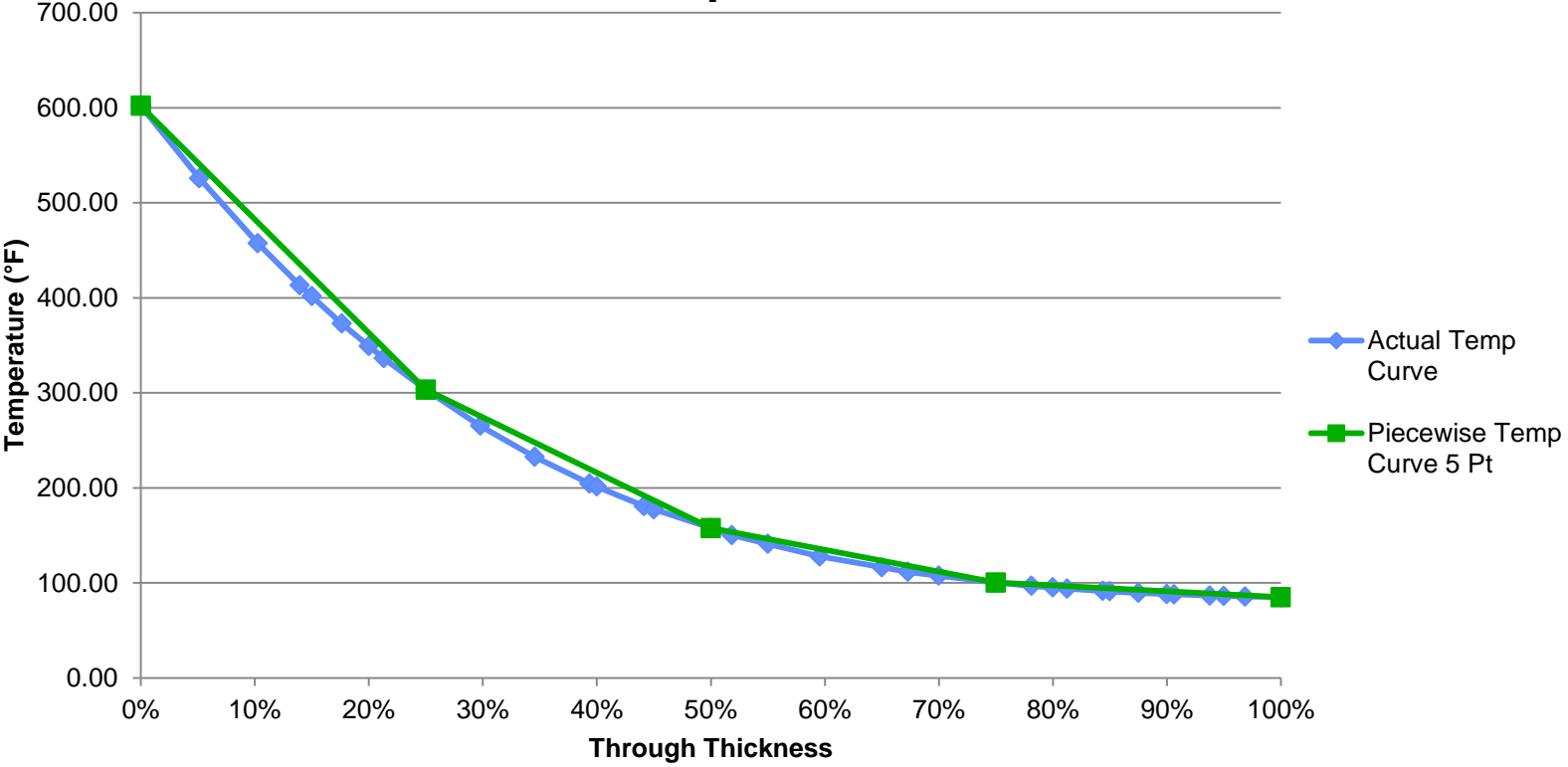
- **Case 2 involves a curved temperature distribution, due to high temperatures which exist for short time durations**
- **ABAQUS only handles applied temperature gradients piecewise-linearly using temperature points equally spaced through the thickness**
- **Five temperature points were applied, following the number of integration points in the shell elements**
- **Several methods attempted to find best way to simulate the temperature gradient along with pressure**
 1. **Piecewise linear with temperature curves corresponding to pressure time steps**
 2. **Piecewise linear with one temperature curve that ramps linearly up to target value at $3.6xP_d$**

Case 2 - Method 1



Case 2 - Method 2

Model 4 Case 2 Temperature Curves at 3.6xPd





Results from Methods Attempted

- **Method 1 was only able to converge to 1.72 x Pd**
- **Method 2 ramped up temperature curve corresponding to the pressure of 3.6, which occurs at time = 3600 minutes in one step, where the solution converged to 3.6 x Pd**



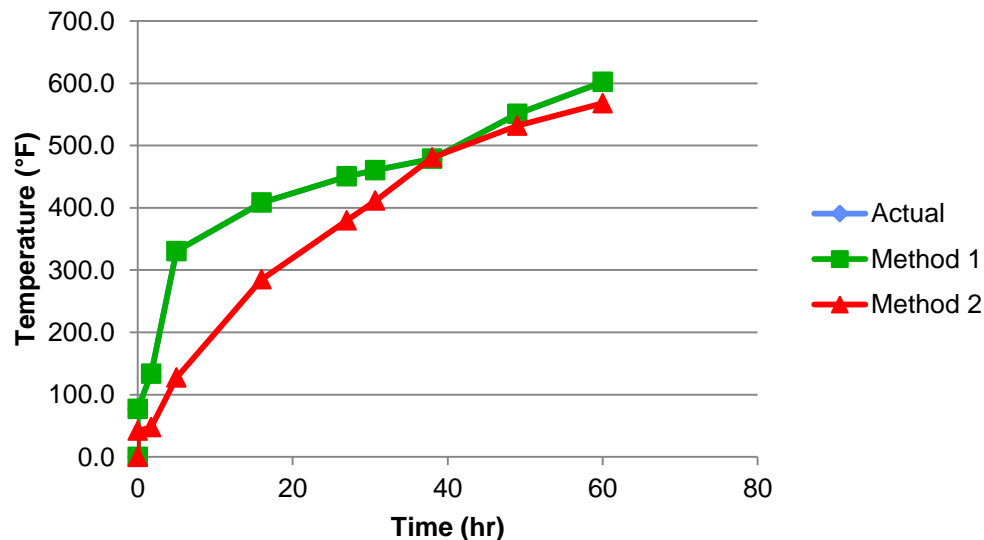


Case 2 Temperature Application

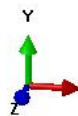
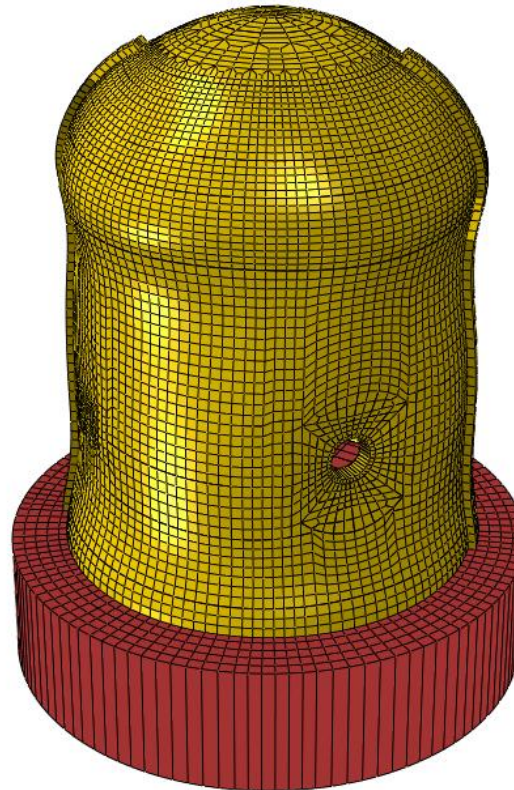
- **In summary, the final solution strategy successfully executed is as follows:**
 - **Solution Step 1: Apply Dead Load**
 - **Solution Step 2: Apply Prestress**
 - **Solution Step 3: Apply Anchor-Set**
 - **Solution Step 4: Apply Pressure and Temperature incrementally**
- **Each step has many load increments and equilibrium iterations; the load incrementation within a step is selected by ABAQUS; cut-backs occur automatically**

Comparison Between Methods

- Graph represents temperature applied to the inside face of the vessel through time
- Method 1 is exactly in line with data through pressure incrementation
- Method 2 matches temperature at final pressure milestone
- Sensitivity studies were performed to compare responses of Method 1 to Method 2 out to P=1.7 Pd; behaviors reasonably close



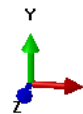
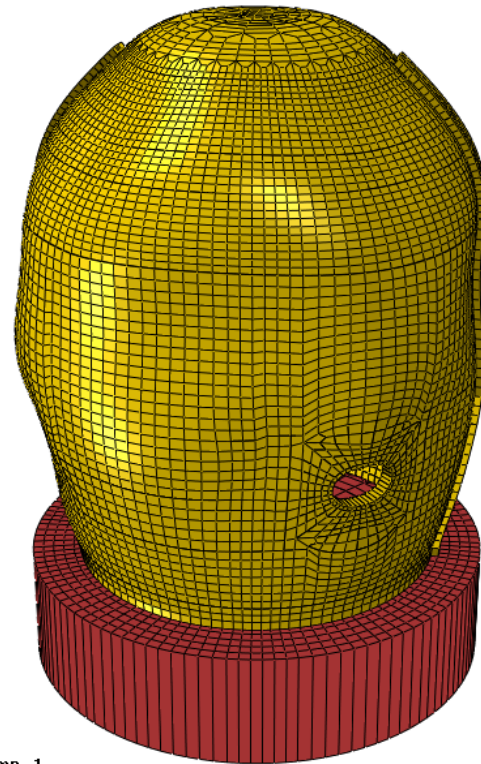
Case 2 Deformed Shape after Tendon Anchorage. Deformation Scale x 500



Step: Anchor
Increment 33: Step Time = 1.000
Deformed Var: U Deformation Scale Factor: +5.000e+02



Case 2 Deformed Shape at 3.6 x Pd. Deformation Scale x 20



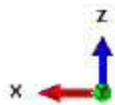
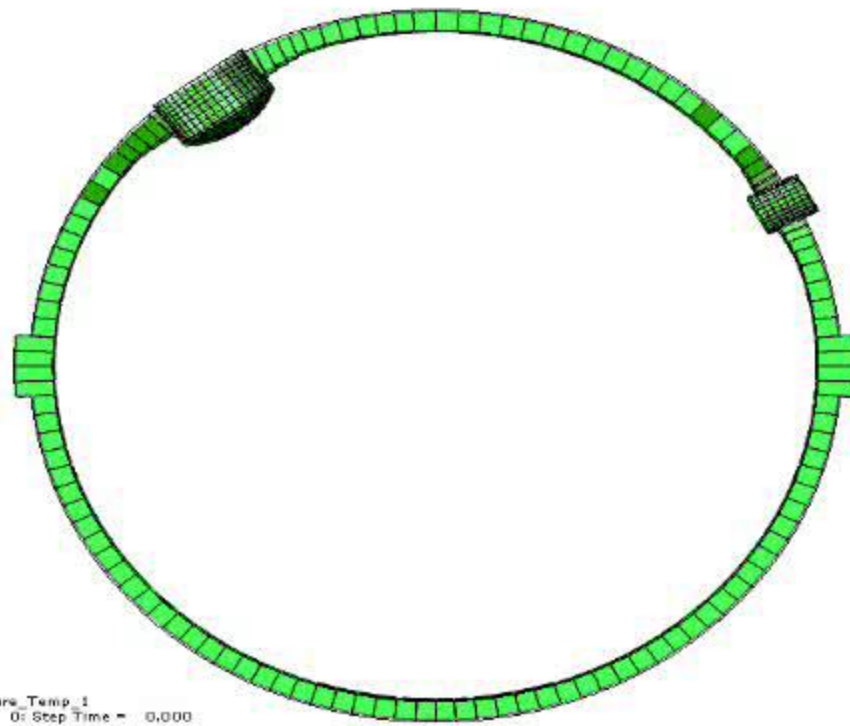
Step: Pressure_Temp_1
Increment 90: Step Time = 0.9010

Deformed Var: U Deformation Scale Factor: +2.000e+01



Case 2 Animation of a “Plan-View” Slice at a Model Elevation of 4.68m

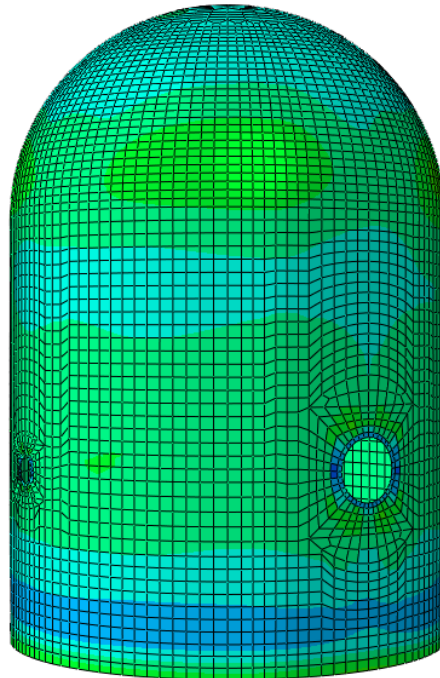
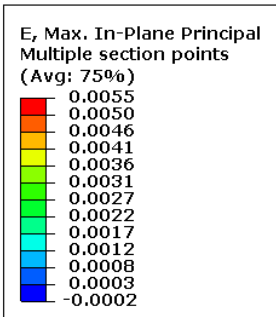
Step: Pressure_Frame: 0
Total Time: 3.000000



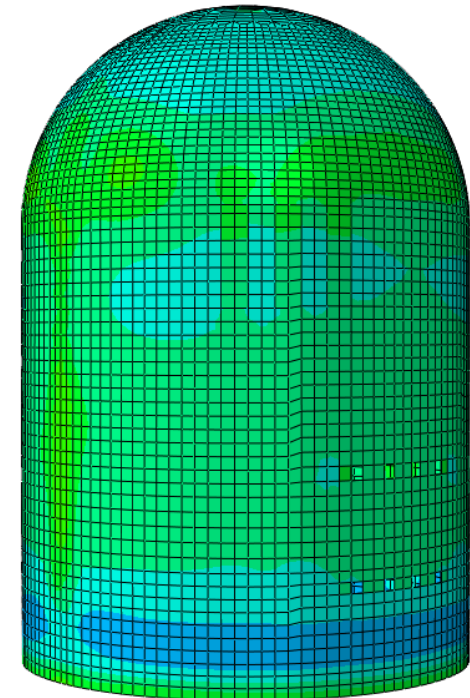
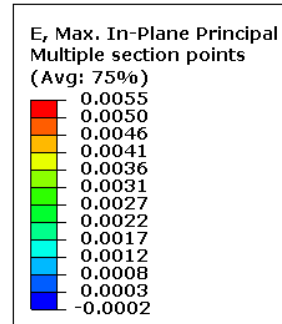
Step: Pressure_Temp_1
Increment: 0; Step Time = 0.000
Deformed Vari U; Deformation Scale Factor: +3.000e+01



Case 2 Max Principal Strain in Liner at 2.0 x Pd

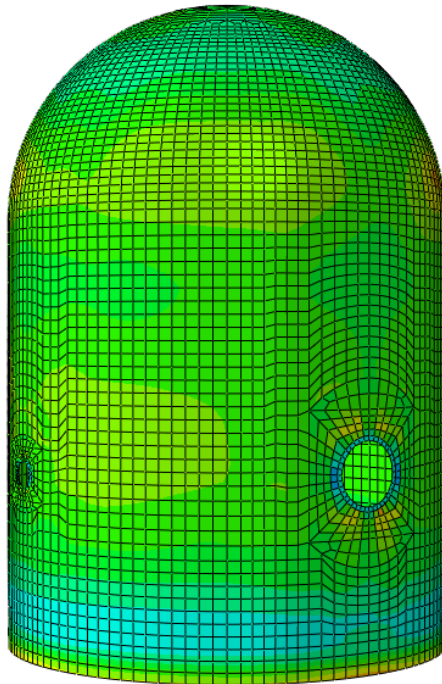
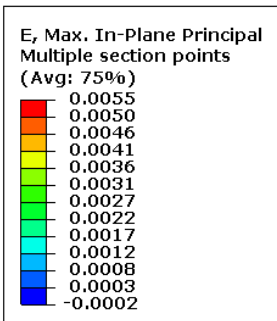


Step: Pressure_Temp_1
Increment 23: Step Time = 0.5063
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

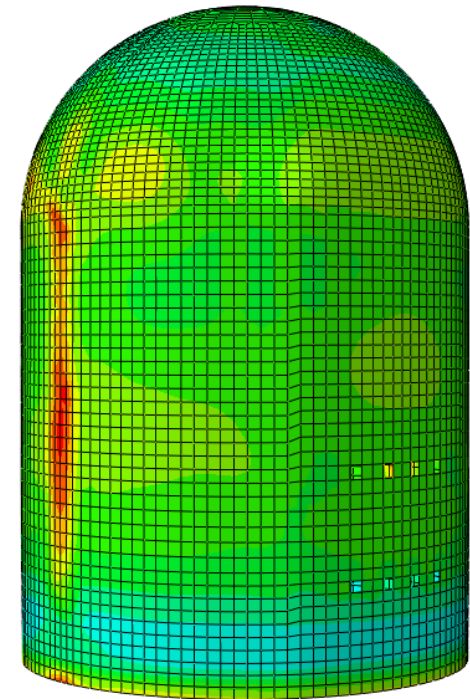
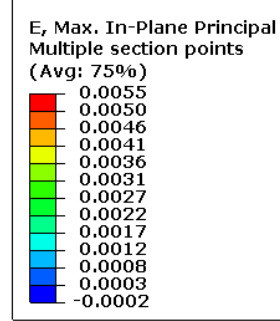


Step: Pressure_Temp_1
Increment 23: Step Time = 0.5063
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Max Principal Strain in Liner at 2.5 x Pd

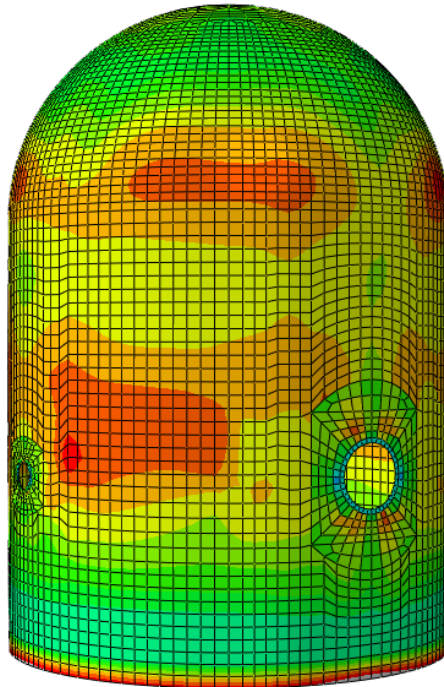
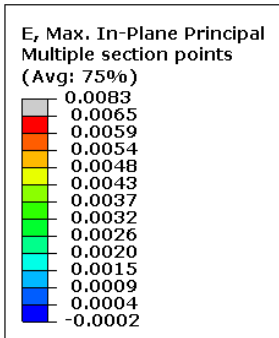


Step: Pressure_Temp_1
Increment 31: Step Time = 0.6239
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

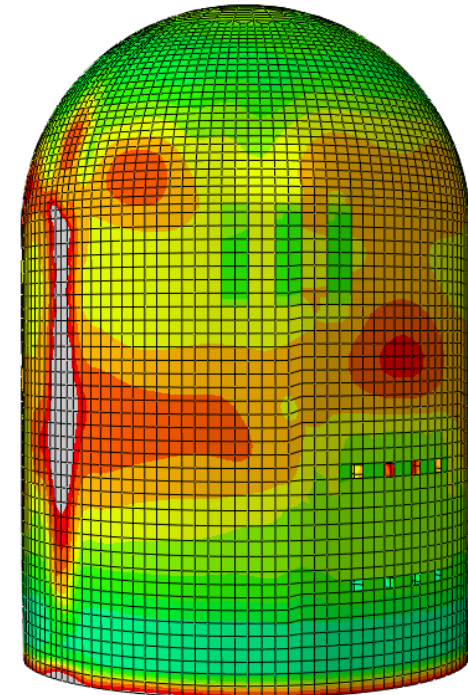
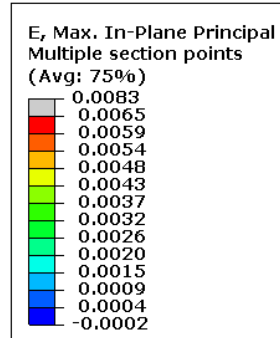


Step: Pressure_Temp_1
Increment 31: Step Time = 0.6239
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Max Principal Strain in Liner at 3.0 x Pd



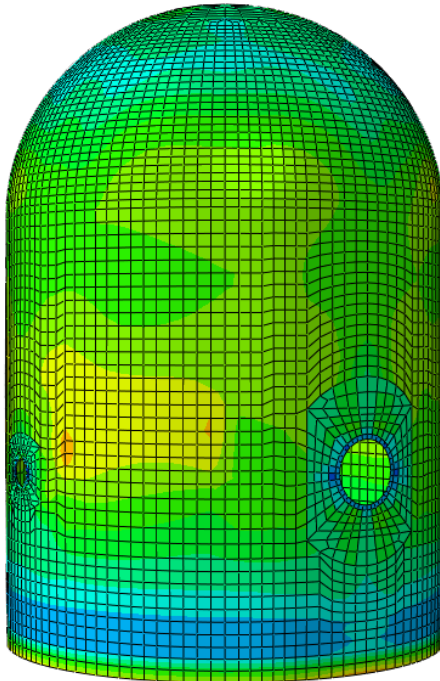
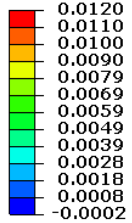
Step: Pressure_Temp_1
Increment 47: Step Time = 0.7550
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00



Step: Pressure_Temp_1
Increment 47: Step Time = 0.7550
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

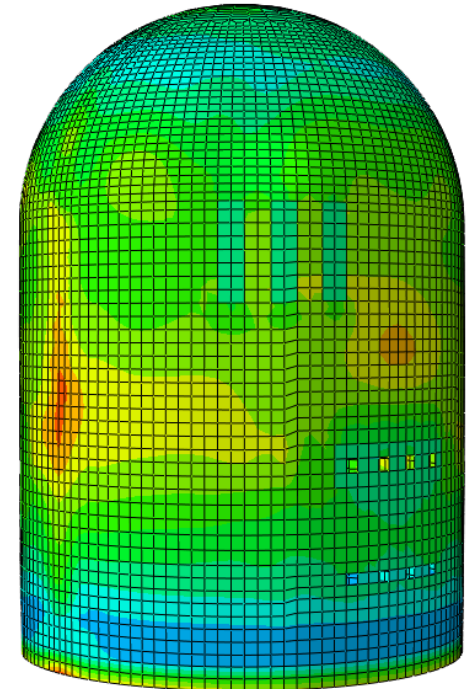
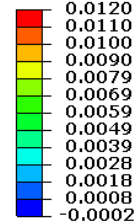
Case 2 Max Principal Strain in Liner at 3.3 x Pd. (Higher Contour Color Limits)

E, Max. In-Plane Principal
Multiple section points
(Avg: 75%)



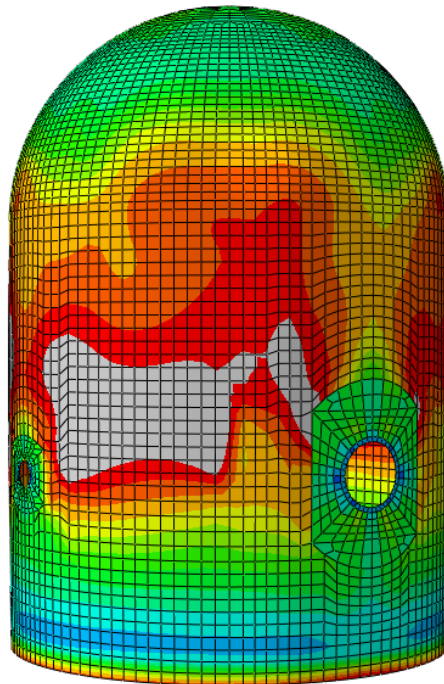
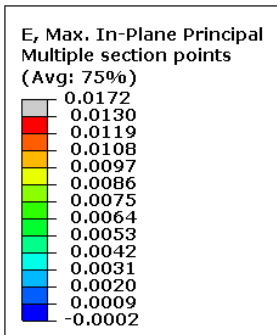
Step: Pressure_Temp_1
Increment 63: Step Time = 0.8254
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

E, Max. In-Plane Principal
Multiple section points
(Avg: 75%)

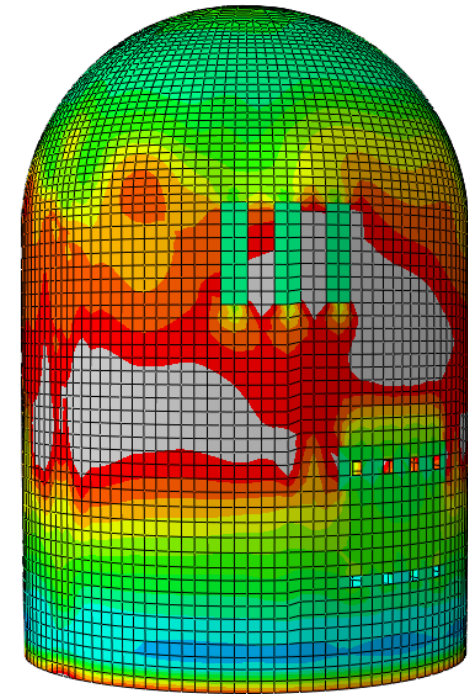
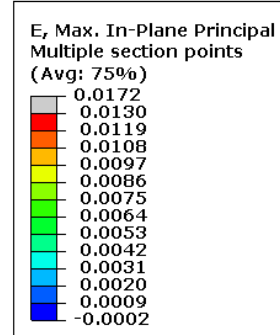


Step: Pressure_Temp_1
Increment 63: Step Time = 0.8254
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Max Principal Strain in Liner at 3.6 x Pd

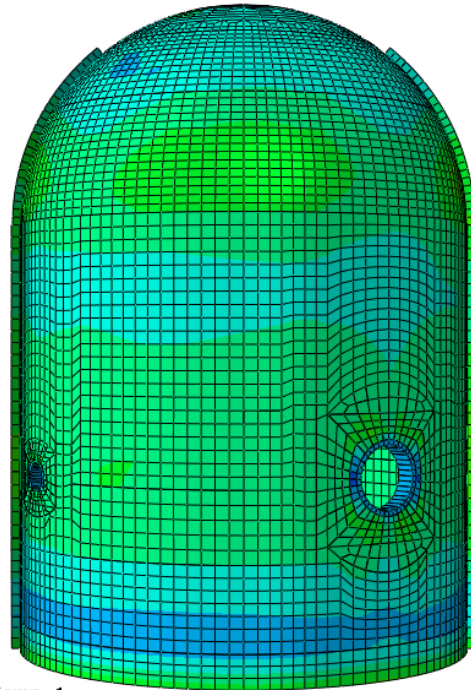
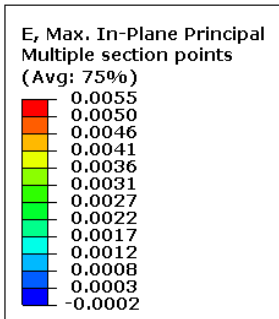


Step: Pressure_Temp_1
Increment 90; Step Time = 0.9010
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

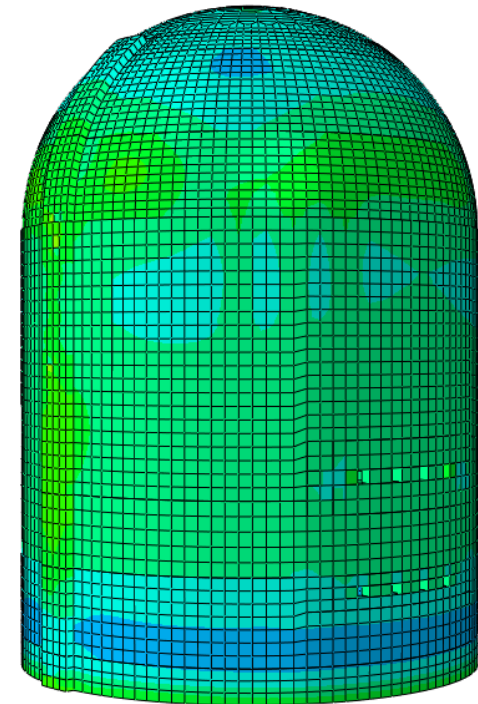
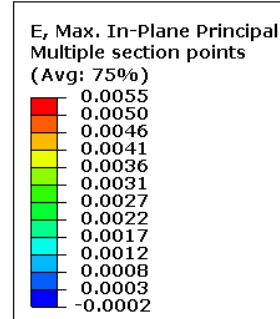


Step: Pressure_Temp_1
Increment 90; Step Time = 0.9010
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Max Principal Membrane Strain in Concrete at 2.0 x Pd

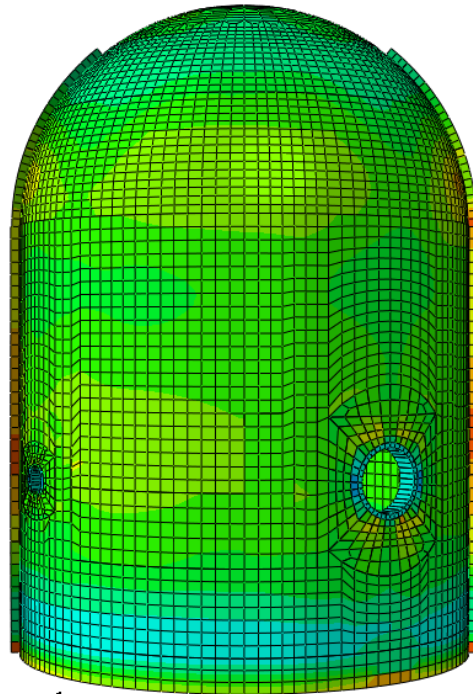
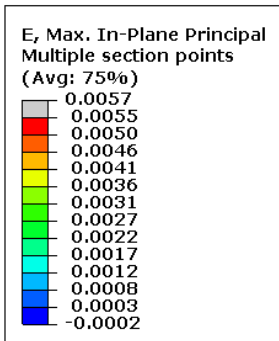


Step: Pressure_Temp_1
Increment 23; Step Time = 0.5063
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

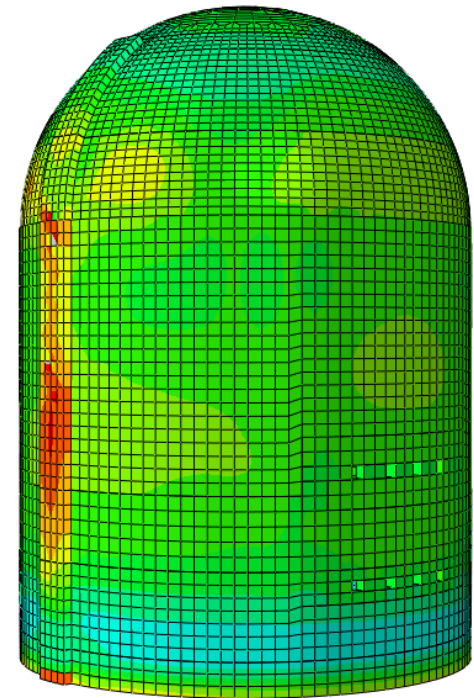
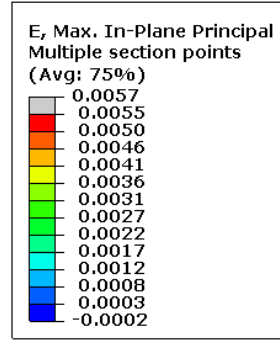


Step: Pressure_Temp_1
Increment 23; Step Time = 0.5063
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Max Principal Membrane Strain in Concrete at 2.5 x Pd

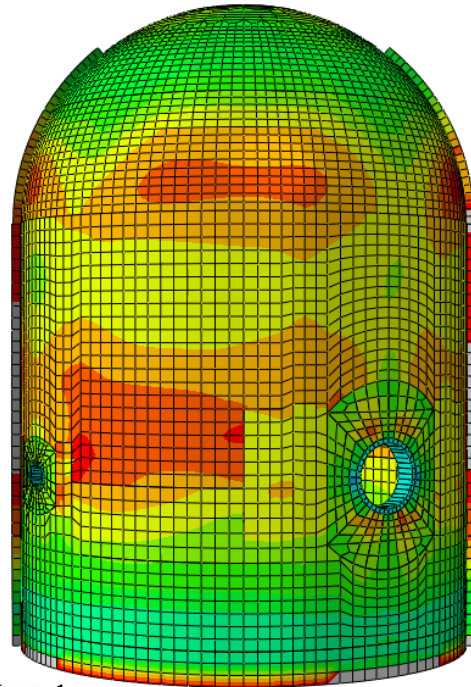
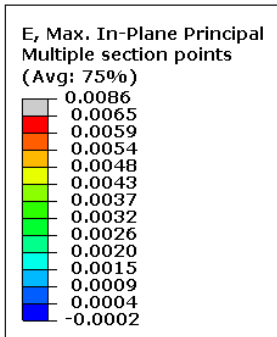


Step: Pressure_Temp_1
Increment 31: Step Time = 0.6239
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

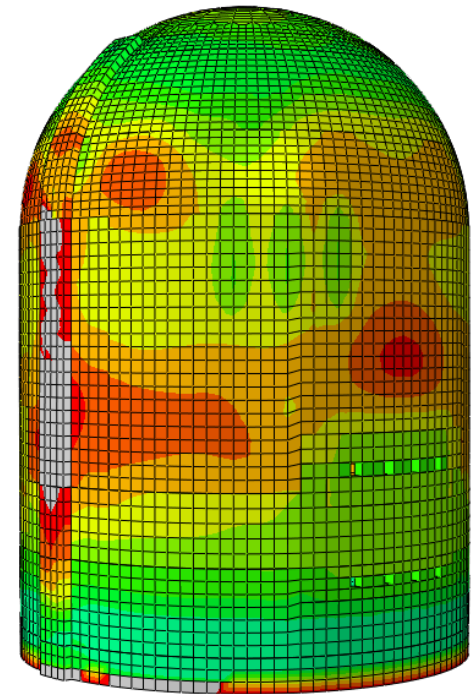
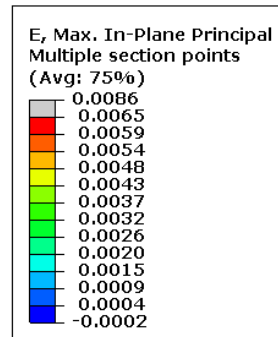


Step: Pressure_Temp_1
Increment 31: Step Time = 0.6239
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Max Principal Membrane Strain in Concrete at 3.0 x Pd



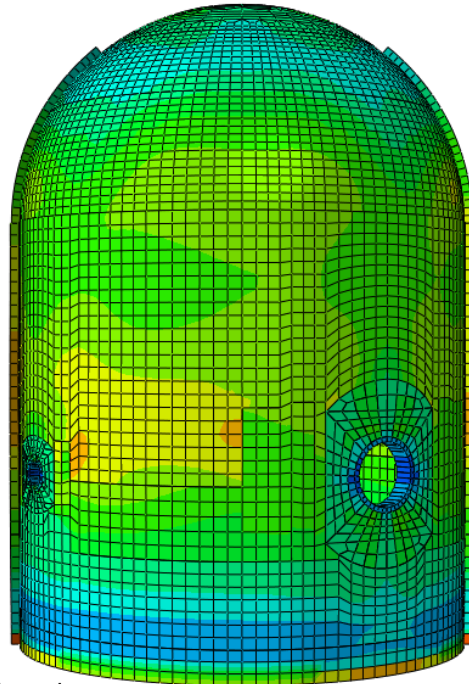
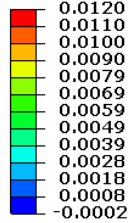
Step: Pressure_Temp_1
Increment 47: Step Time = 0.7550
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00



Step: Pressure_Temp_1
Increment 47: Step Time = 0.7550
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

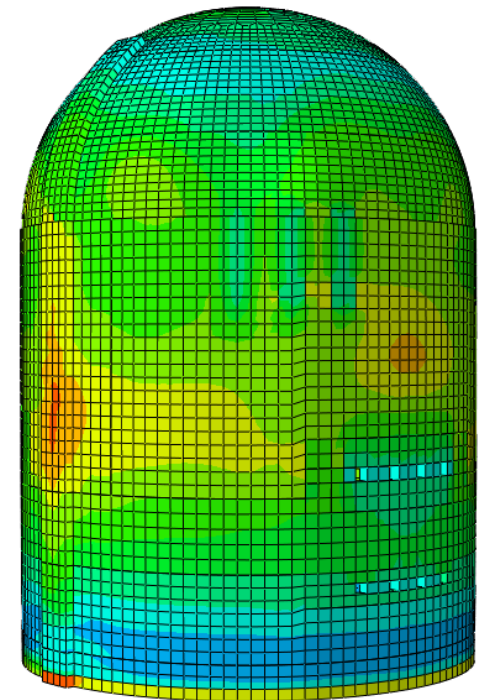
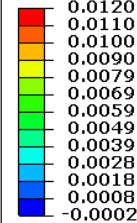
Case 2 Max Principal Membrane Strain in Concrete at 3.3 x Pd

E, Max. In-Plane Principal
Multiple section points
(Avg: 75%)



Step: Pressure_Temp_1
Increment 63; Step Time = 0.8254
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

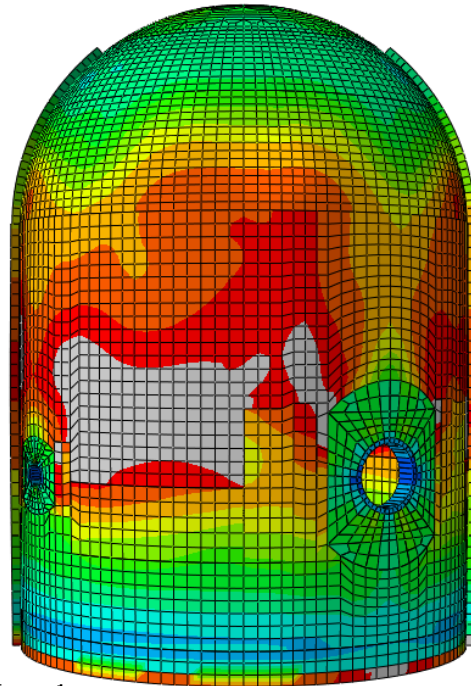
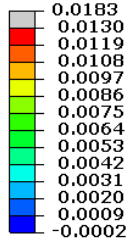
E, Max. In-Plane Principal
Multiple section points
(Avg: 75%)



Step: Pressure_Temp_1
Increment 63; Step Time = 0.8254
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

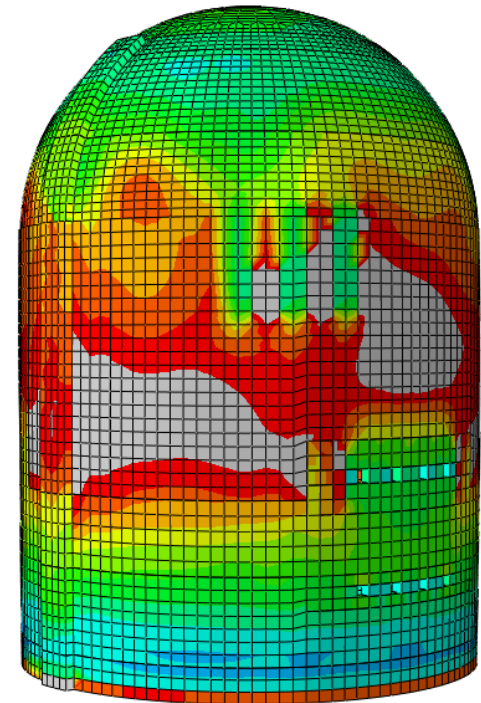
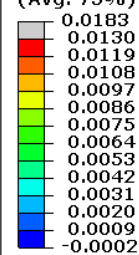
Case 2 Max Principal Membrane Strain in Concrete at 3.6 x Pd

E, Max. In-Plane Principal
Multiple section points
(Avg: 75%)



Step: Pressure_Temp_1
Increment 90: Step Time = 0.9010
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

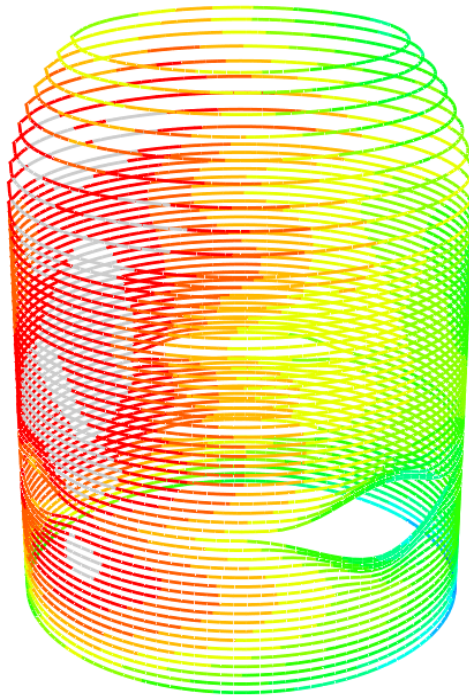
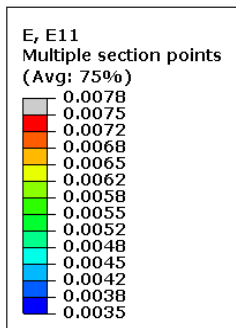
E, Max. In-Plane Principal
Multiple section points
(Avg: 75%)



Step: Pressure_Temp_1
Increment 90: Step Time = 0.9010
Primary Var: E, Max. In-Plane Principal
Deformed Var: U Deformation Scale Factor: +1.0000e+00

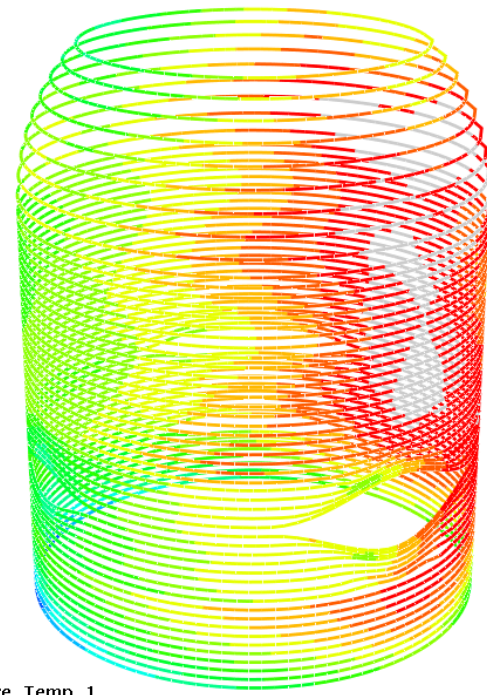
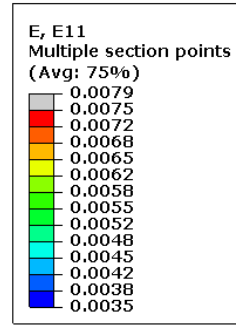
Case 2 Strain in Hoop Tendons

Anchored at 90° at 2.0 x Pd



Y
Z
Step: Pressure_Temp_1
Increment 23: Step Time = 0.5063
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

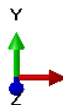
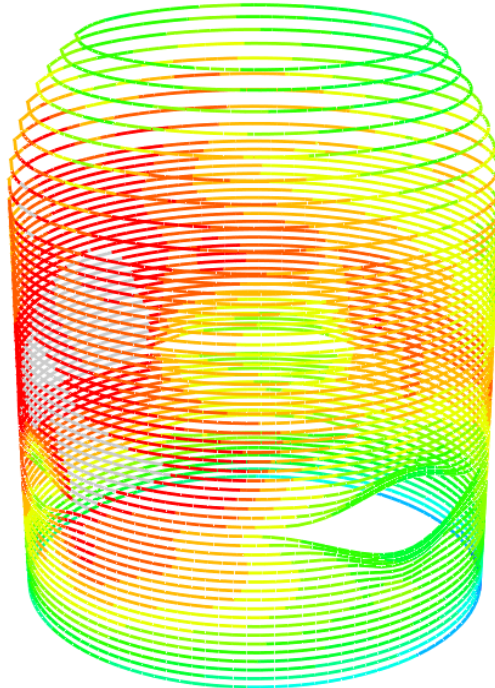
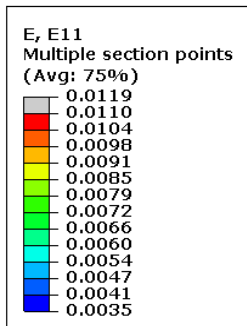
Anchored at 270° at 2.0 x Pd



Y
Z
Step: Pressure_Temp_1
Increment 23: Step Time = 0.5063
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

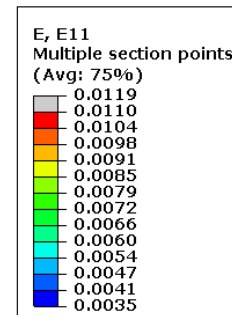
Case 2 Strain in Hoop Tendons

Anchored at 90° at 3.0 x Pd



Step: Pressure_Temp_1
Increment 47: Step Time = 0.7550
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

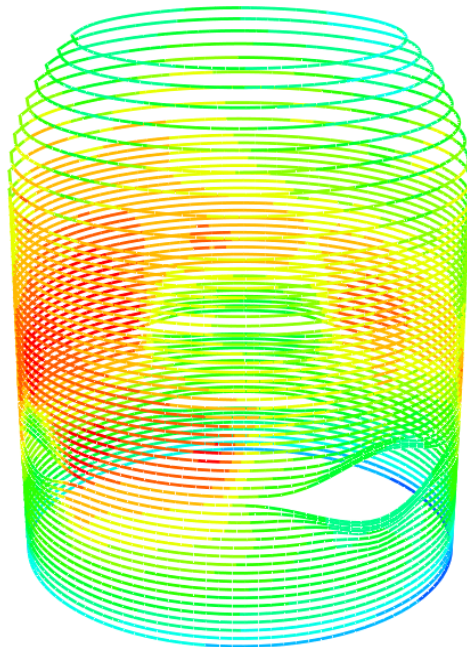
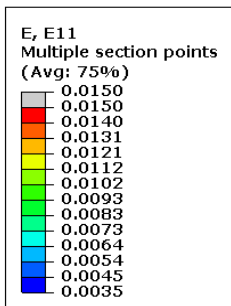
Anchored at 270° at 3.0 x Pd



Step: Pressure_Temp_1
Increment 47: Step Time = 0.7550
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

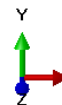
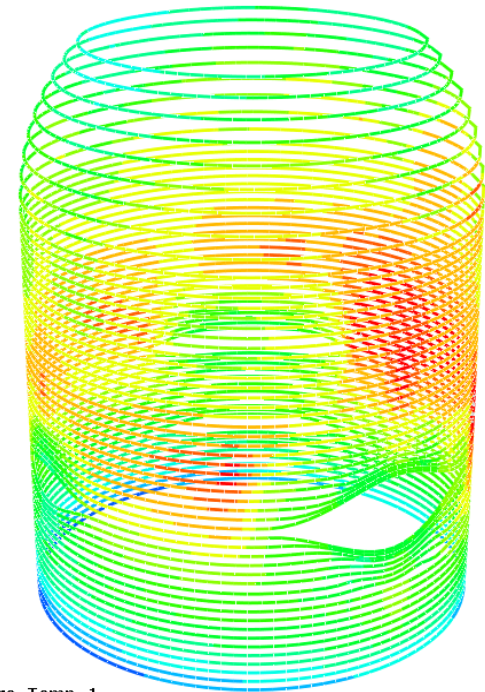
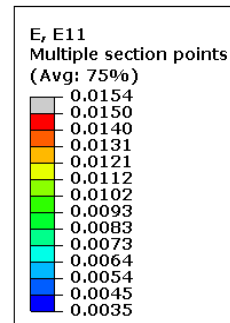
Case 2 Strain in Hoop Tendons

Anchored at 90° at 3.3 x Pd



Step: Pressure_Temp_1
Increment 63: Step Time = 0.8254
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

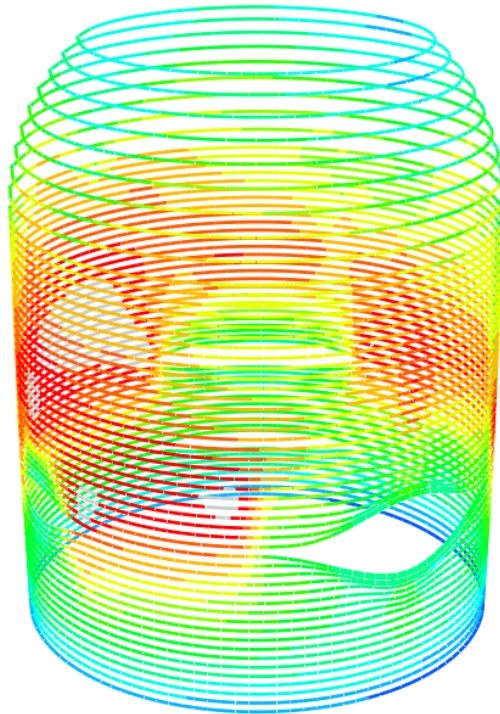
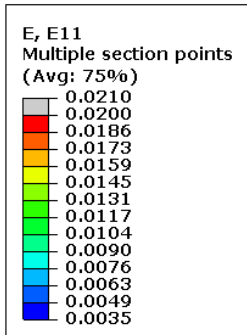
Anchored at 270° at 3.3 x Pd



Step: Pressure_Temp_1
Increment 63: Step Time = 0.8254
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

Case 2 Strain in Hoop Tendons

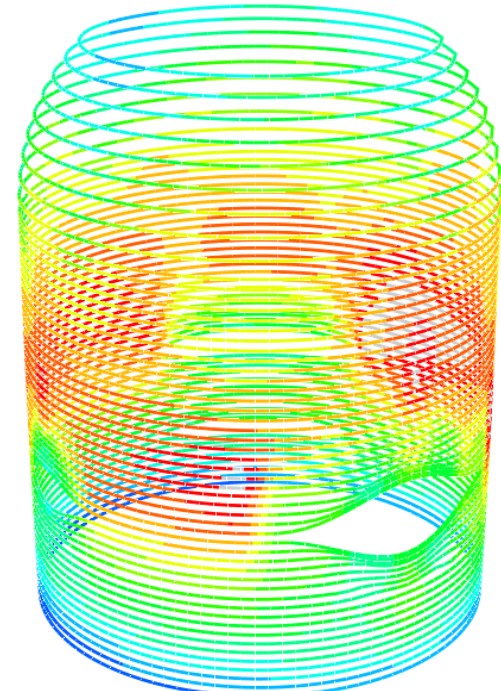
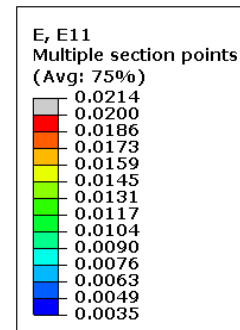
Anchored at 90° at 3.6 x Pd



Y
X
Z

Step: Pressure_Temp_1
Increment 90: Step Time = 0.9010
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

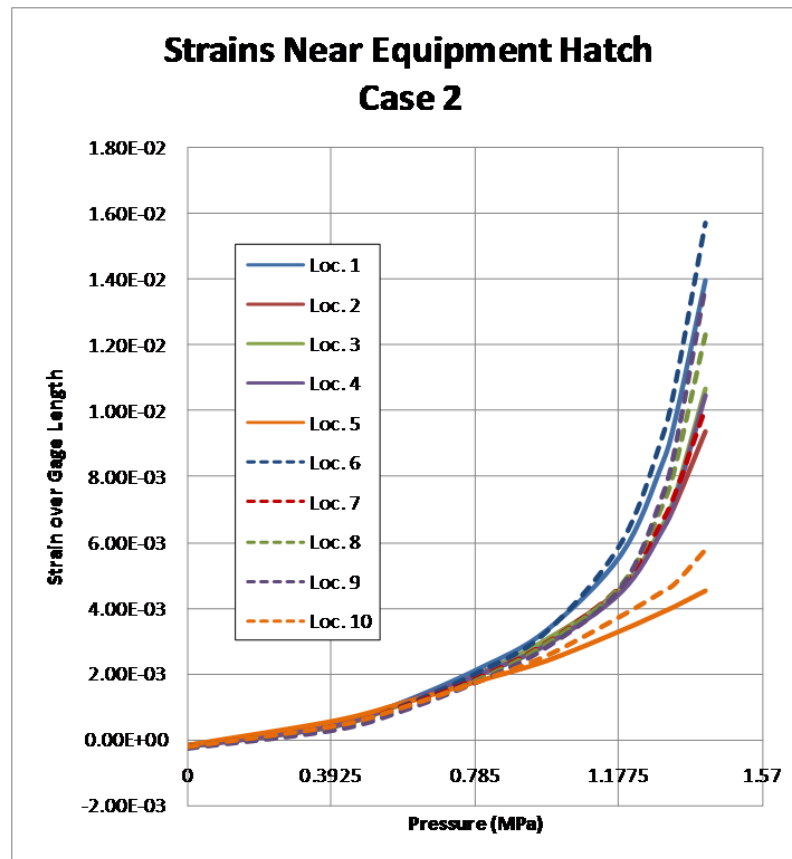
Anchored at 270° at 3.6 x Pd



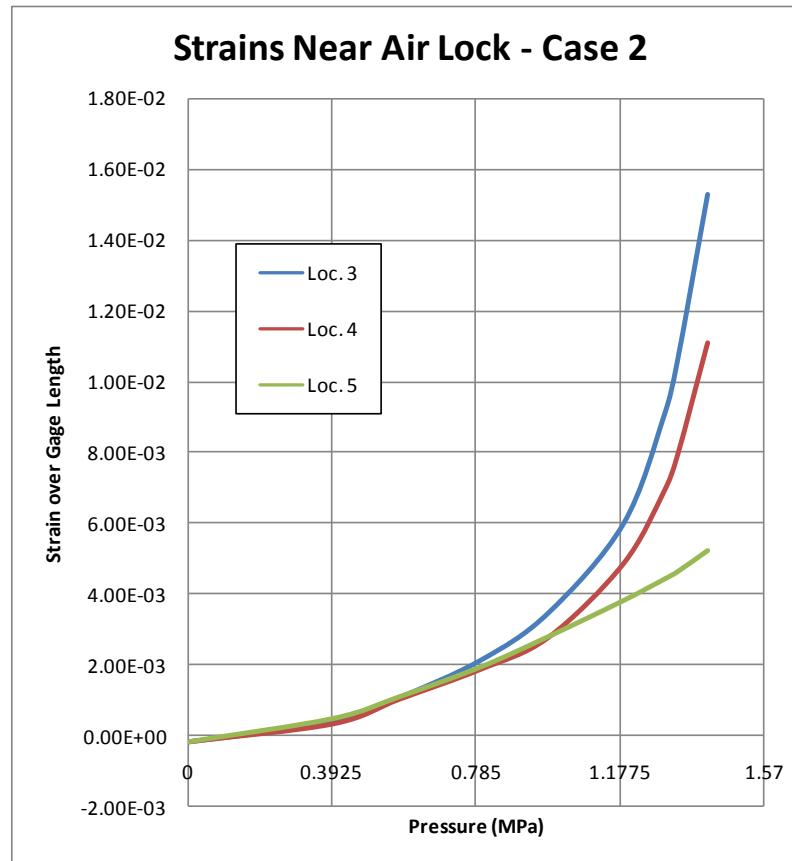
Y
X
Z

Step: Pressure_Temp_1
Increment 90: Step Time = 0.9010
Primary Var: E, E11
Deformed Var: U Deformation Scale Factor: +1.0000e+00

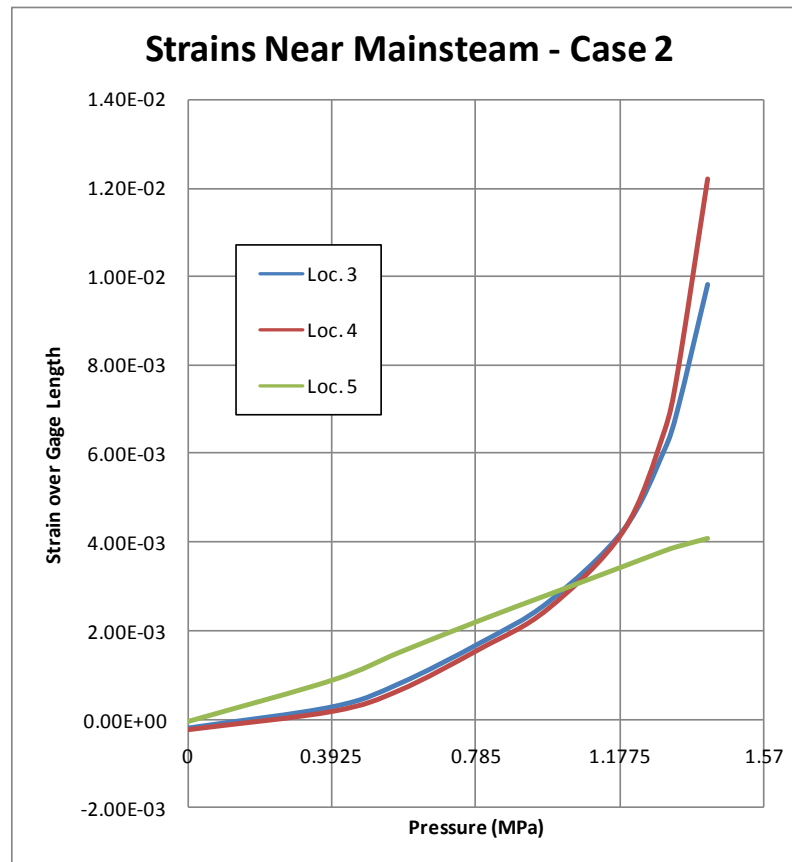
Case 2 Strains over Selected Gage Length Near E/H



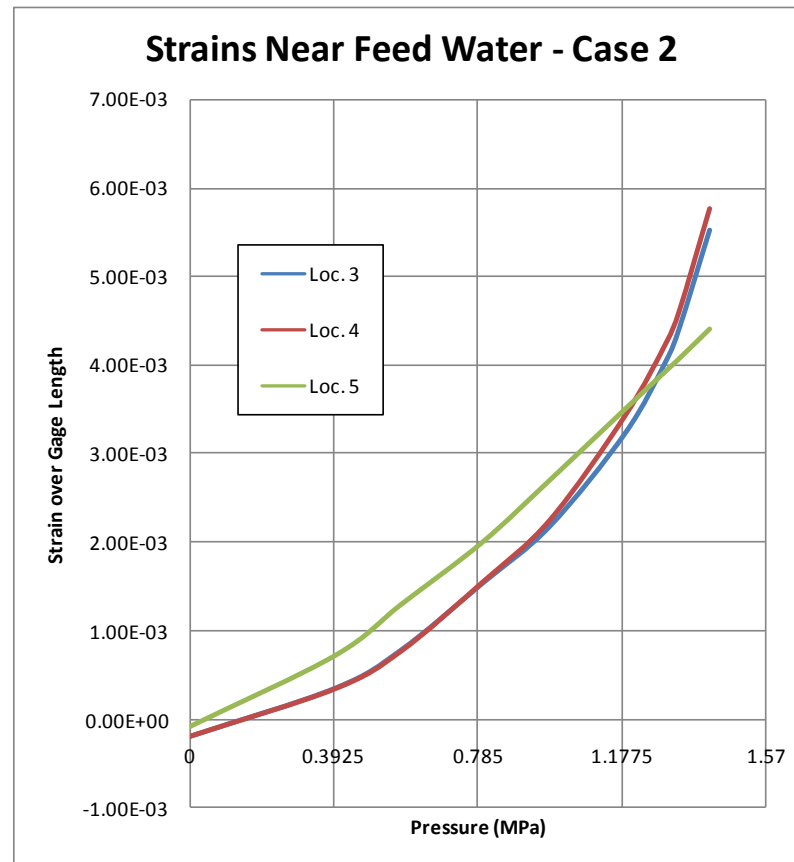
Case 2 Strains over Selected Gage Length Near A/L



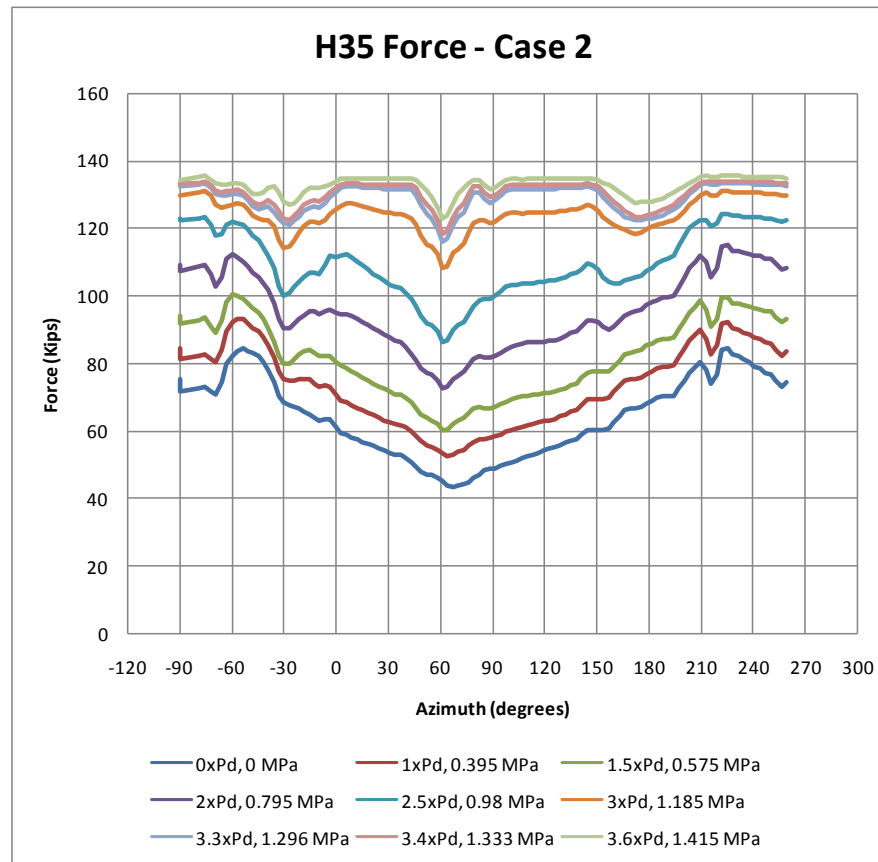
Case 2 Strains over Selected Gage Length Near M/S



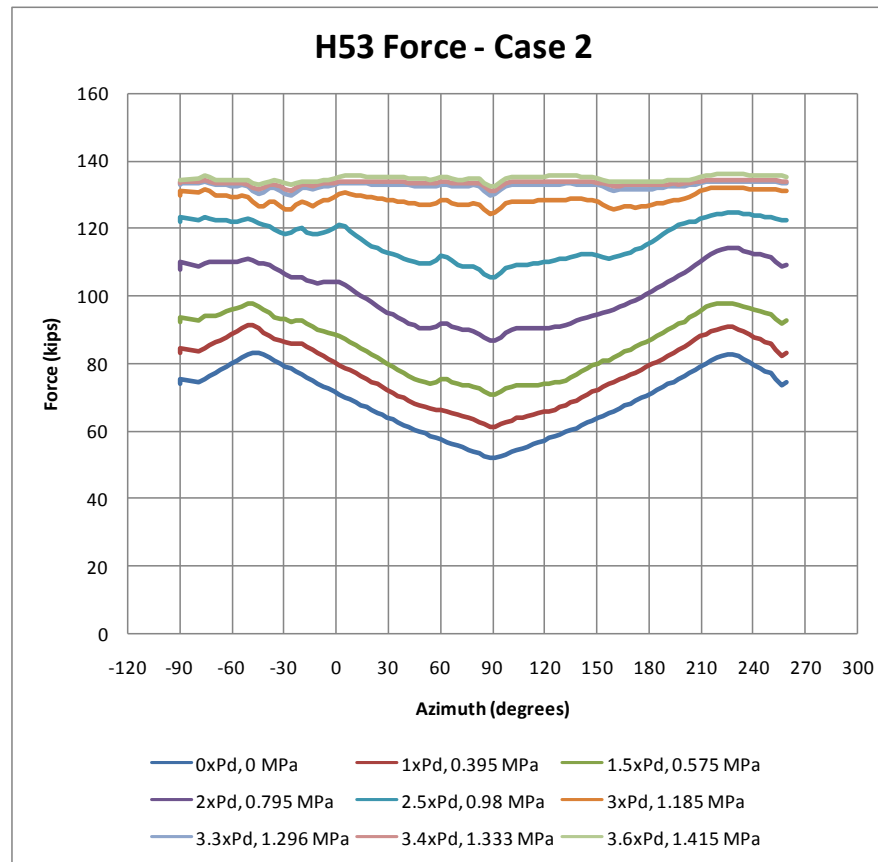
Case 2 Strains over Selected Gage Length Near F/W



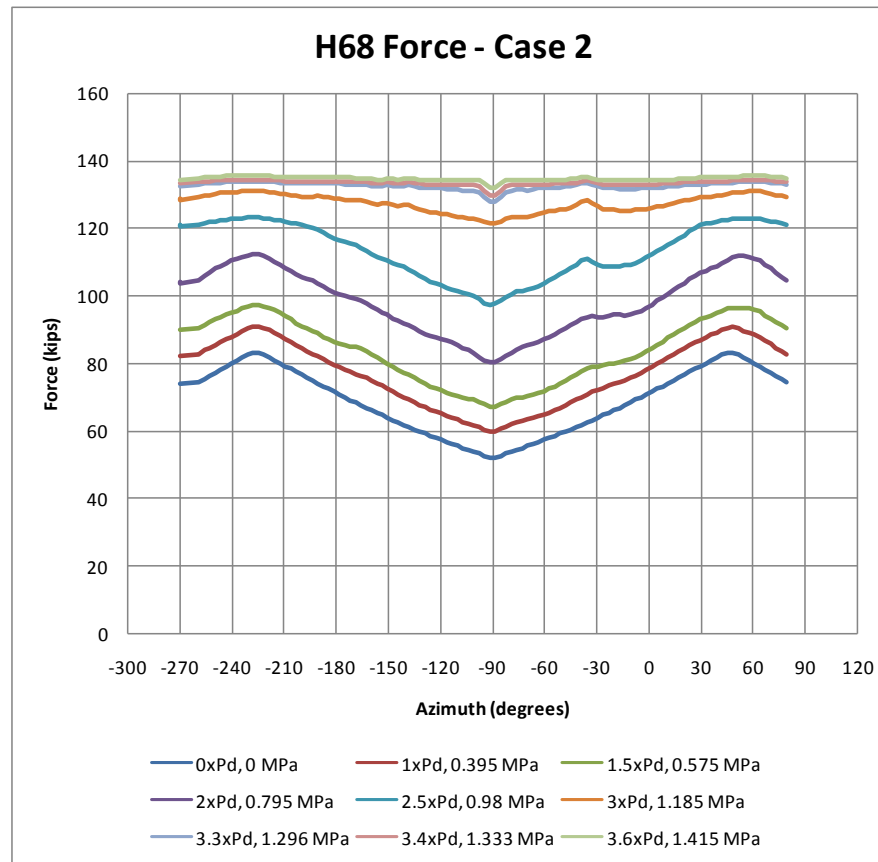
Case 2 Abaqus Analysis – Hoop Tendon H35 Force



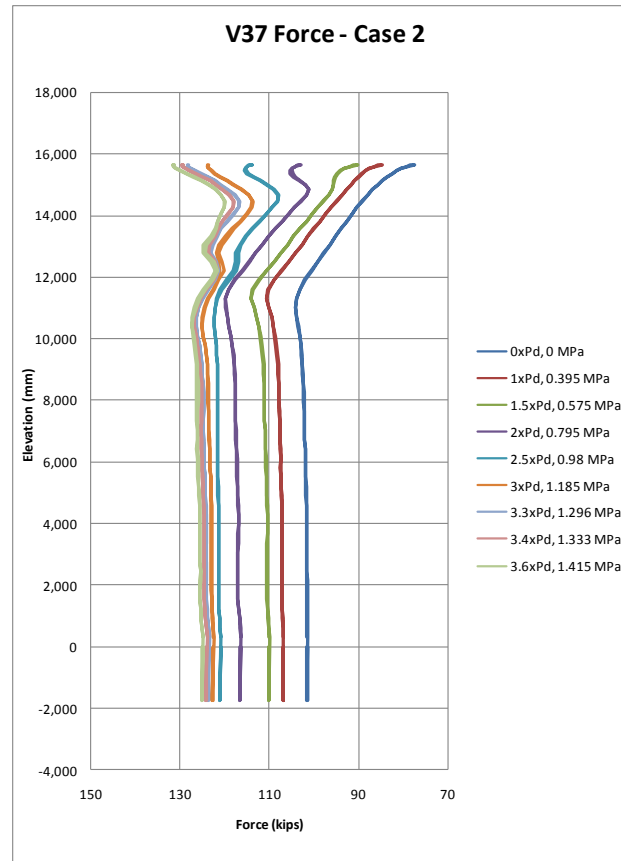
Case 2 Abaqus Analysis – Hoop Tendon H53 Force



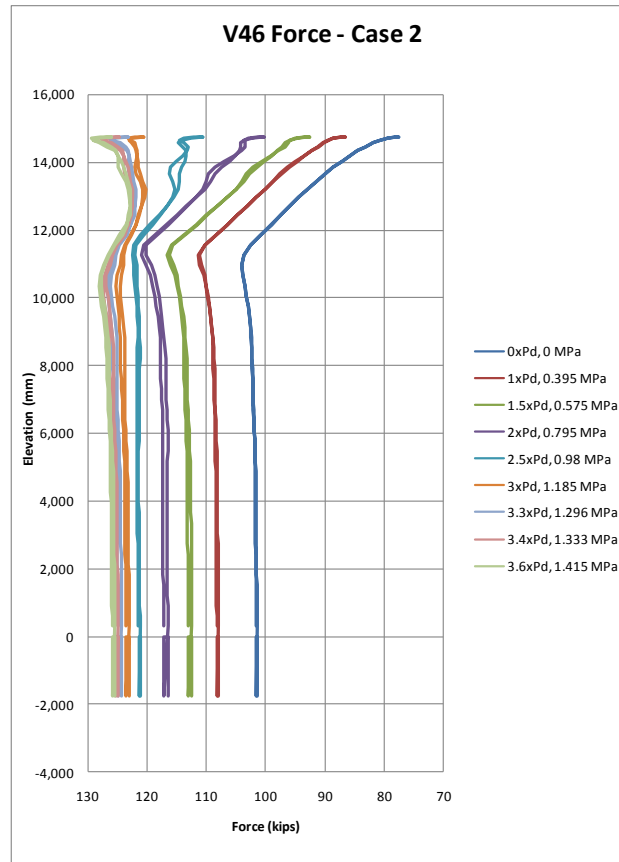
Case 2 Abaqus Analysis – Hoop Tendon H68 Force



Case 2 Abaqus Analysis – Hairpin Tendon V37 Force

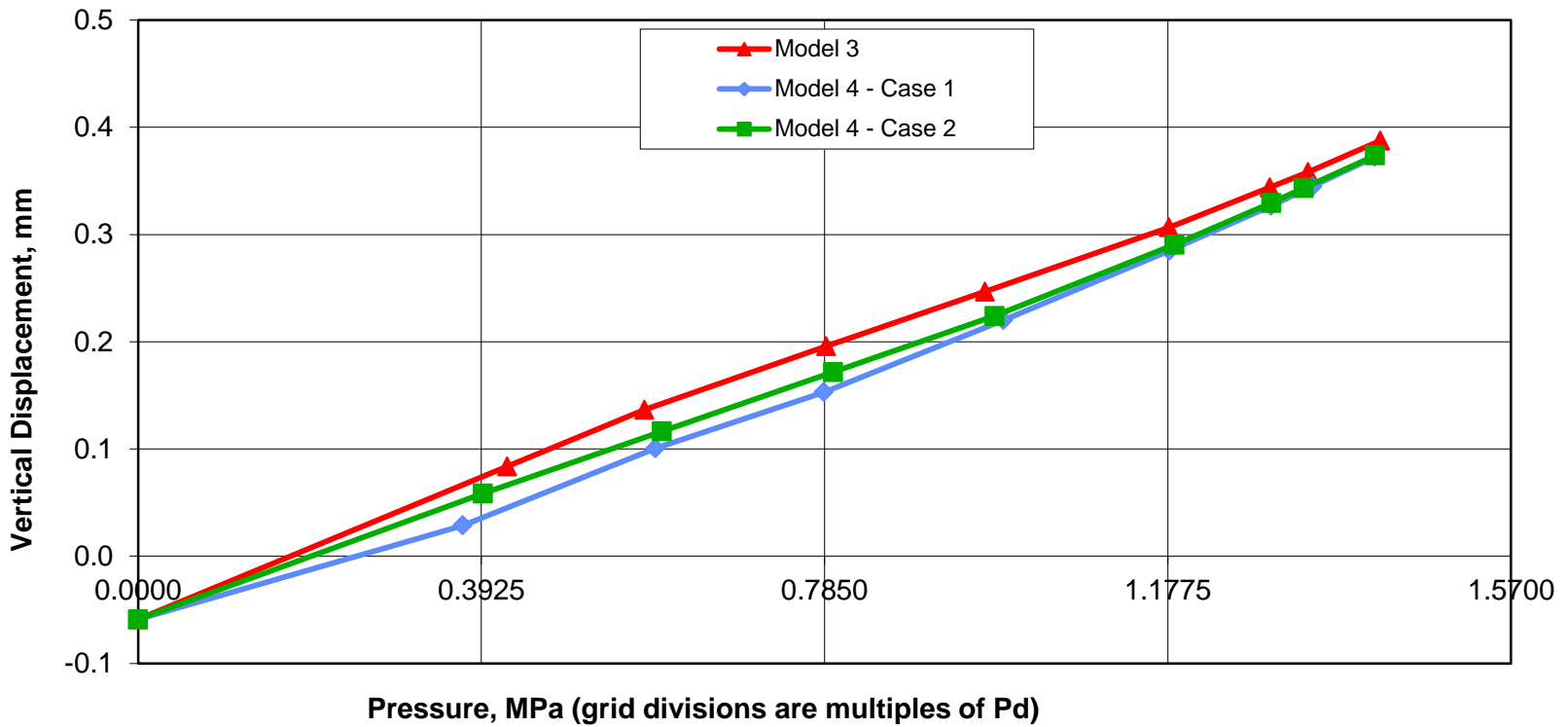


Case 2 Abaqus Analysis – Hairpin Tendon V46 Force



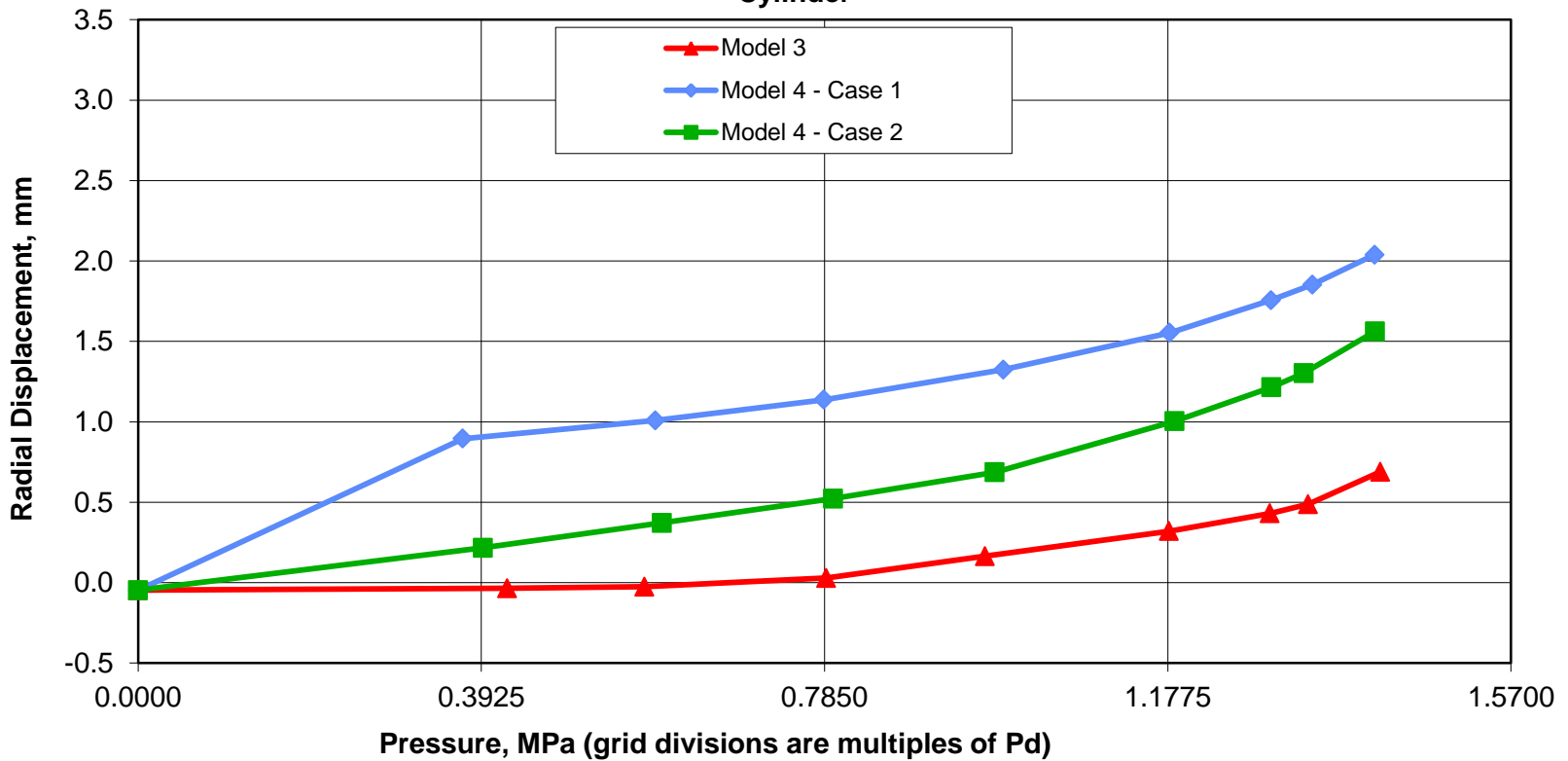


Standard Output Location #1. Azimuth: 135 Degrees, Elevation: 0.00 Meters, Top of Basemat



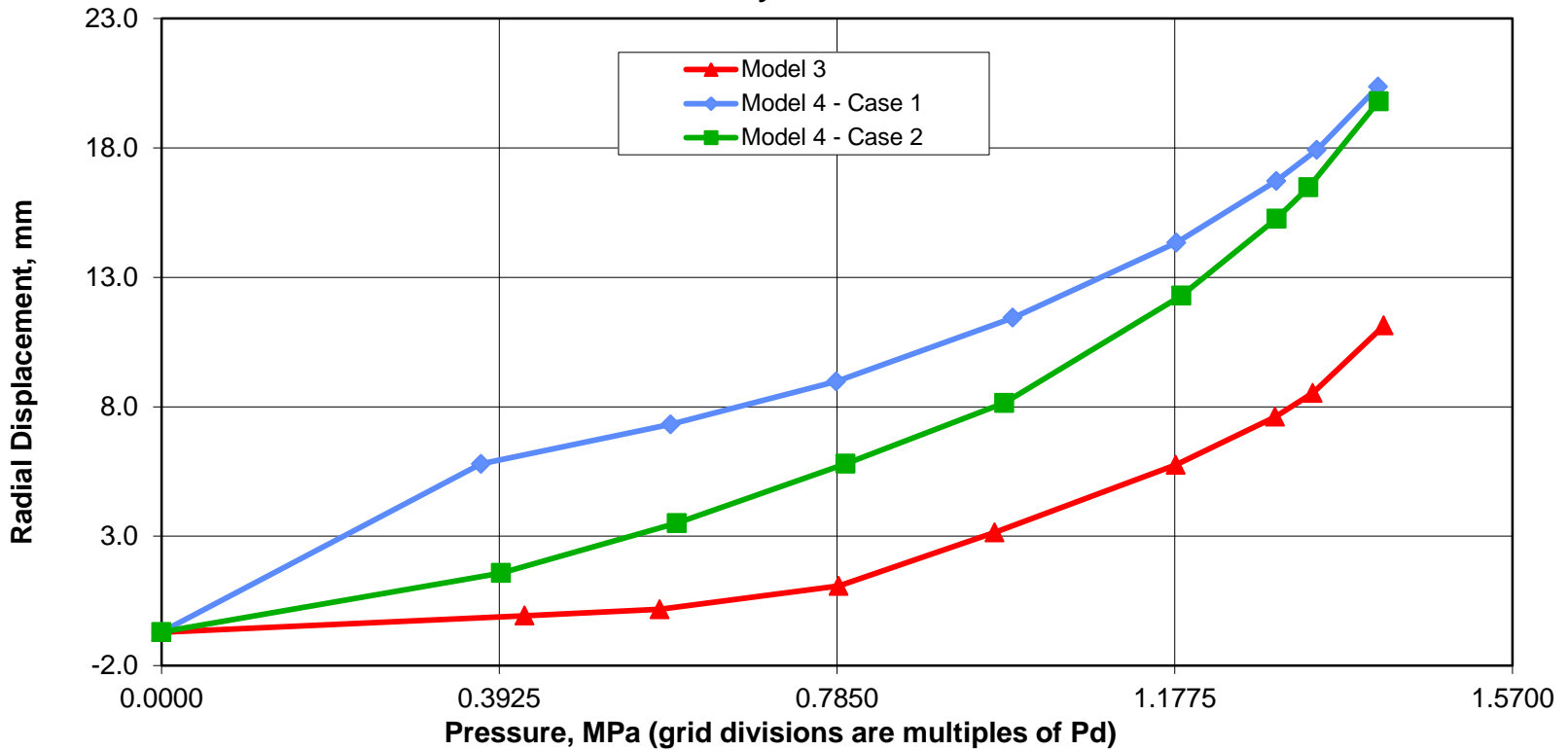


Standard Output Location #2. Azimuth: 135 Degrees, Elevation: 0.25 Meters, Base of Cylinder



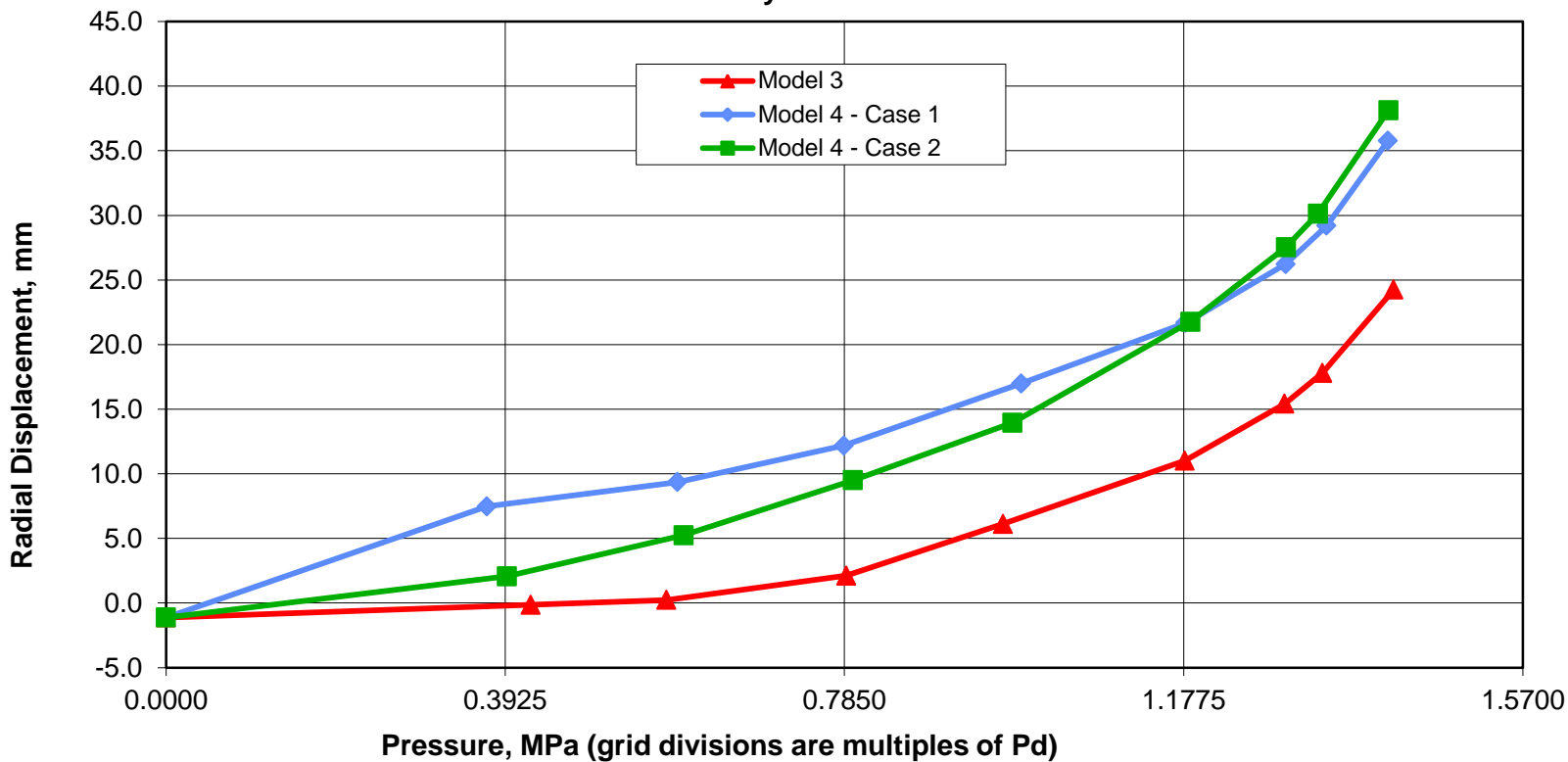


Standard Output Location #3. Azimuth: 135 Degrees, Elevation: 1.43 Meters, Base of Cylinder



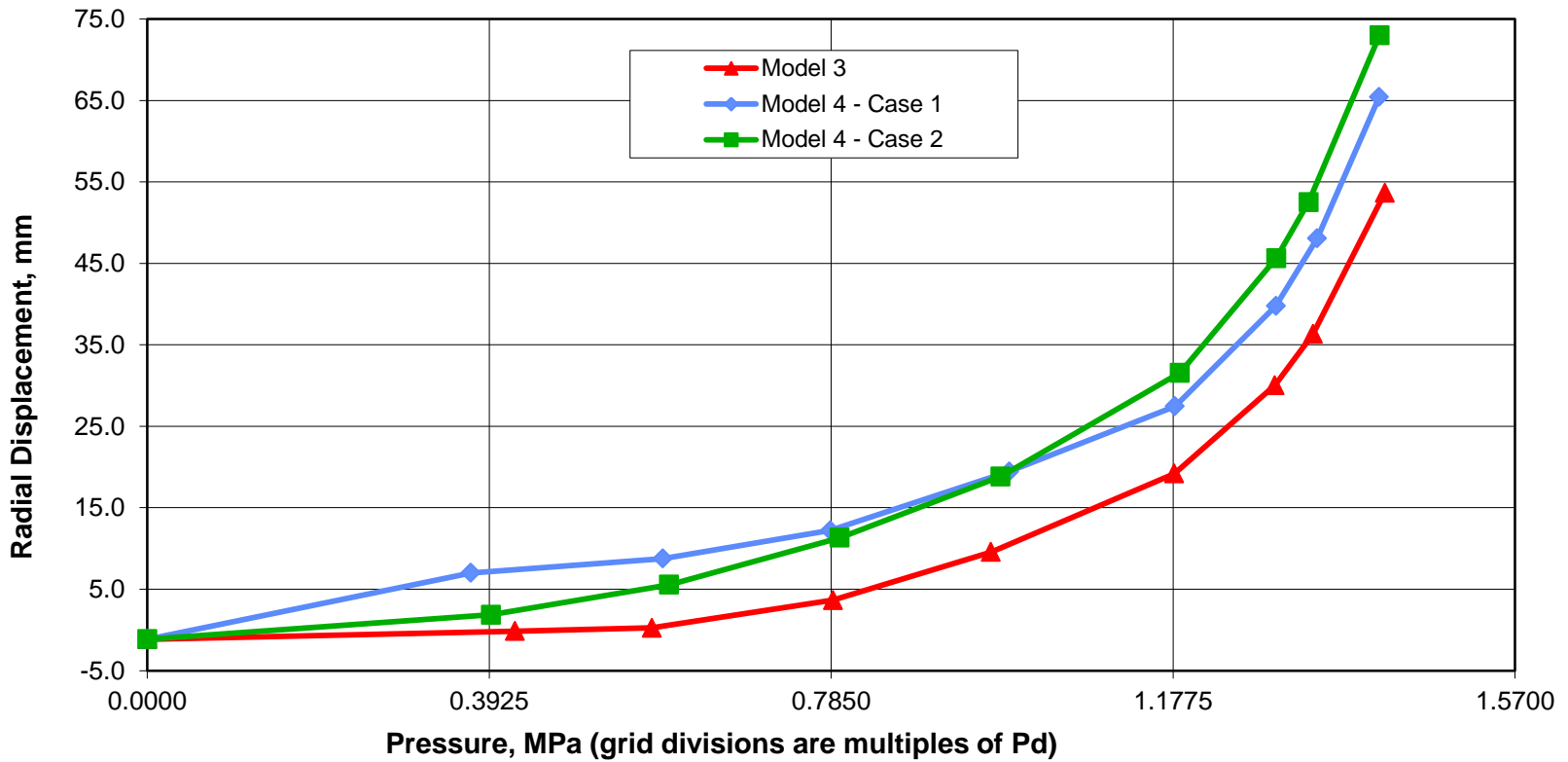


Standard Output Location #4. Azimuth: 135 Degrees, Elevation: 2.63 Meters, Base of Cylinder



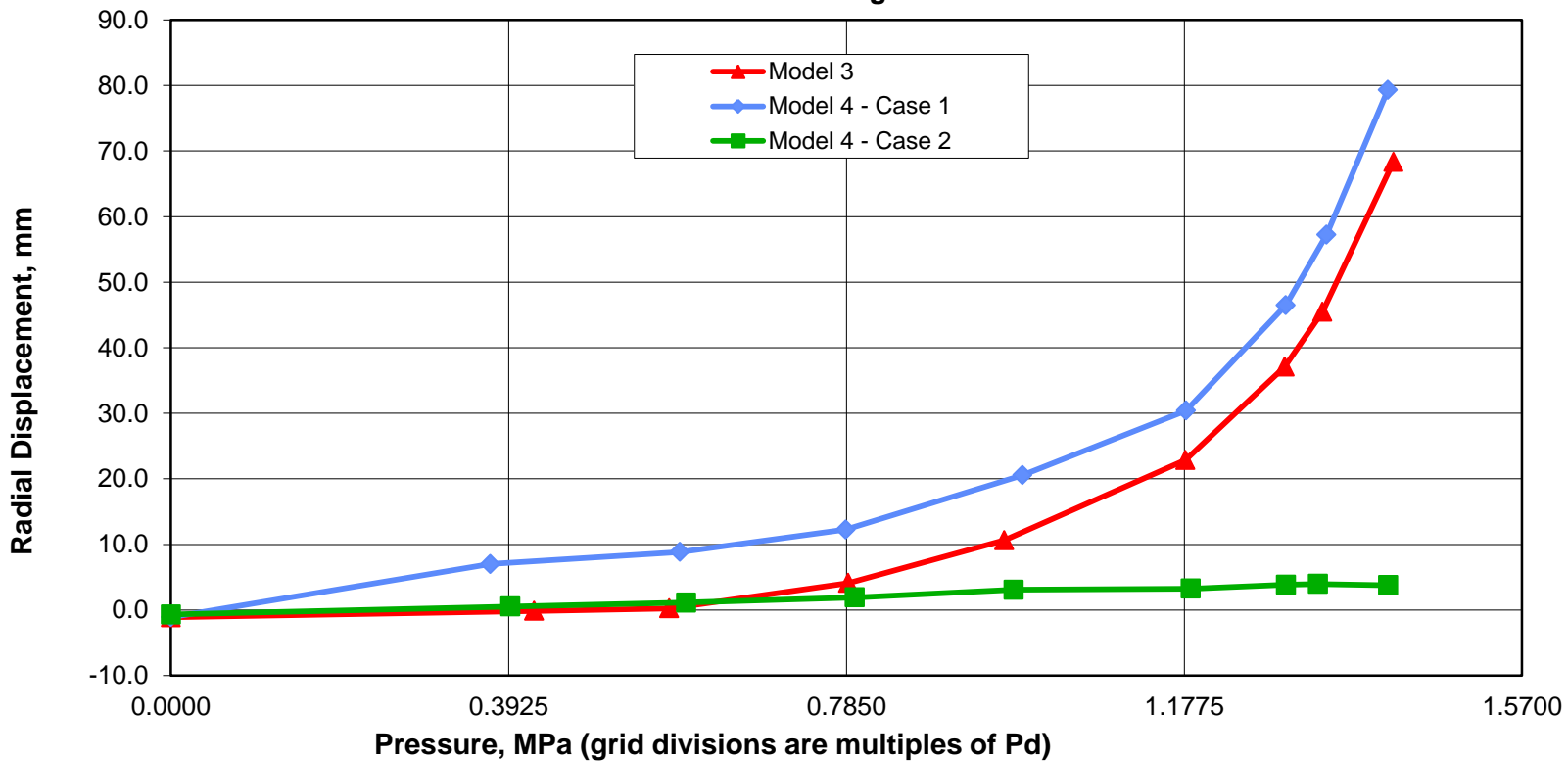


Standard Output Location #5. Azimuth: 135 Degrees, Elevation: 4.68 Meters, E/H Elevation



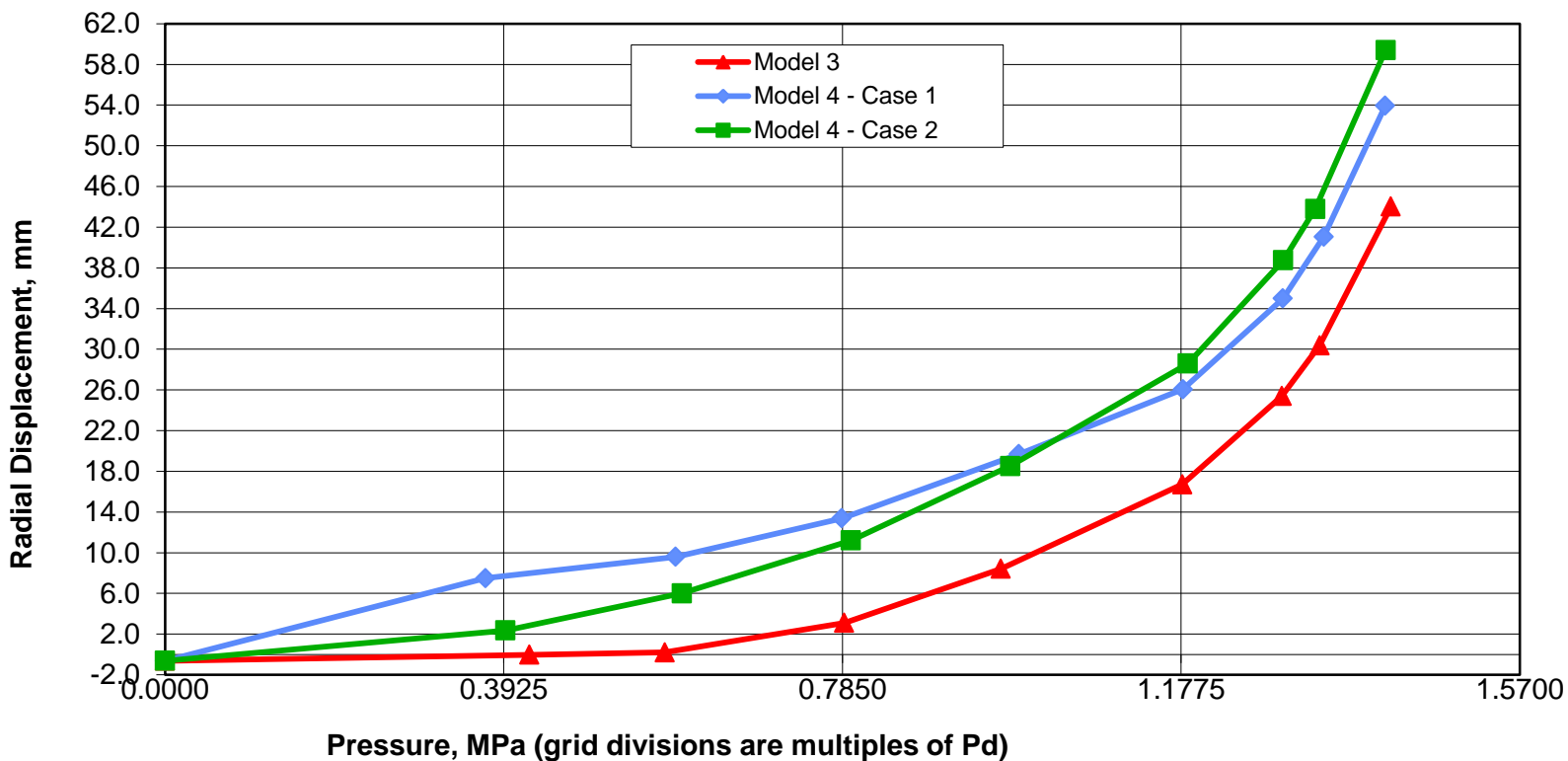


Standard Output Location #6. Azimuth: 135 Degrees, Elevation: 6.20 Meters, Approximate Midheight



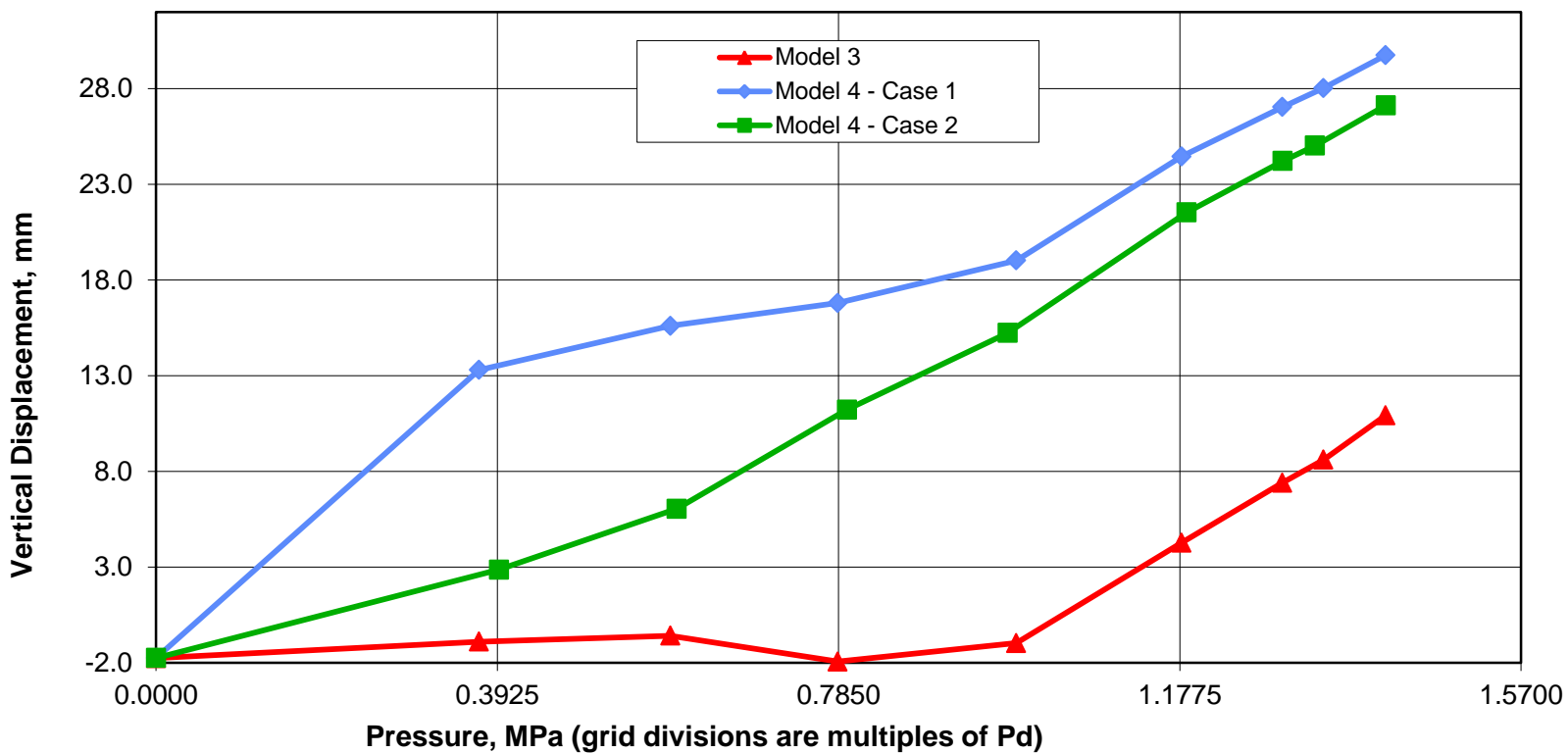


Standard Output Location #7. Azimuth: 135 Degrees, Elevation: 10.75 Meters, Springline



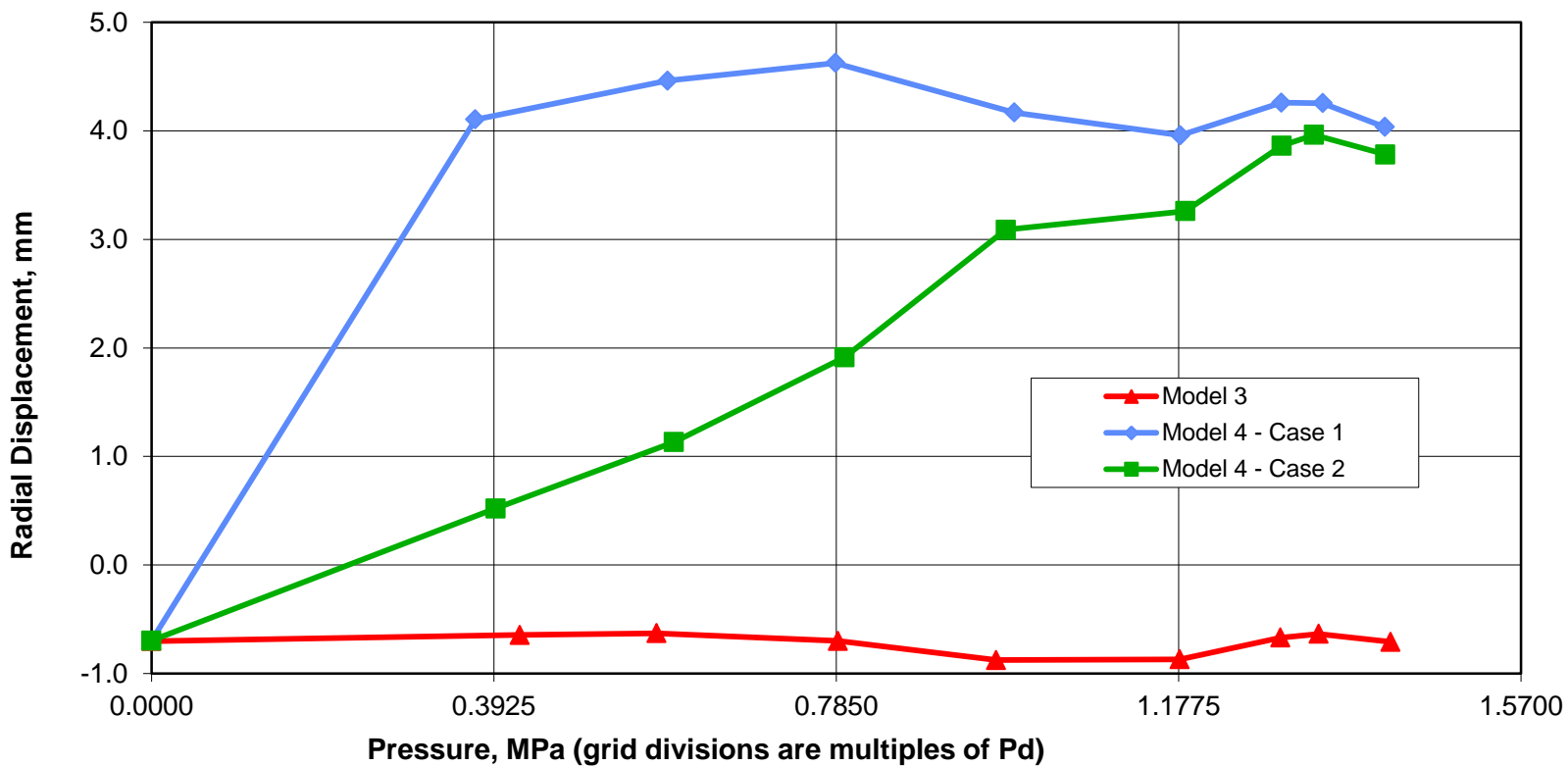


Standard Output Location #8. Azimuth: 135 Degrees, Elevation: 10.75 Meters, Springline



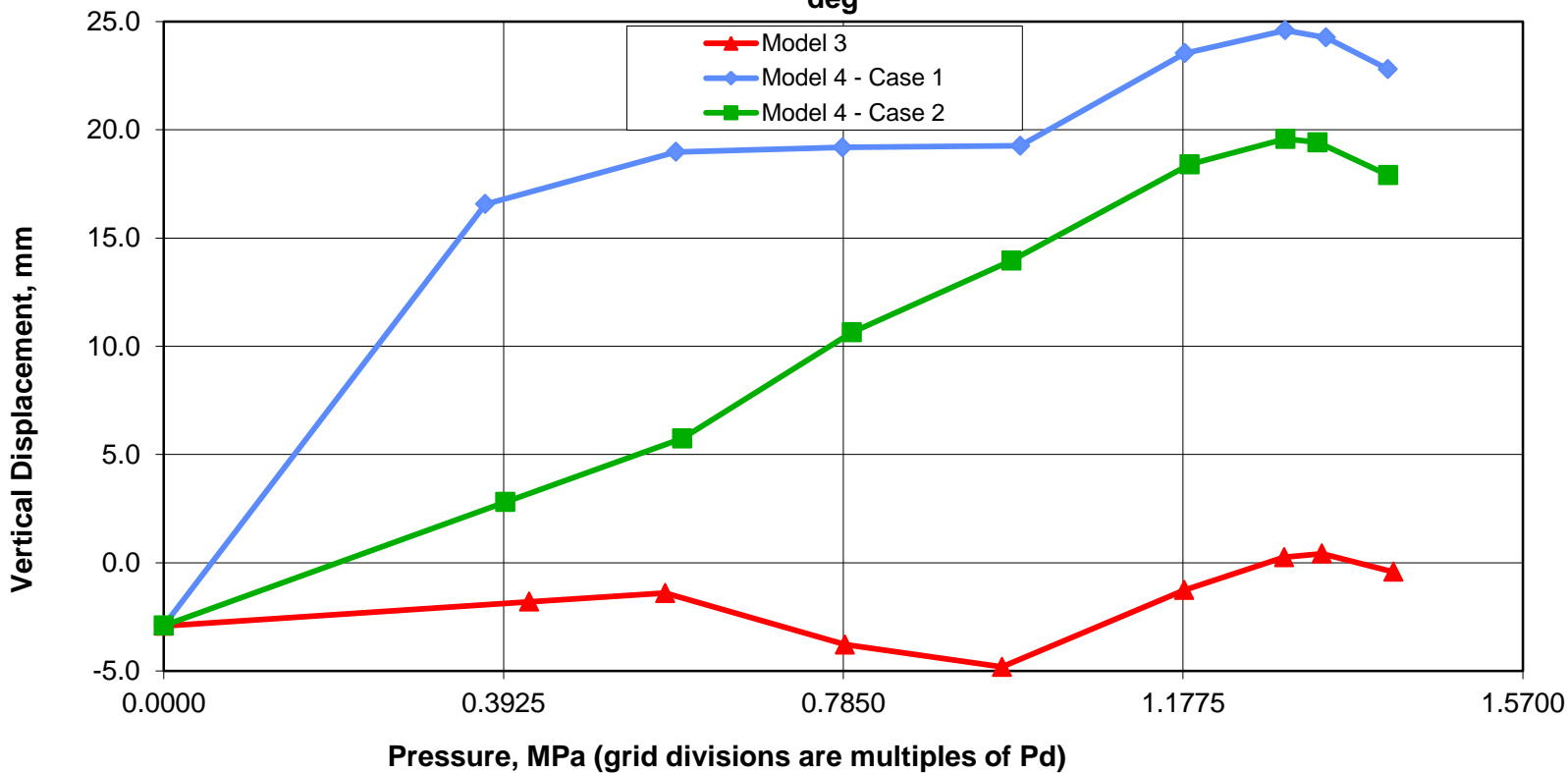


Standard Output Location #9. Azimuth: 135 Degrees, Elevation: 14.55 Meters, Dome 45 deg



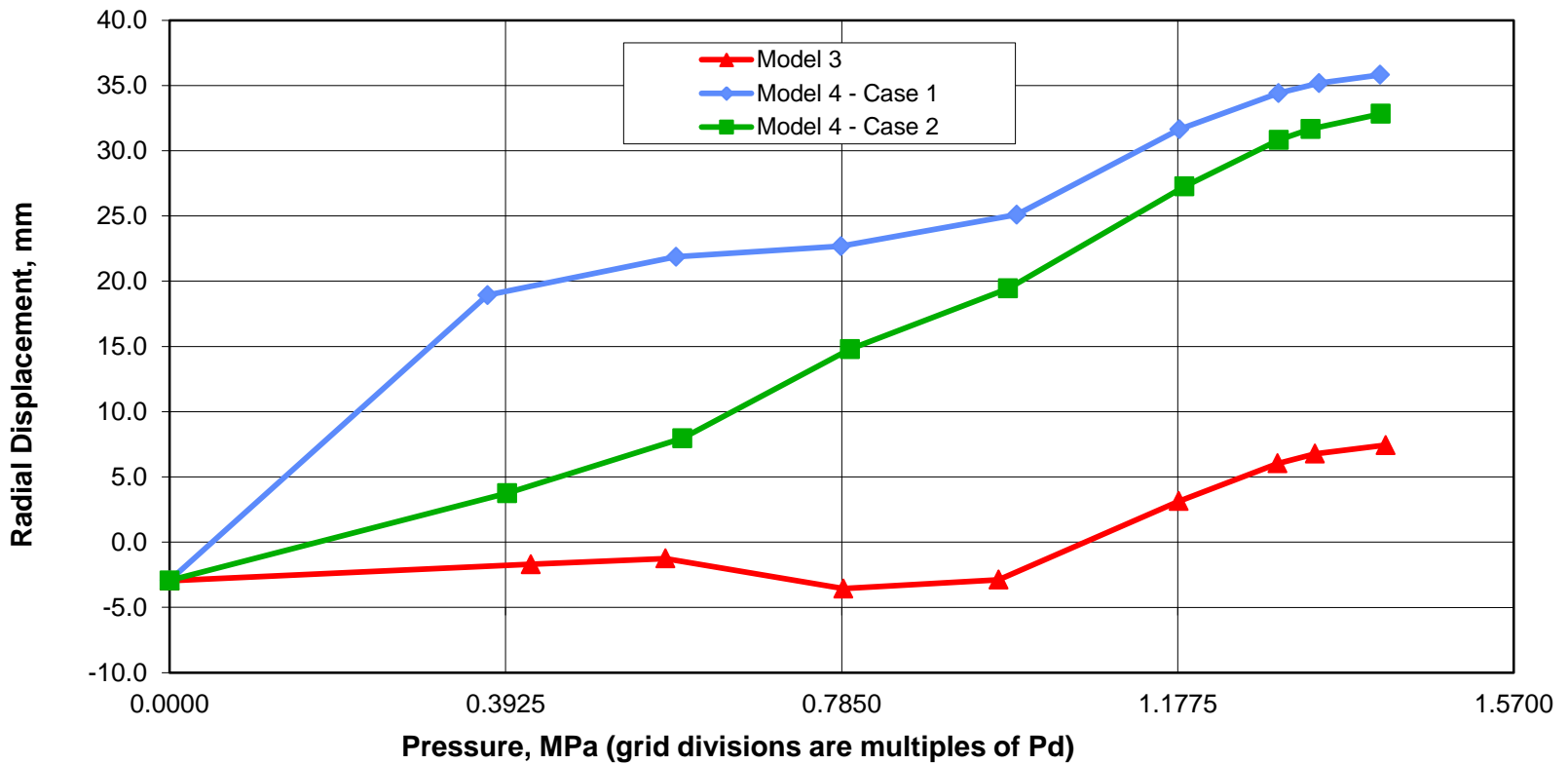


Standard Output Location #10. Azimuth: 135 Degrees, Elevation: 14.55 Meters, Dome 45 deg



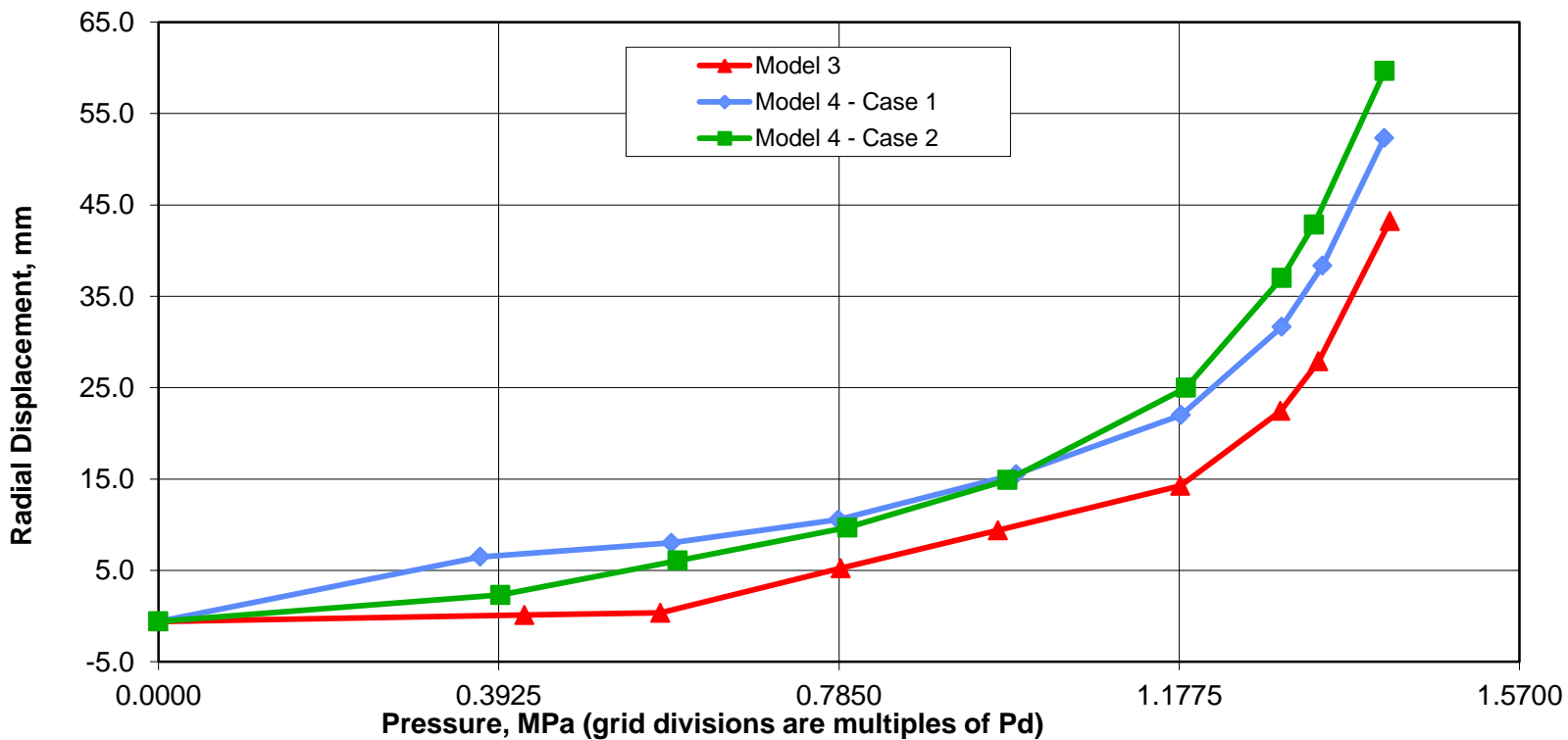


Standard Output Location #11. Azimuth: Apex , Elevation: 16.13 Meters,



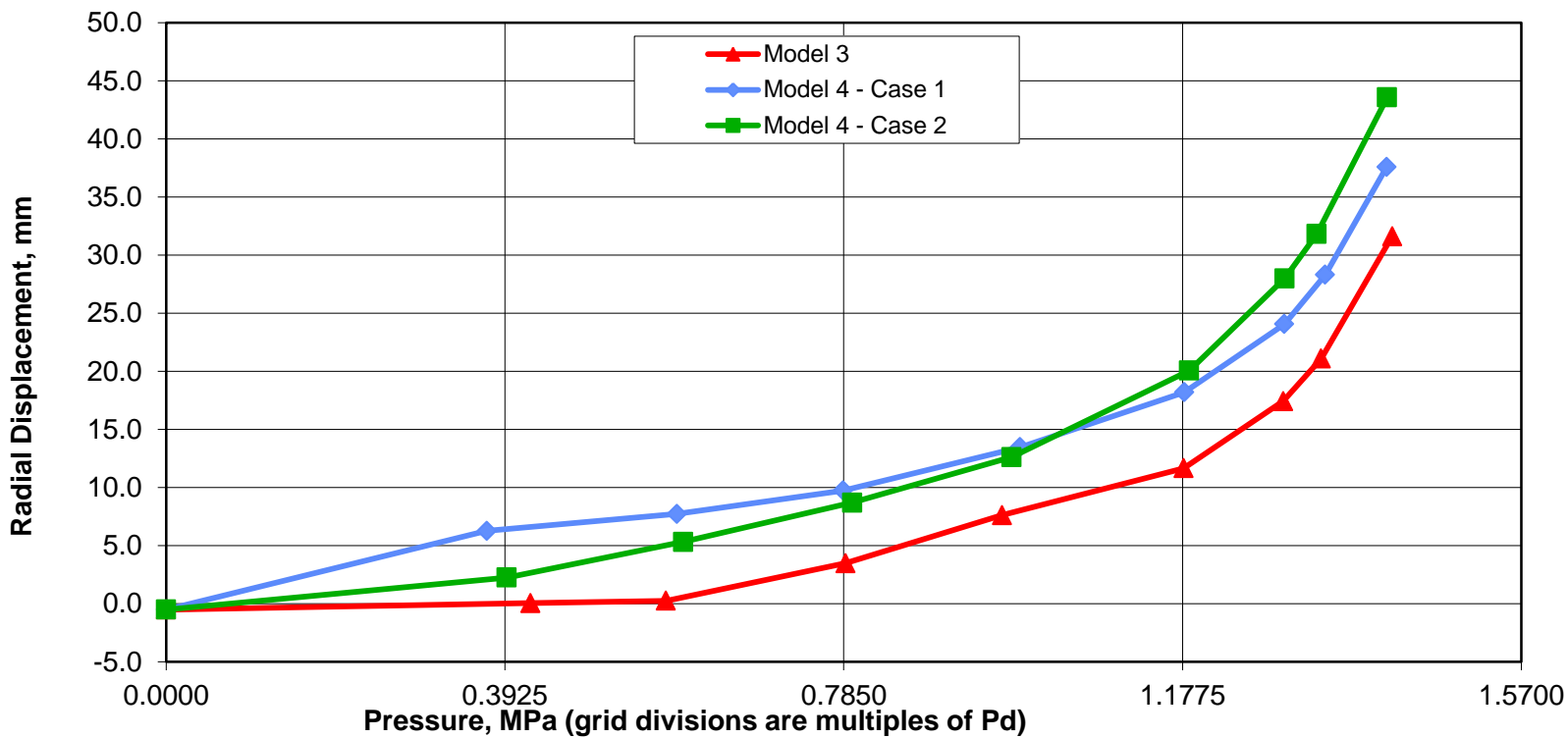


Standard Output Location #12. Azimuth: 90 Degrees, Elevation: 6.2 Meters, Midheight at Buttress



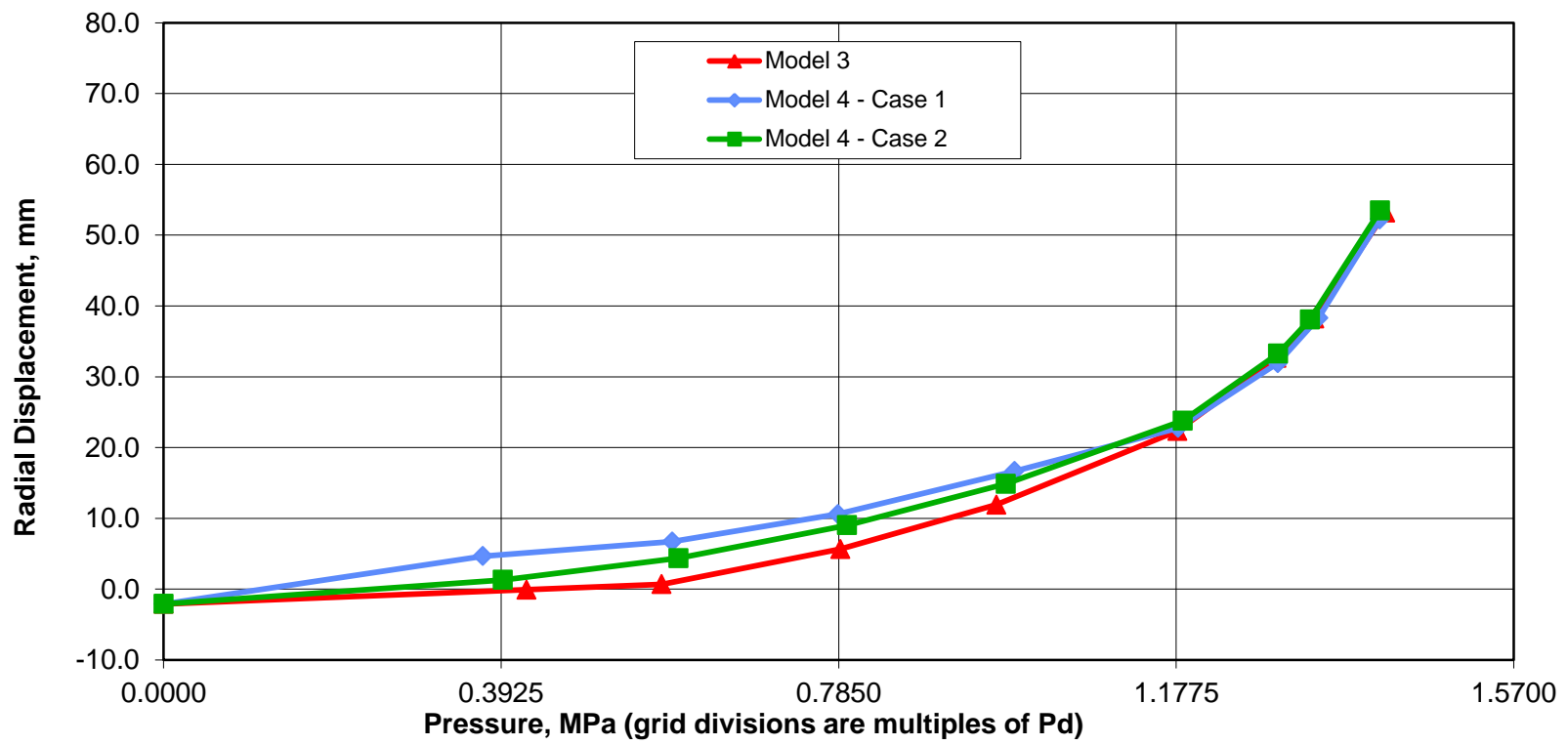


Standard Output Location #13. Azimuth: 90 Degrees, Elevation: 10.75 Meters, Springline at Buttress



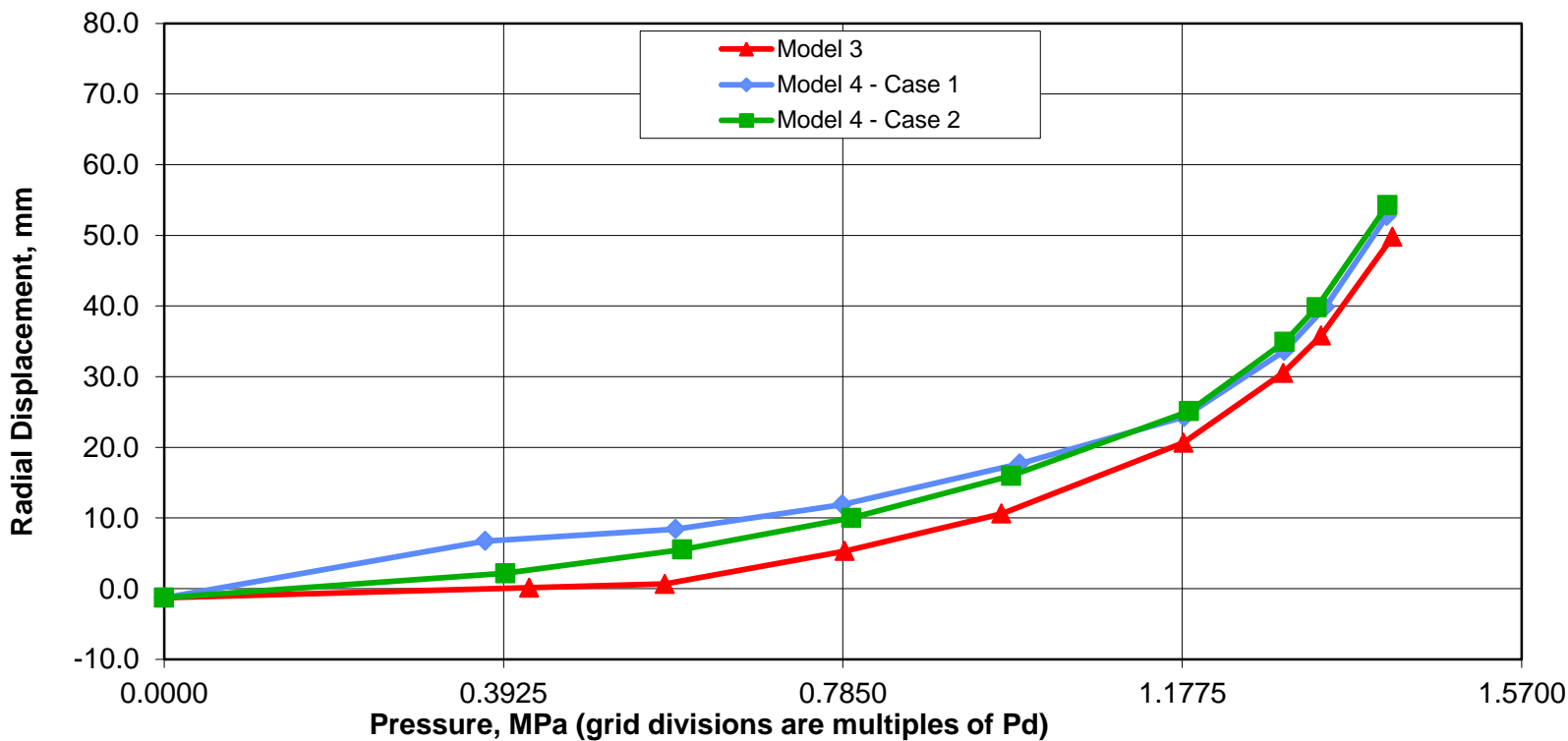


**Standard Output Location #14. Azimuth: 334 Degrees, Elevation: 4.675 Meters,
Center of E/H**



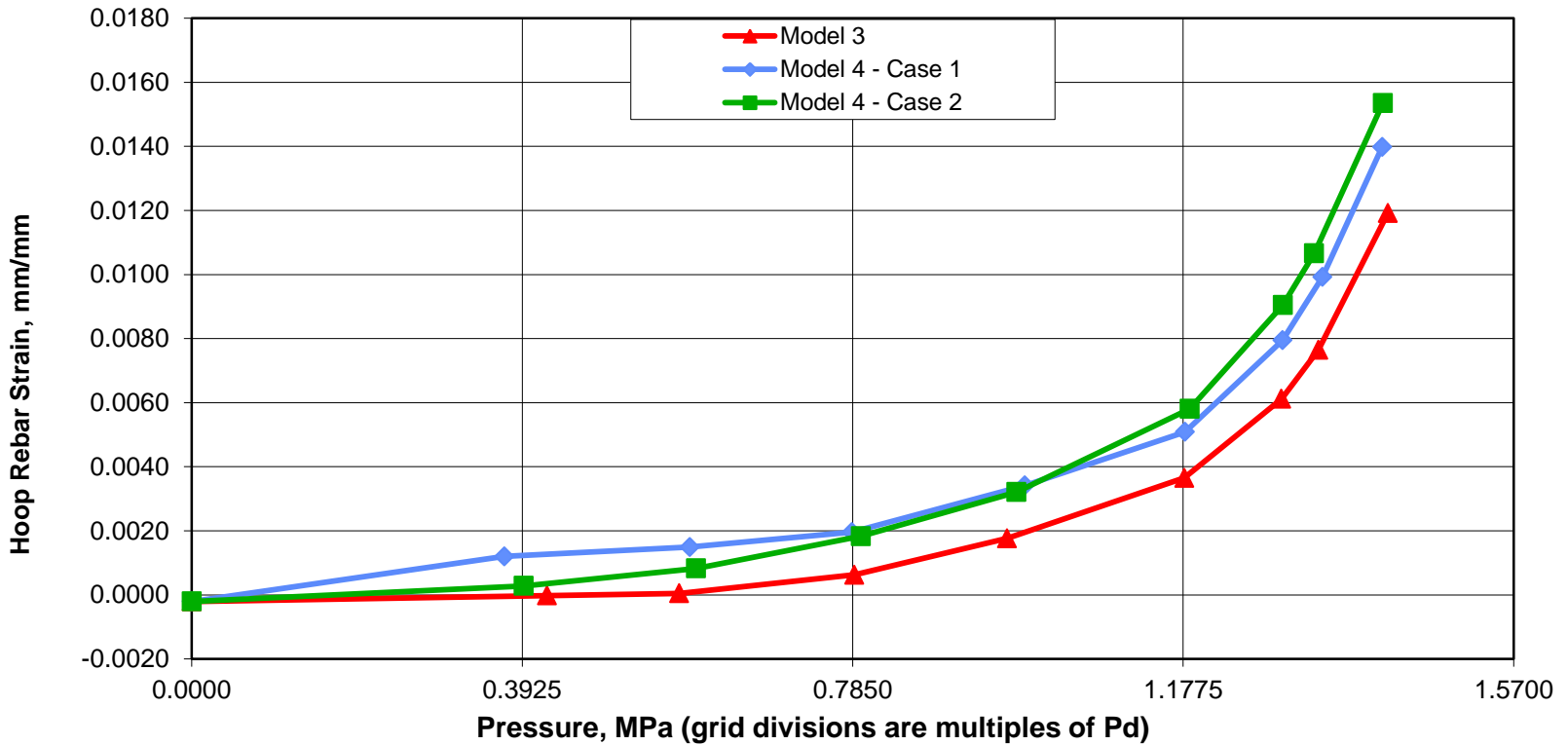


**Standard Output Location #15. Azimuth: 66 Degrees, Elevation: 4.525 Meters,
Center of A/L**



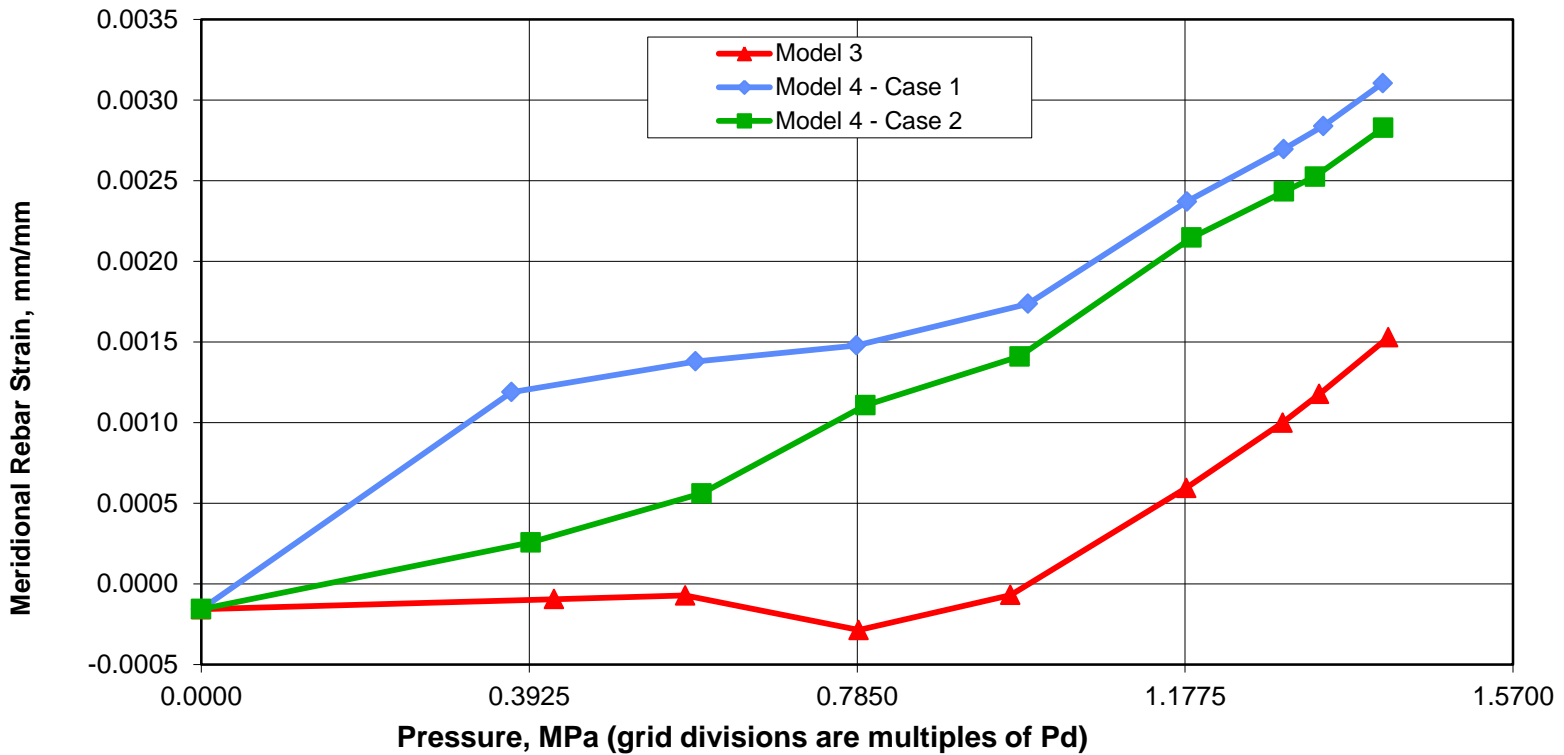


Standard Output Location #22. Azimuth: 135 Degrees, Elevation: 6.20 Meters,
Outer Rebar Layer, Midheight



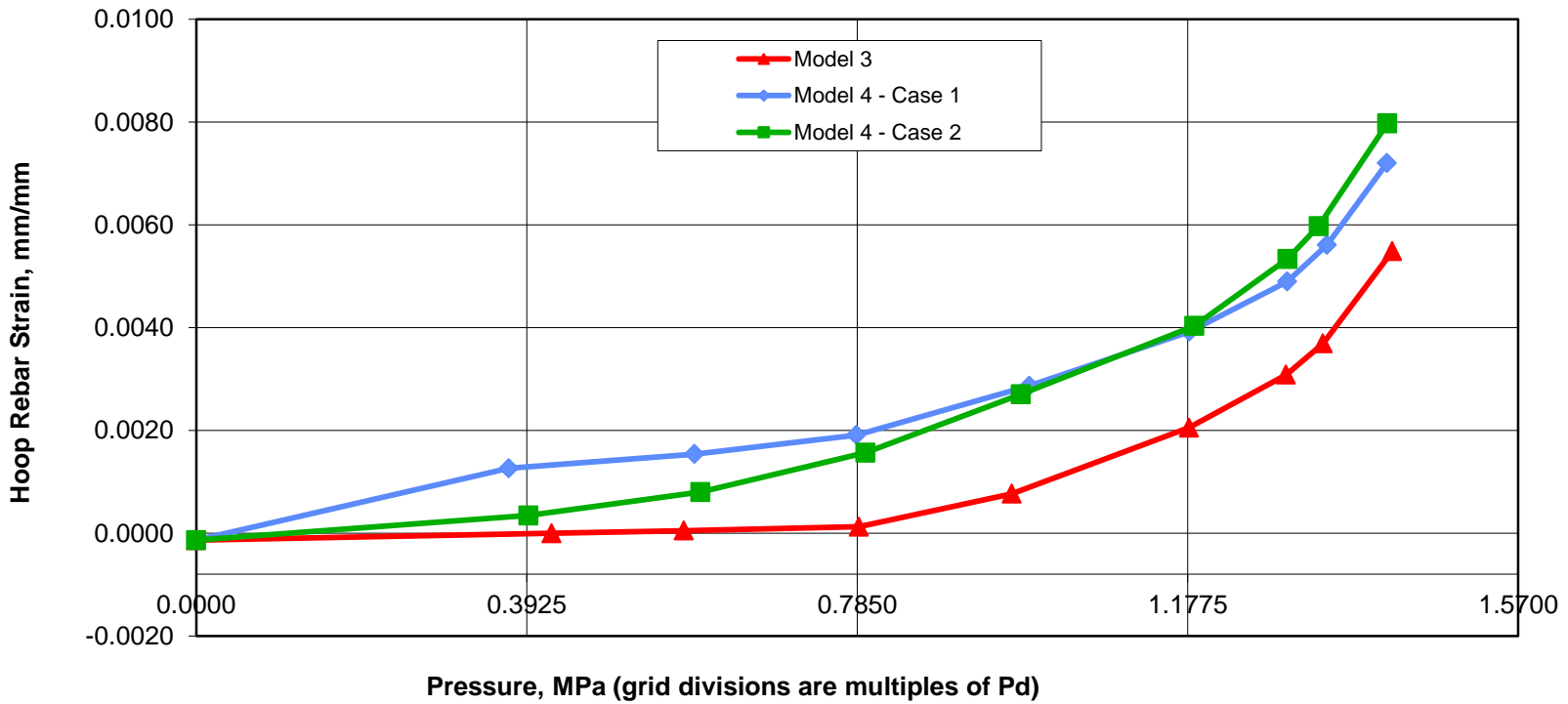


**Standard Output Location #23. Azimuth: 135 Degrees, Elevation: 6.20 Meters,
Outer Rebar Layer, Midheight**



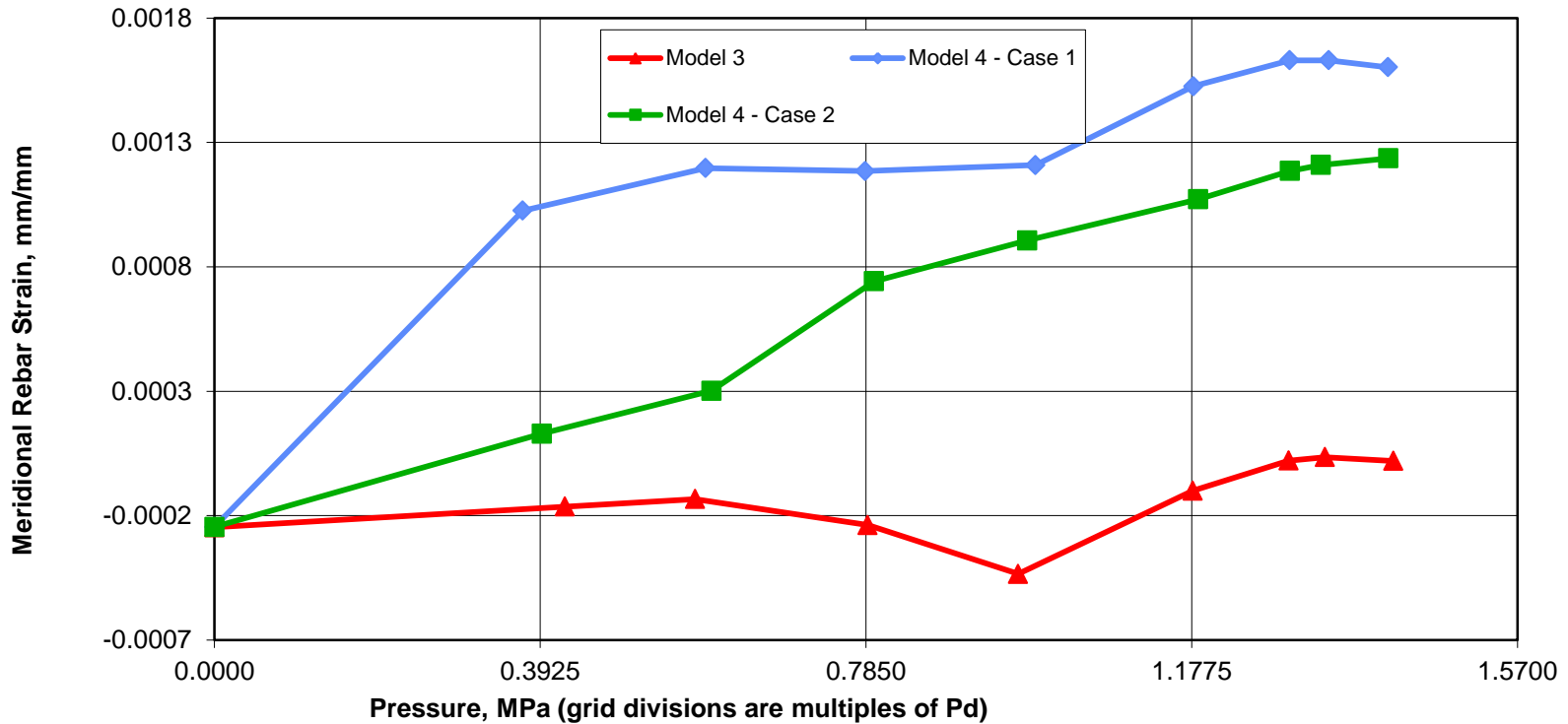


**Standard Output Location #24. Azimuth: 135 Degrees, Elevation: 10.75 Meters,
Outer Rebar Layer, Springline**



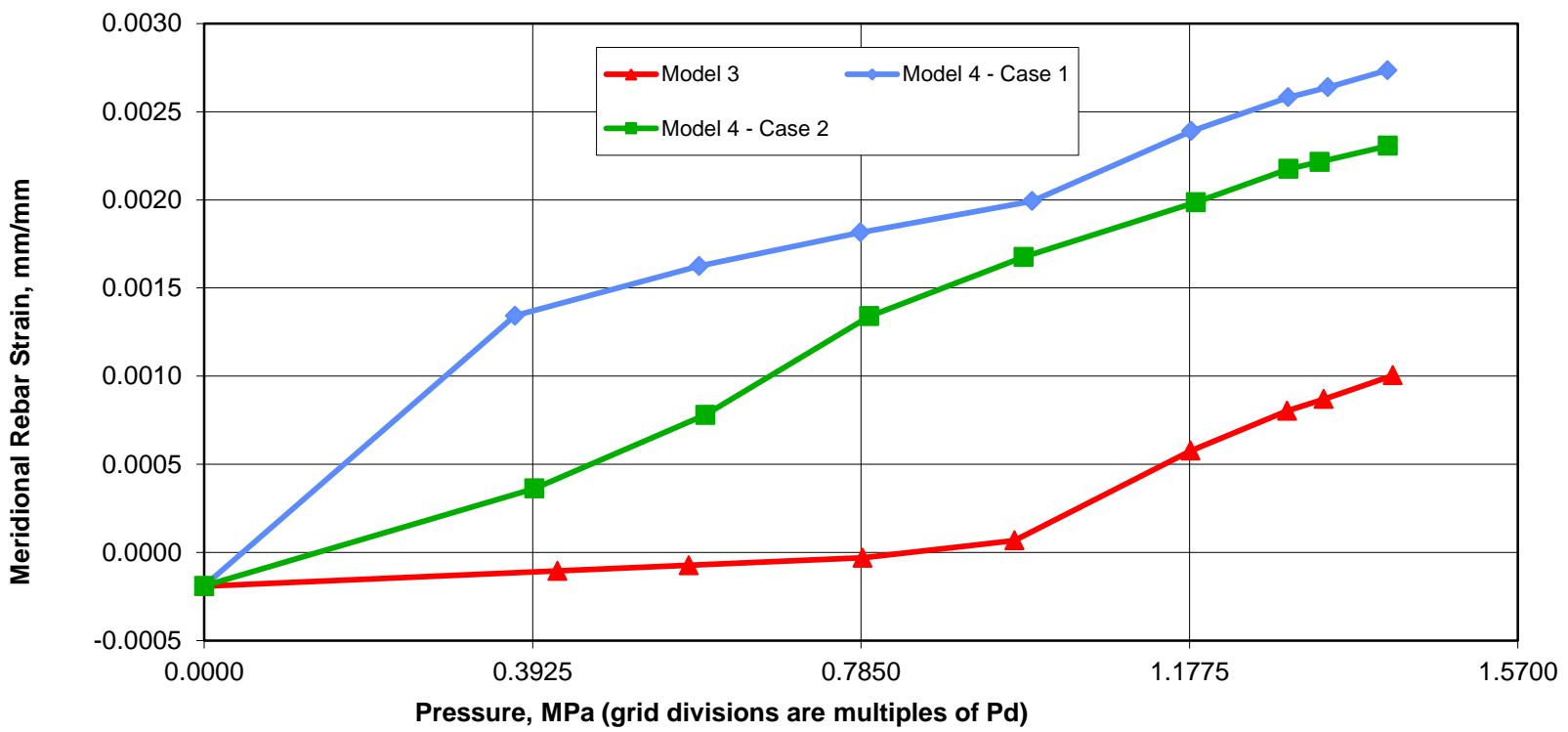


Standard Output Location #25. Azimuth: 135 Degrees, Elevation: 10.75 Meters,
Inner Rebar Layer, Springline



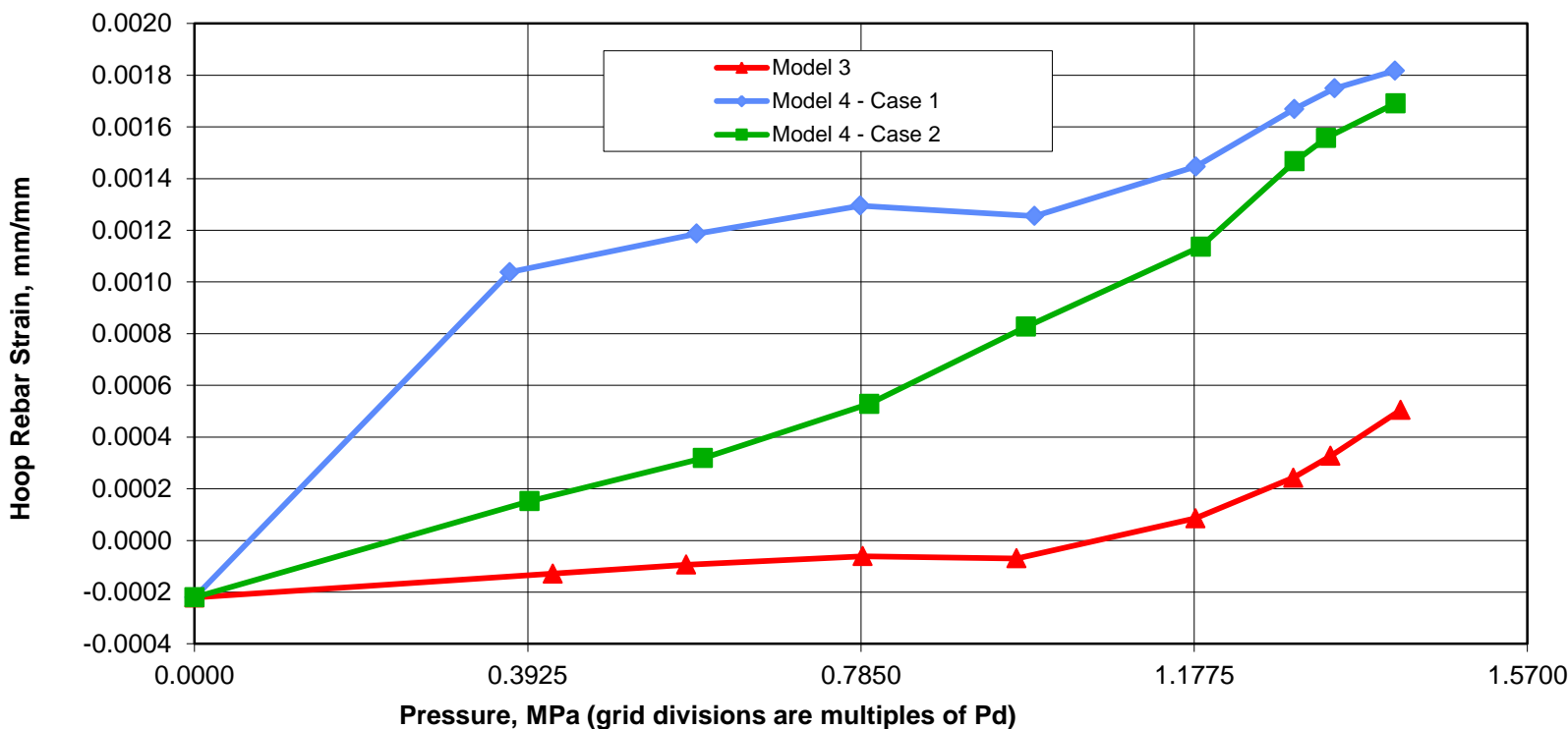


**Standard Output Location #26. Azimuth: 135 Degrees, Elevation: 10.75 Meters,
Outer Rebar Layer, Springline**



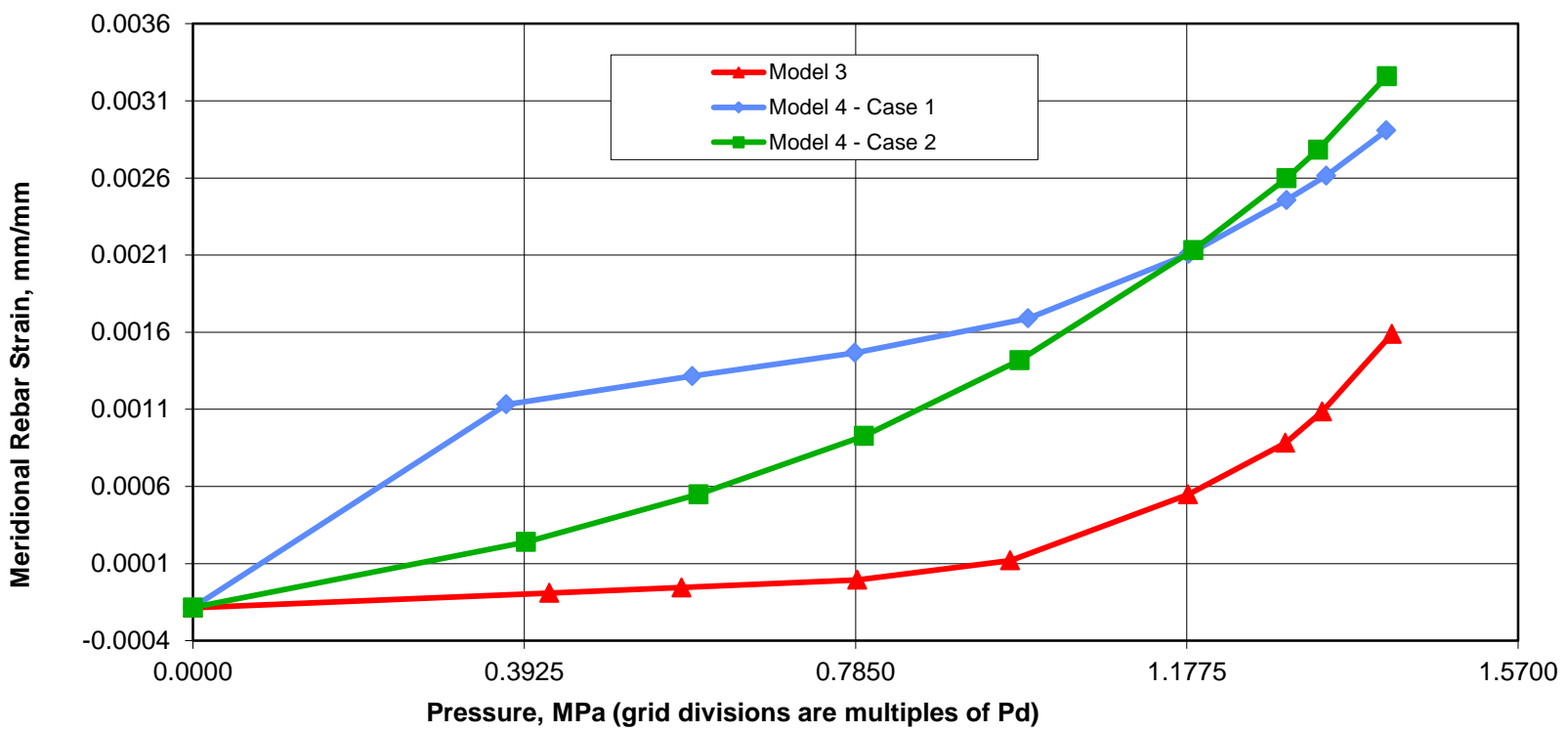


**Standard Output Location #27. Azimuth: 135 Degrees, Elevation: 14.55 Meters,
Outer Rebar Layer, Dome 45 deg**



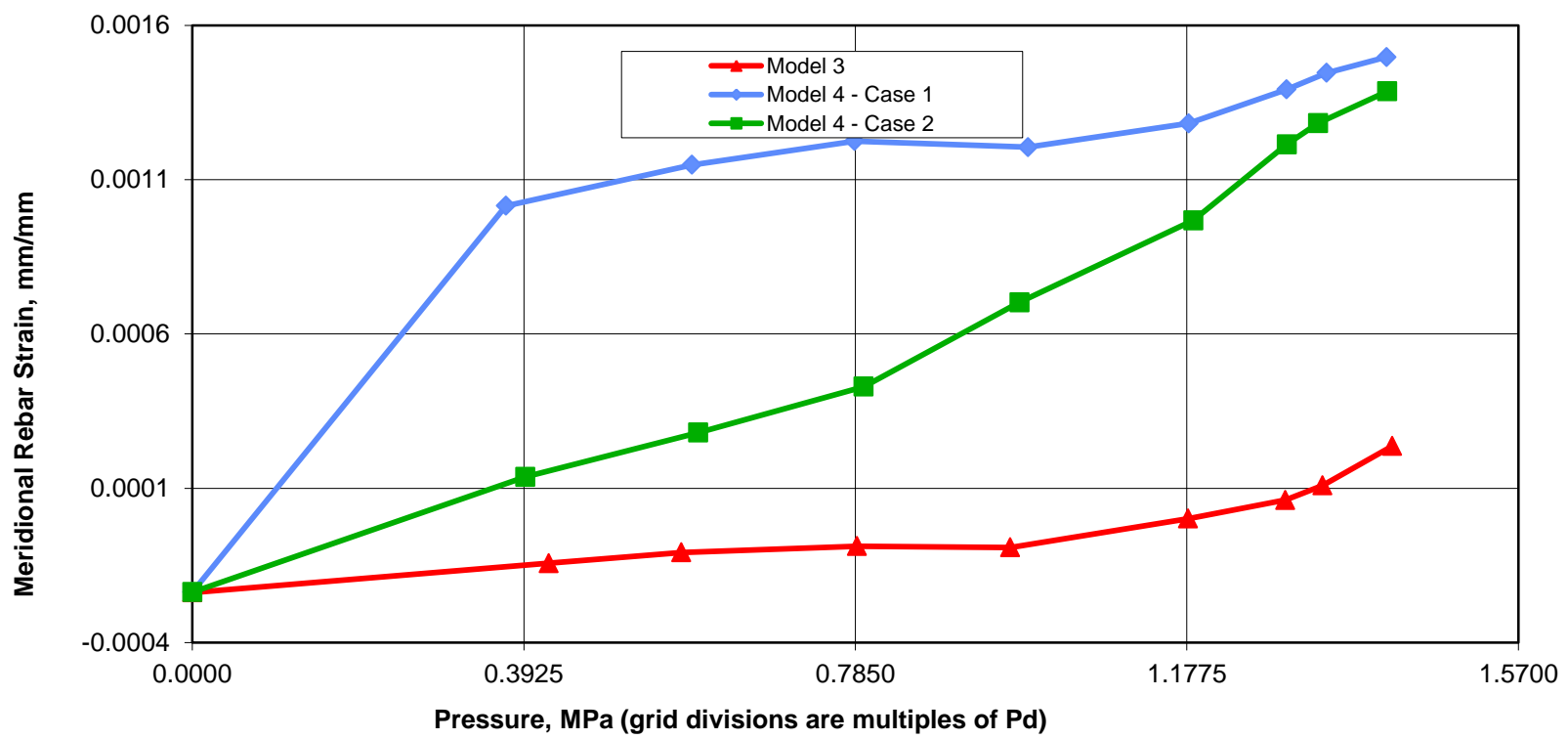


**Standard Output Location #28. Azimuth: 135 Degrees, Elevation: 14.55 Meters,
Inner Rebar Layer, Dome 45 deg**



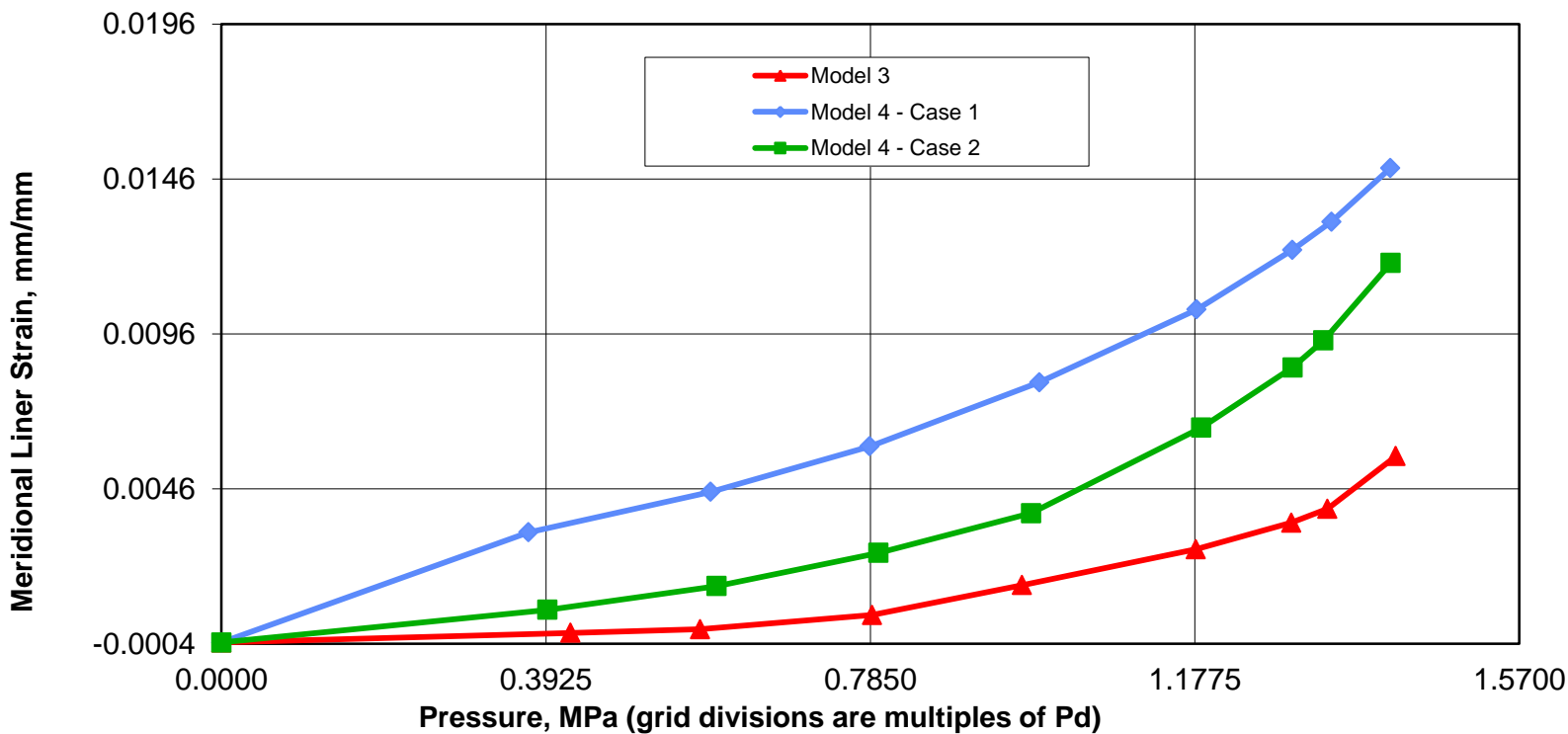


Standard Output Location #29. Azimuth: 135 Degrees, Elevation: 14.55 Meters, Outer Rebar Layer, Dome 45 deg



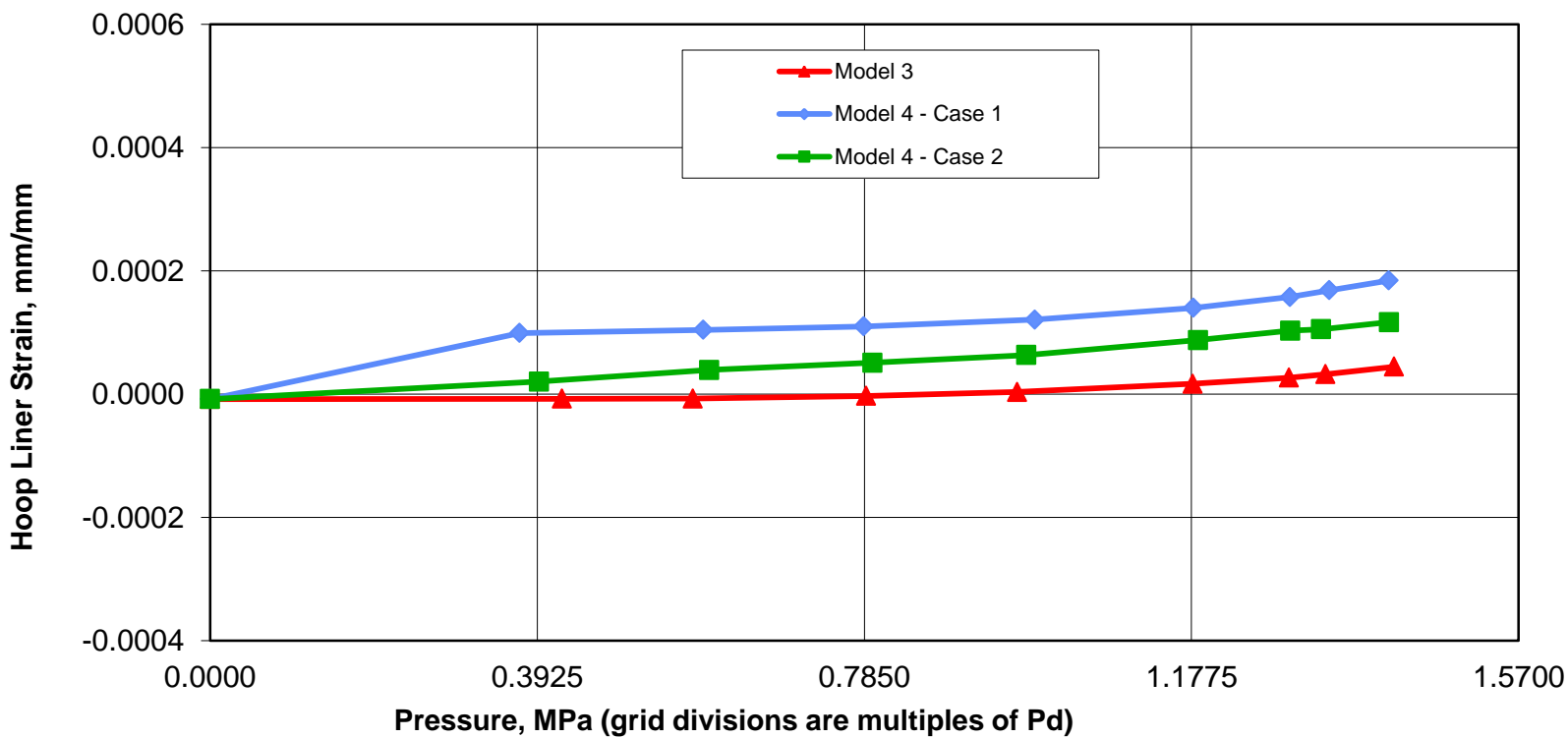


Standard Output Location: #36. Azimuth: 135 Degrees, Elevation: 0.25 Meters,
Inside Liner Surface, Base of Cylinder



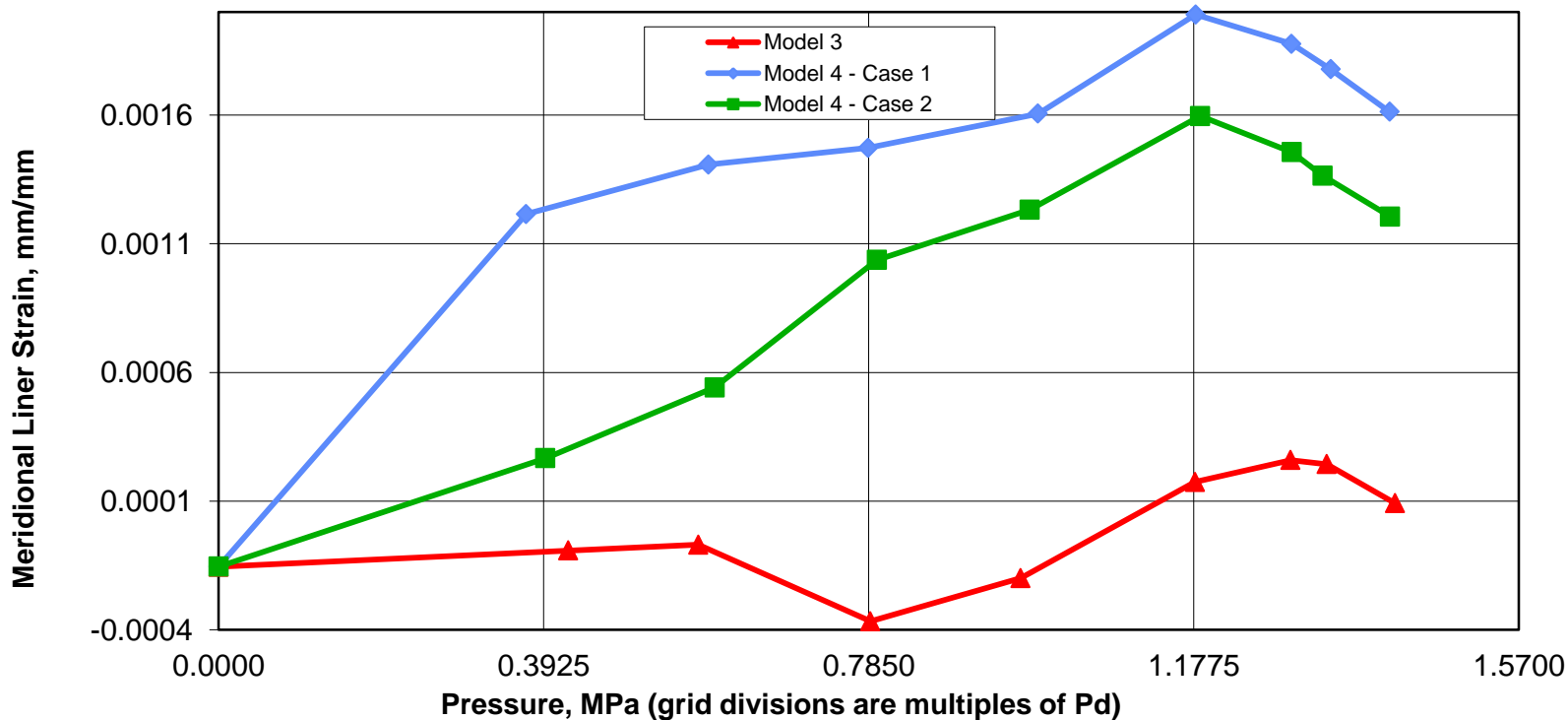


Standard Output Location: #37. Azimuth: 135 Degrees, Elevation: 0.25 Meters,
Inside Liner Surface, Base of Cylinder



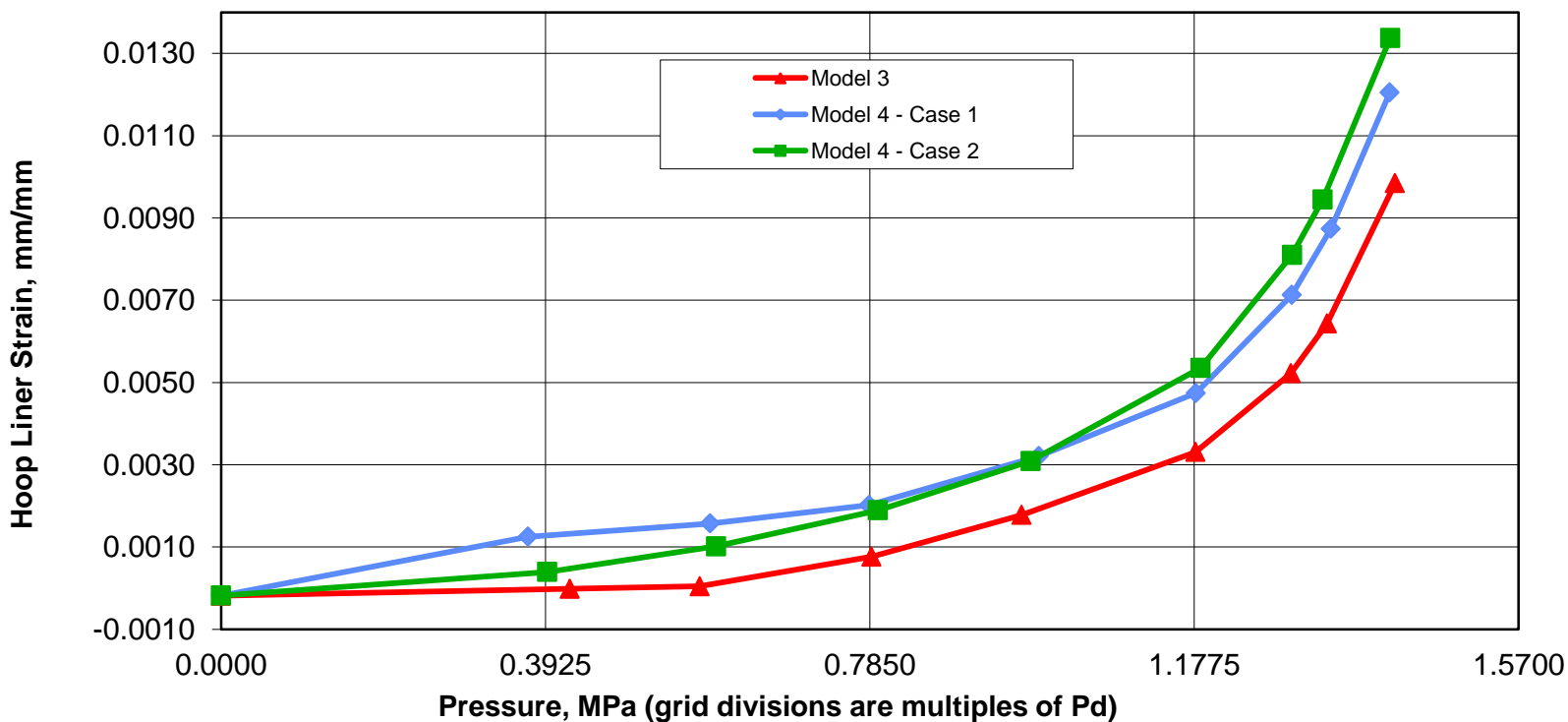


Standard Output Location: #38. Azimuth: 135 Degrees, Elevation: 6.20 Meters,
Inside Liner Surface, Midheight



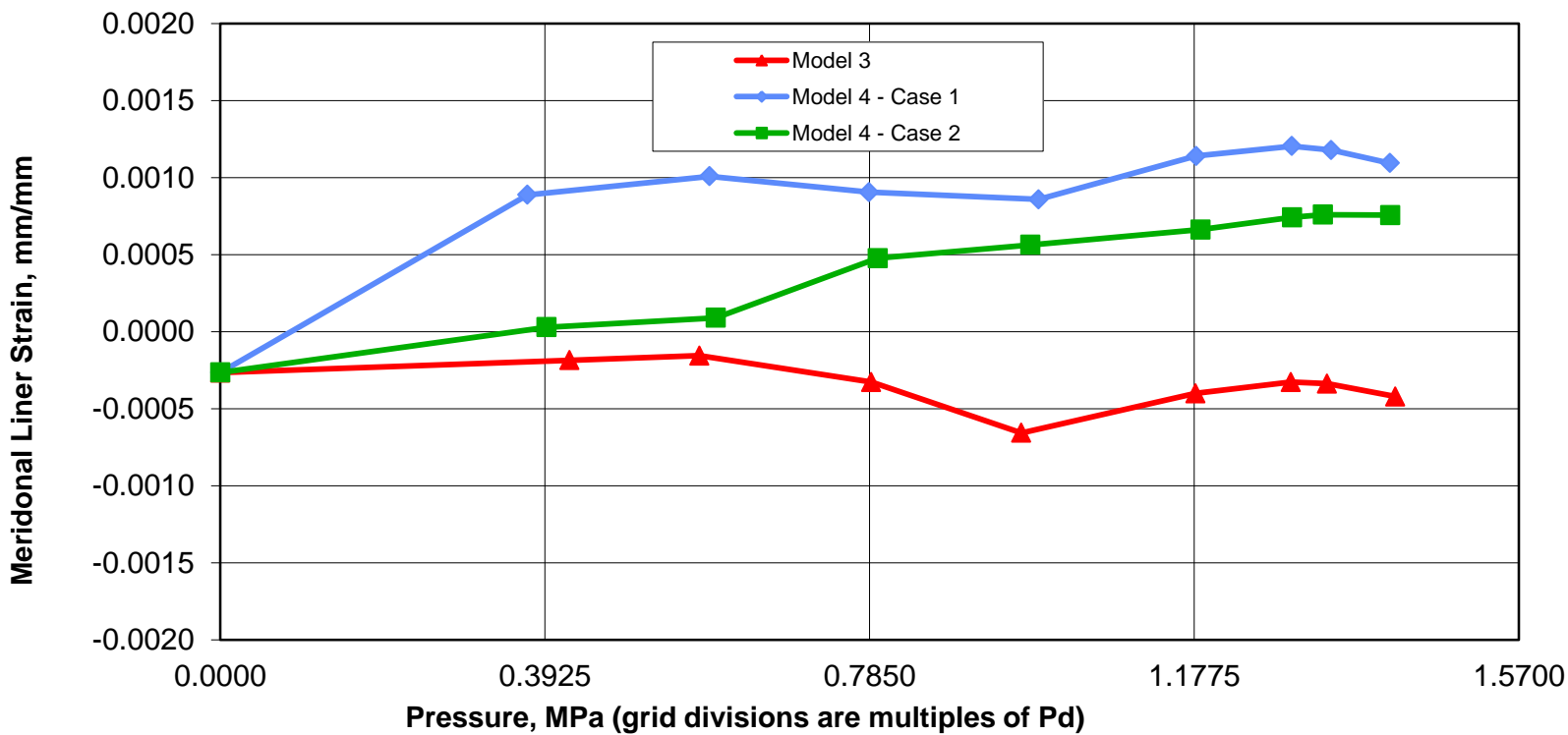


Standard Output Location: #39. Azimuth: 135 Degrees, Elevation: 6.20 Meters,
Inside Liner Surface, Midheight



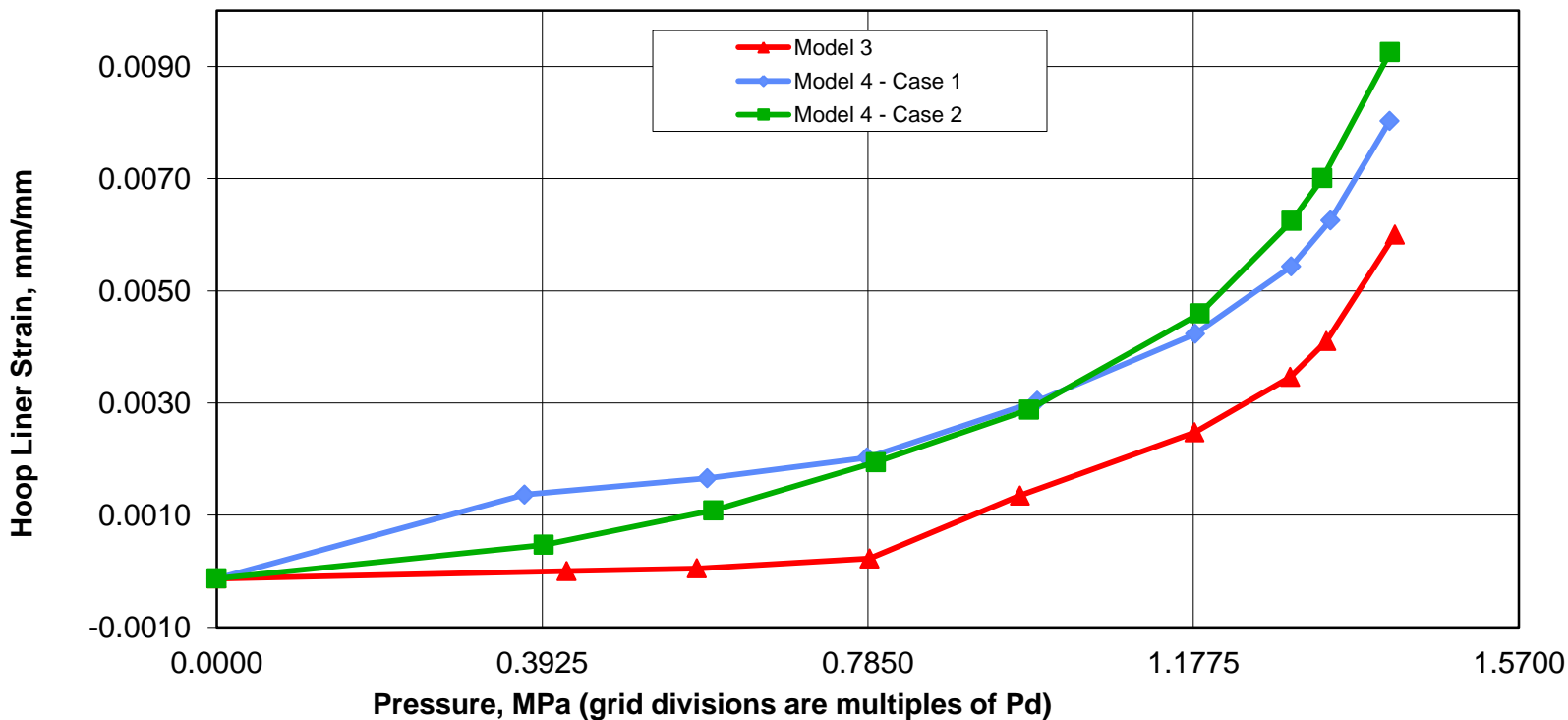


**Standard Output Location: #40. Azimuth: 135 Degrees, Elevation: 10.75 Meters,
Inside Liner Surface, Springline**



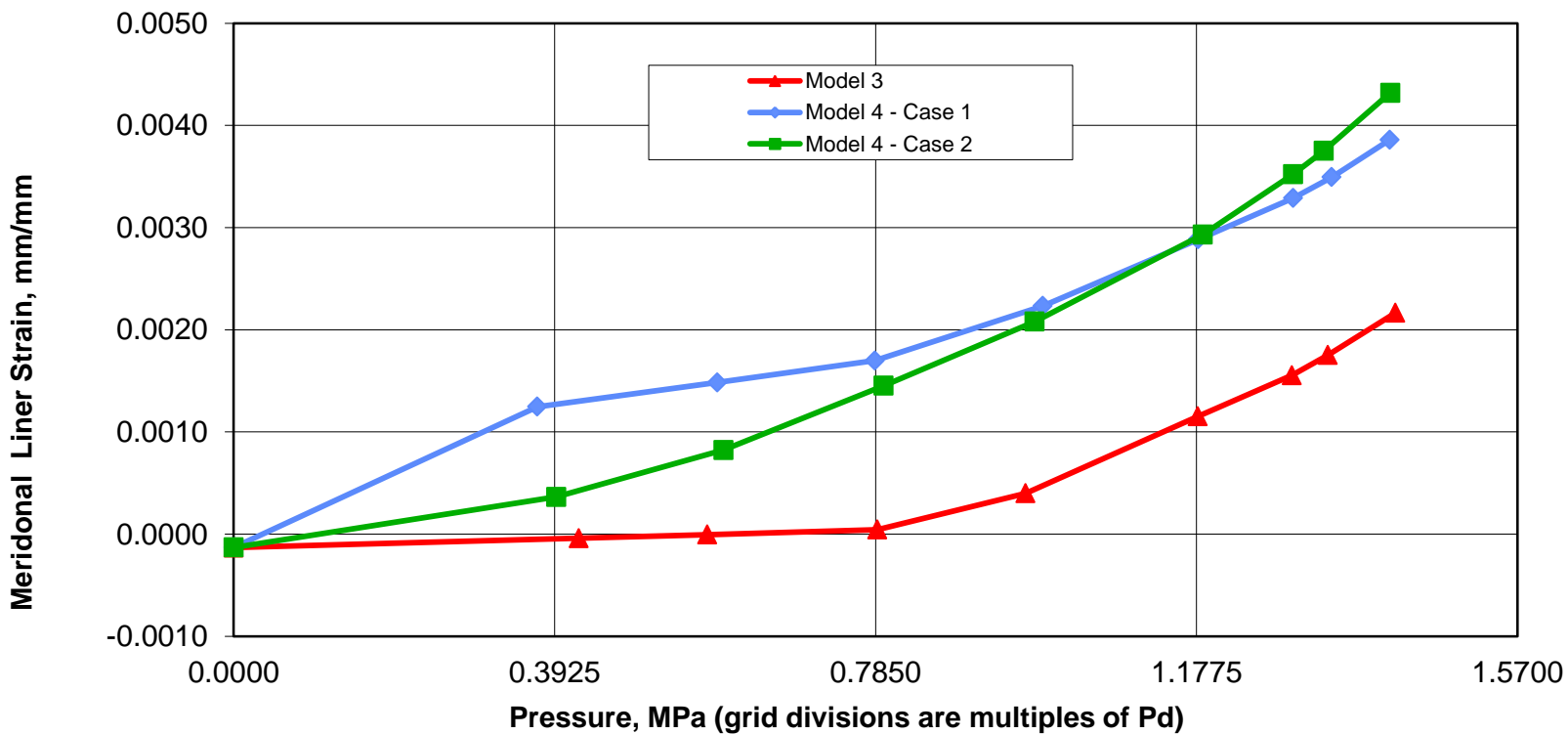


Standard Output Location: #41. Azimuth: 135 Degrees, Elevation: 10.75 Meters,
Inside Liner Surface, Springline



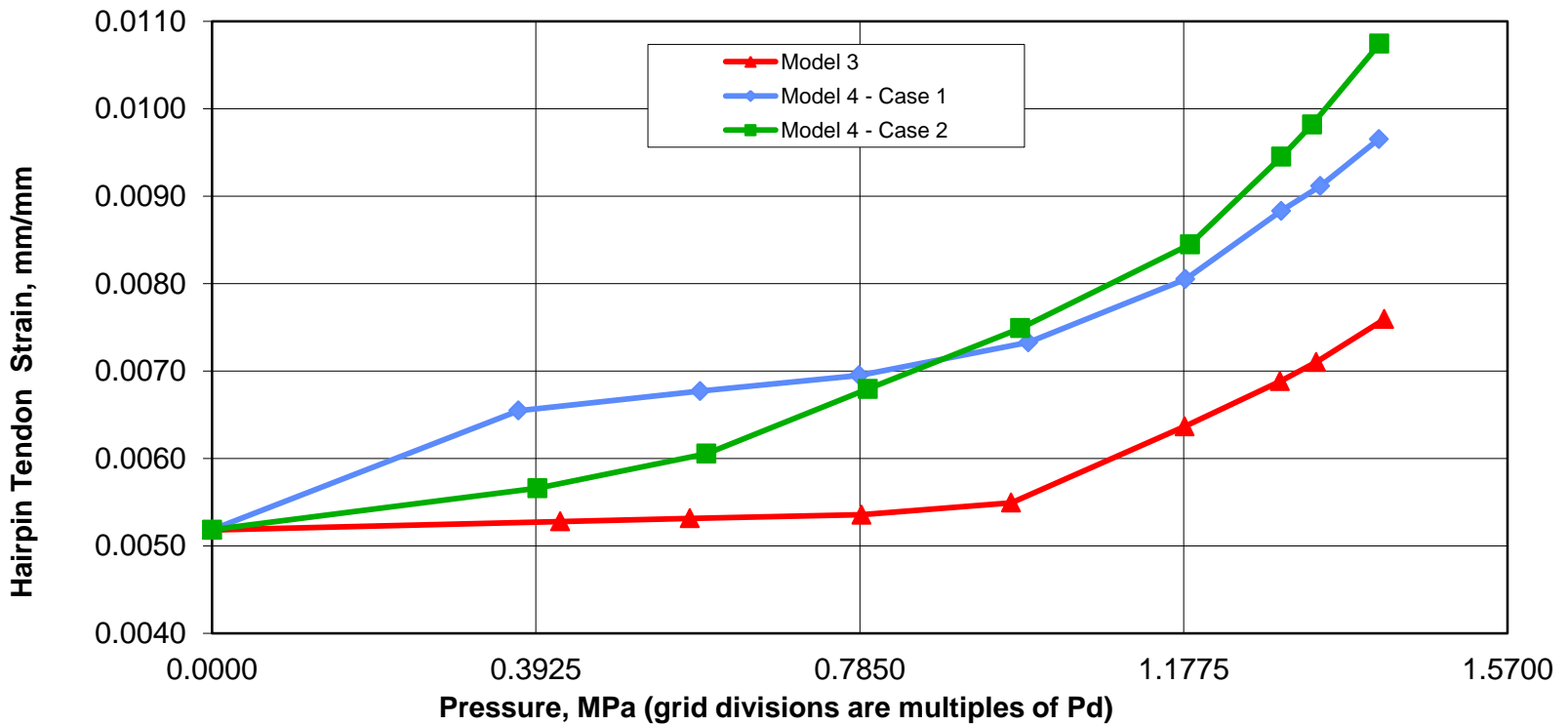


**Standard Output Location: #42. Azimuth: 135 Degrees, Elevation: 16.13 Meters,
Inside Liner Surface, Dome Apex**



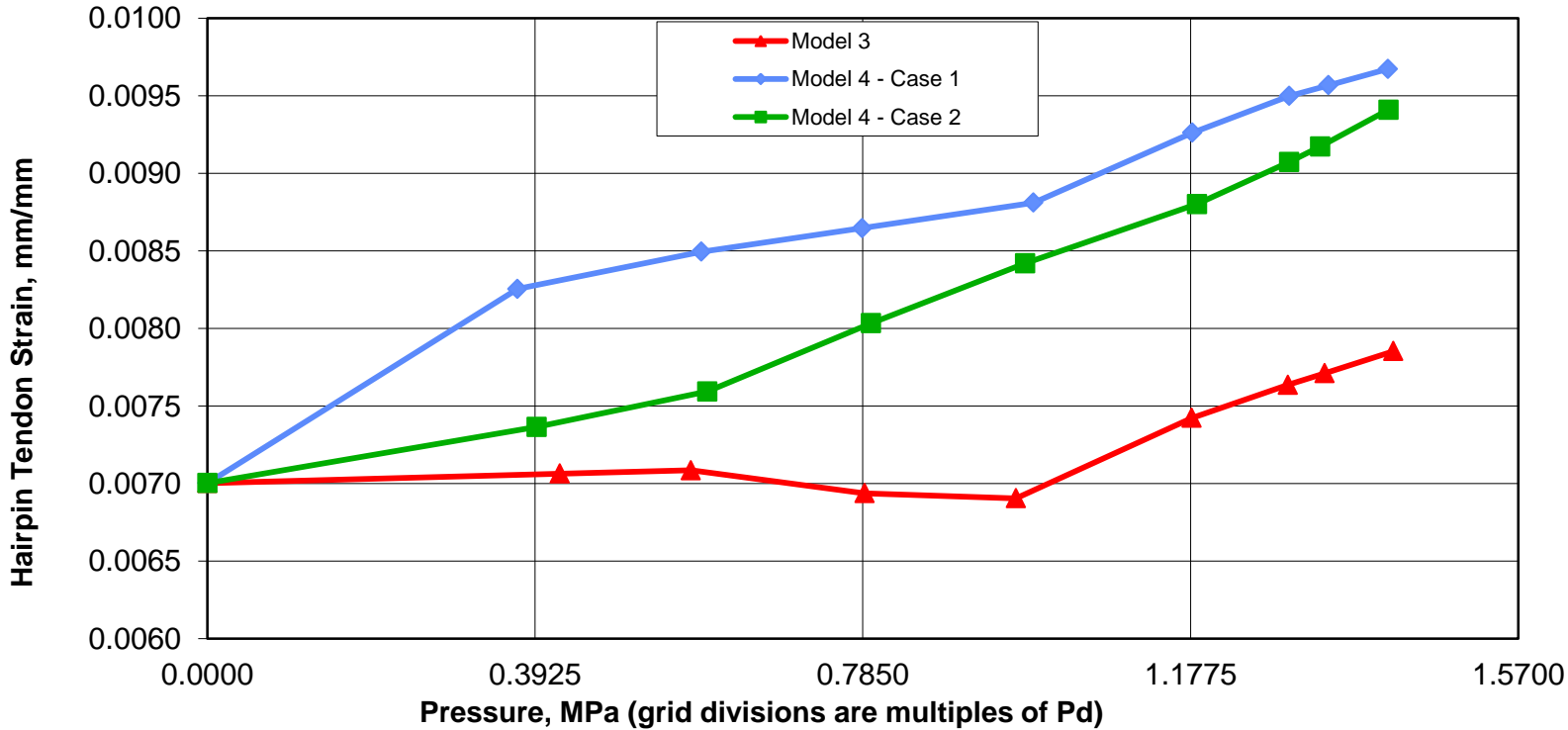


Standard Output Location: #48. Azimuth: 180 Degrees, Elevation: 15.6 Meters,
Tendon V37, Tendon Apex



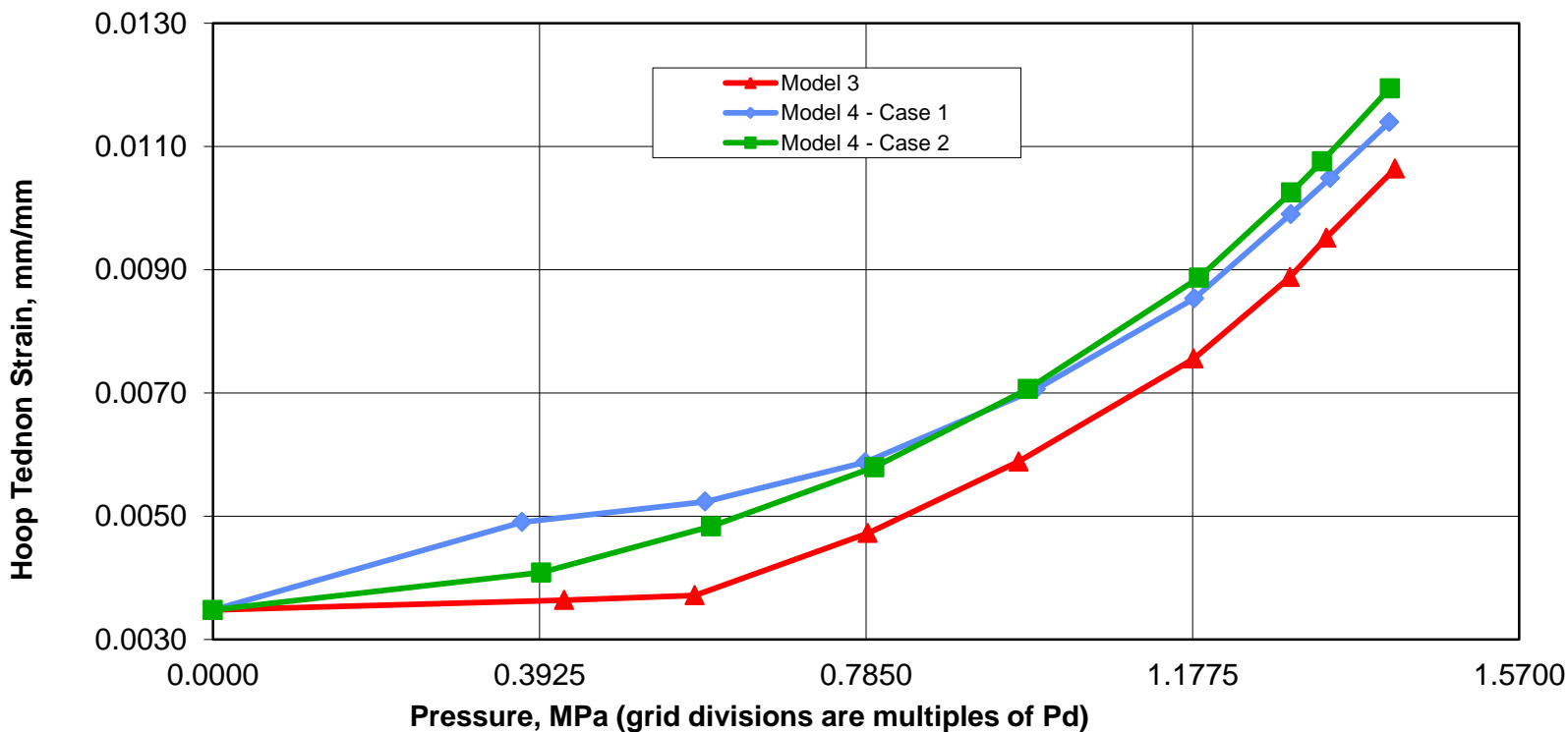


Standard Output Location: #49. Azimuth: 135 Degrees, Elevation: 10.75 Meters,
Tendon V46, Tendon Springline



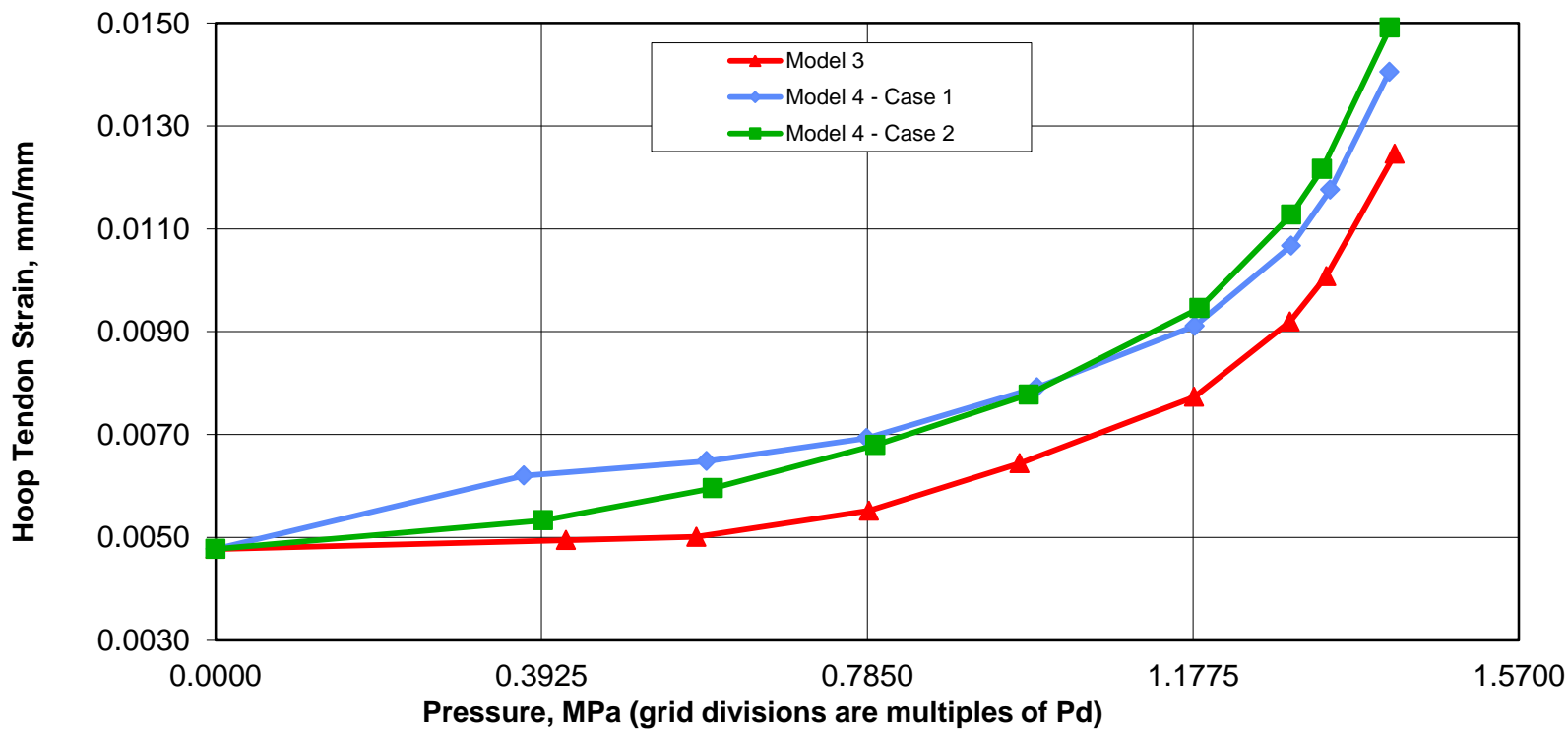


Standard Output Location: #50. Azimuth: 90 Degrees, Elevation: 6.58 Meters,
Tendon H53, Mid. Tendon



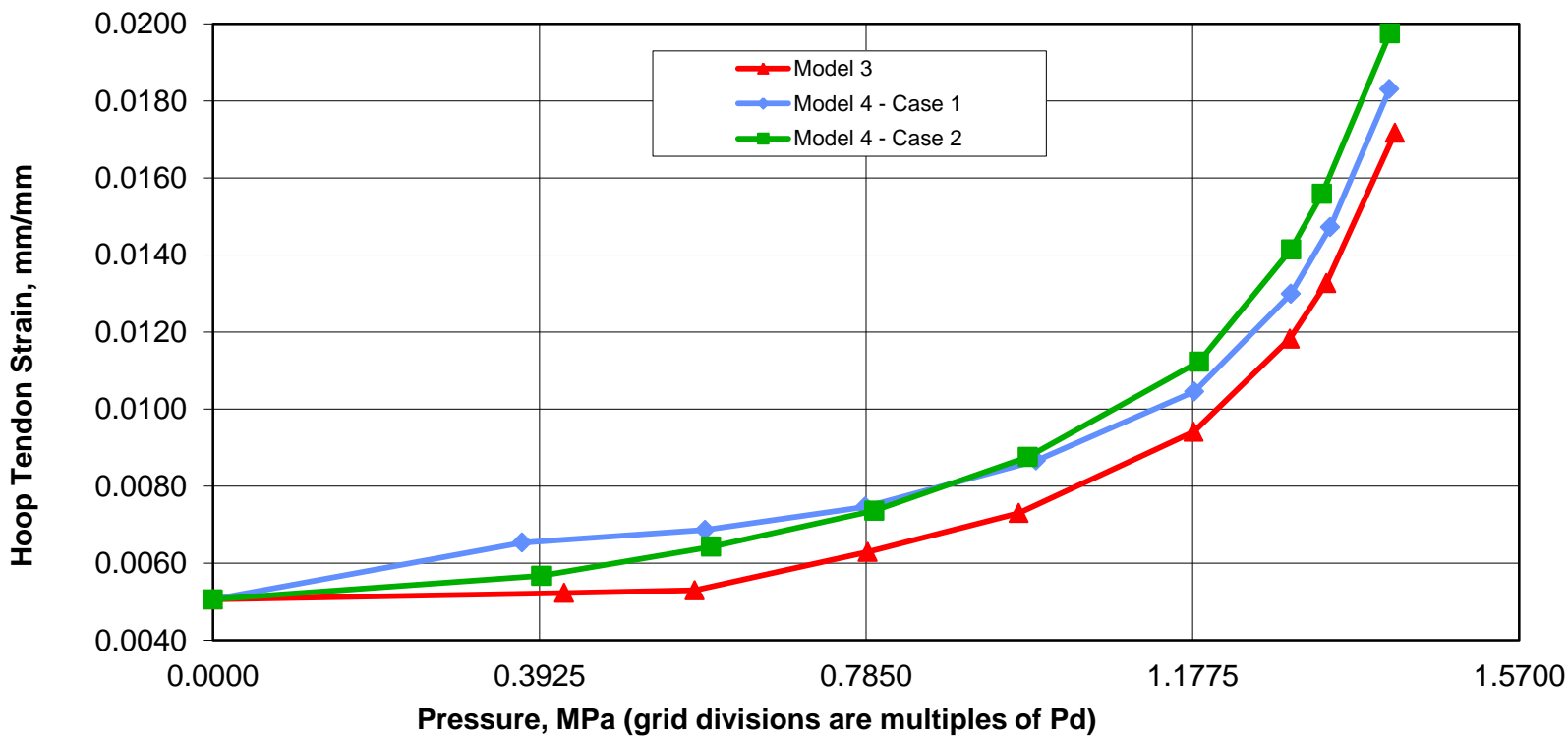


Standard Output Location: #51. Azimuth: 180 Degrees, Elevation: 6.56 Meters,
Tendon H53, 1/4 Tendon



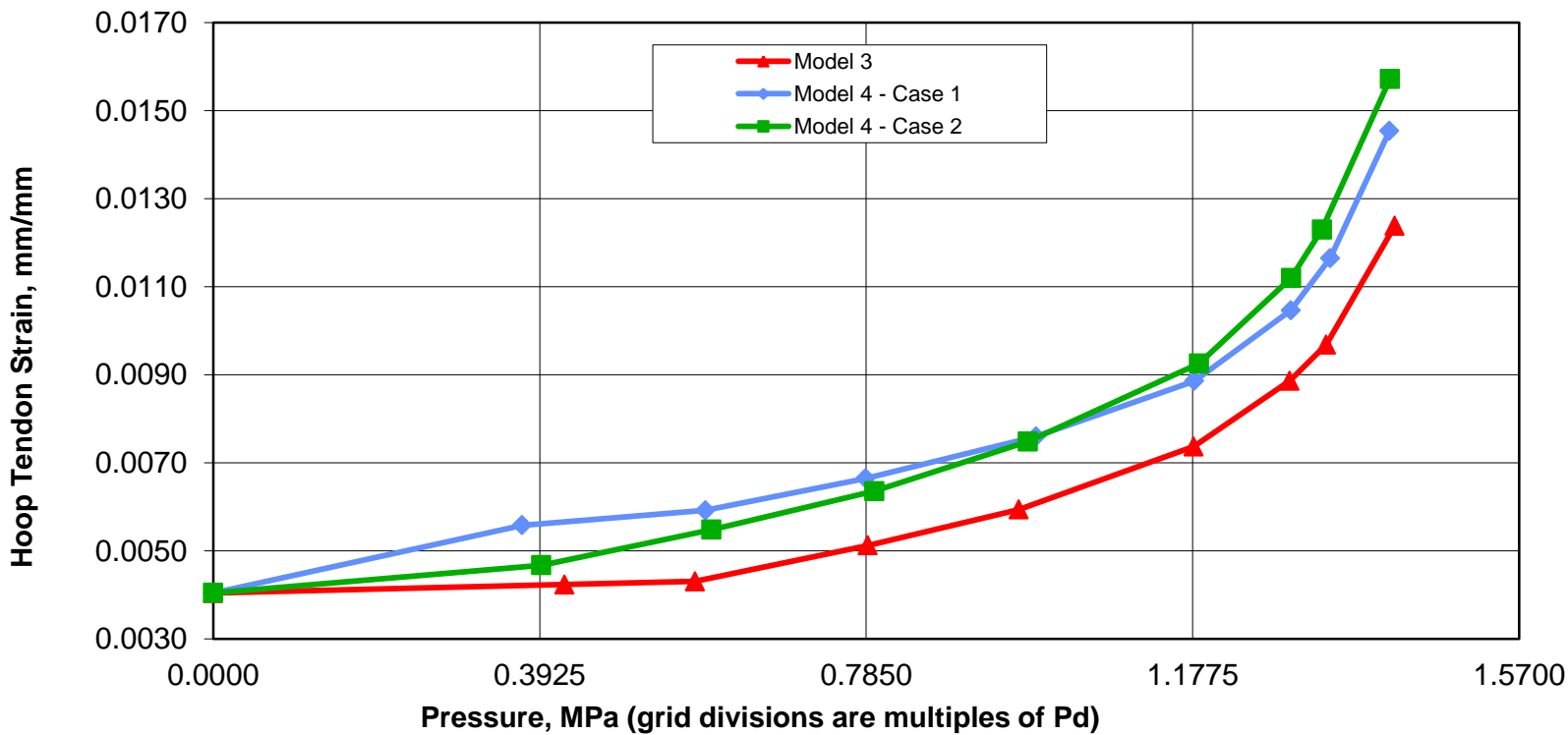


Standard Output Location: #52. Azimuth: 280 Degrees, Elevation: 6.58 Meters,
Tendon H53, Tendon Near Buttress



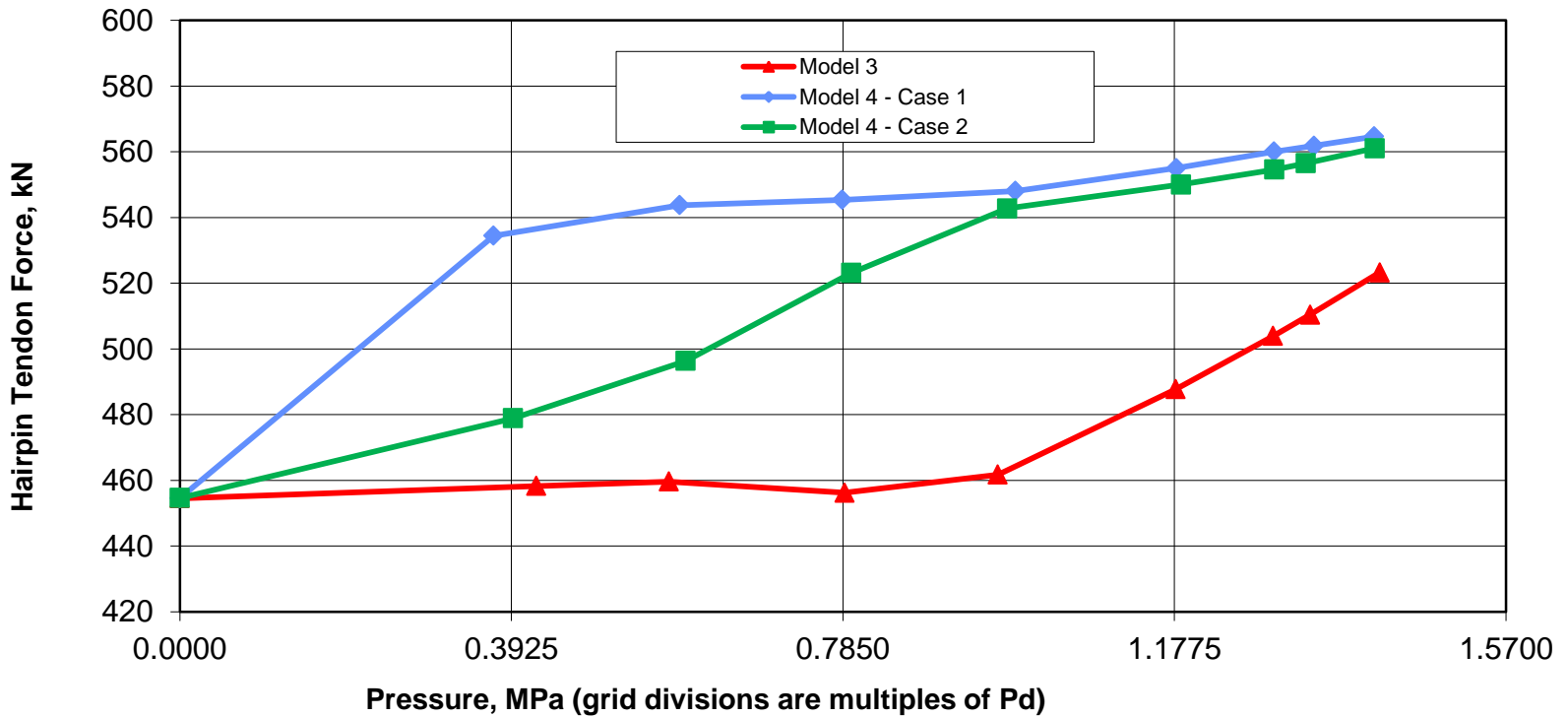


Standard Output Location: #53. Azimuth: 0 Degrees, Elevation: 4.57 Meters,
Tendon H35, Tendon between E/H and A/L



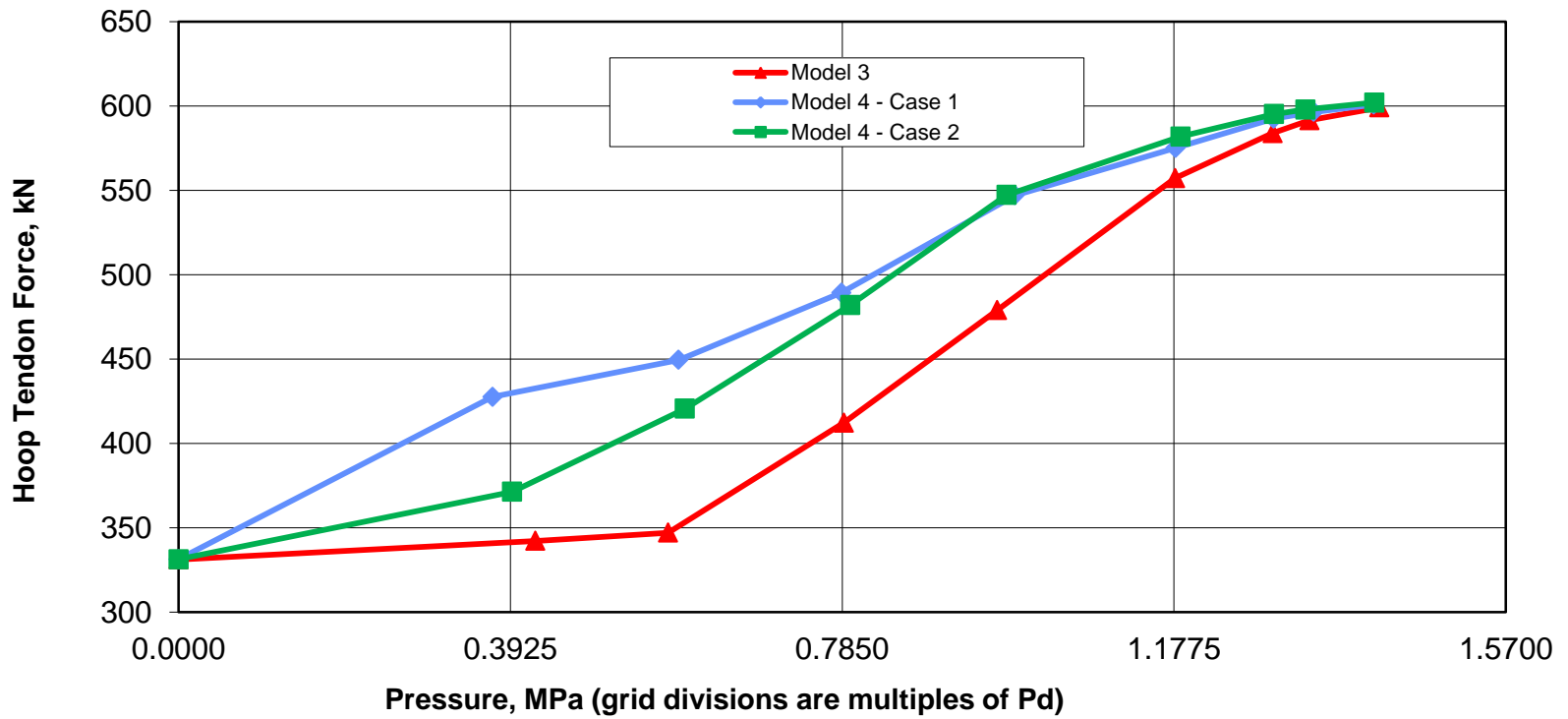


Standard Output Location: #54. Azimuth: 241 Degrees, Elevation: -1.16 Meters,
Tendon V37, Tendon Gallery





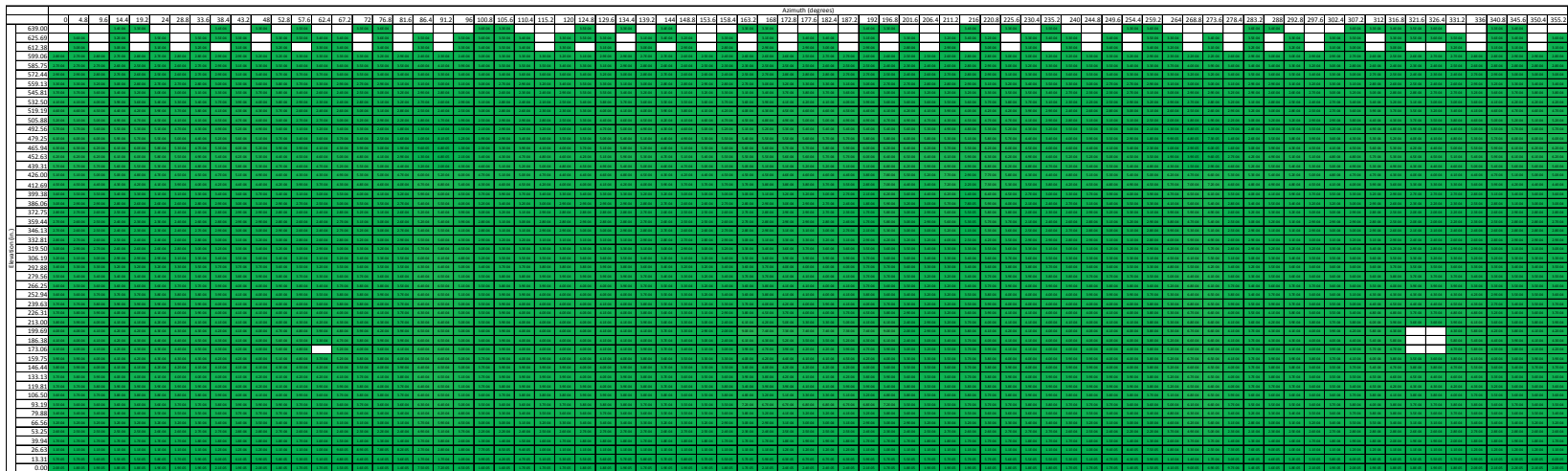
Standard Output Location: #55. Azimuth: 275 Degrees, Elevation: 6.58 Meters,
Tendon H53, at Buttress



Liner Strain Mapping

Case 2 – Blackout Station

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



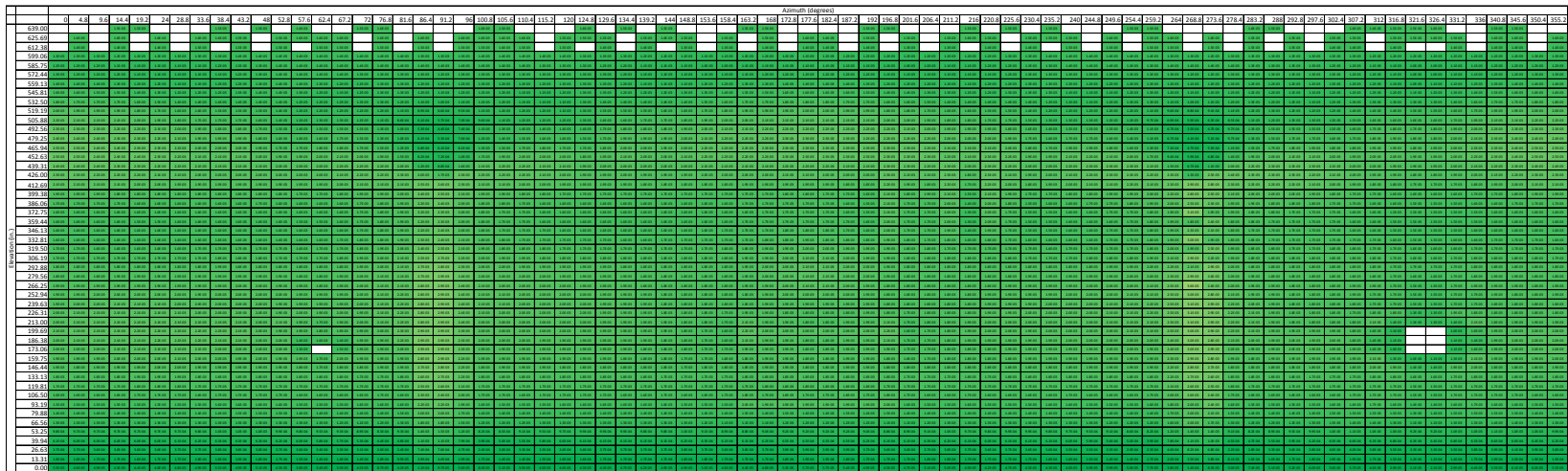
Strain Map of Entire Liner Surface at 1.0xPd



Liner Strain Mapping

Case 2 – Blackout Station

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



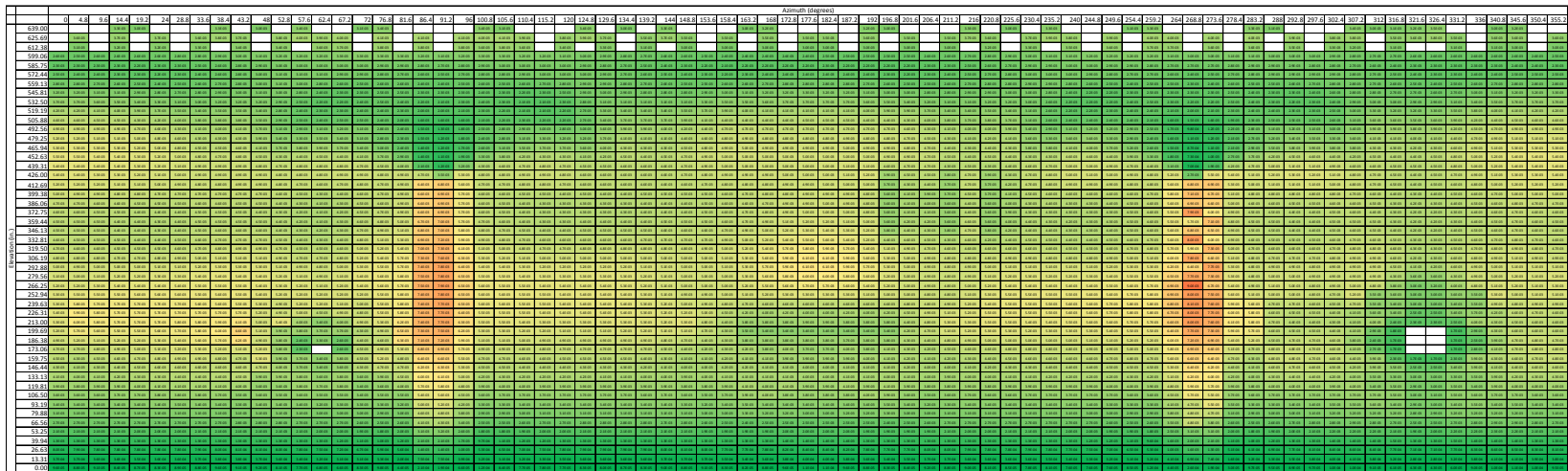
Strain Map of Entire Liner Surface at 2.0xPd



Liner Strain Mapping

Case 2 – Blackout Station

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



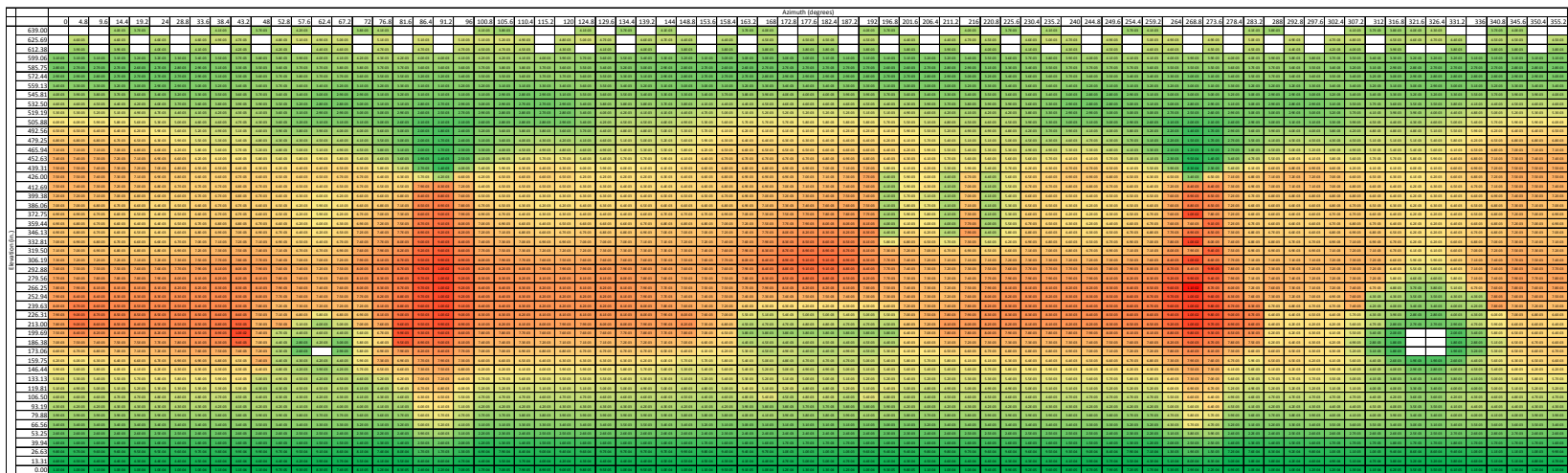
Strain Map of Entire Liner Surface at 3.0xPd



Liner Strain Mapping

Case 2 – Blackout Station

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



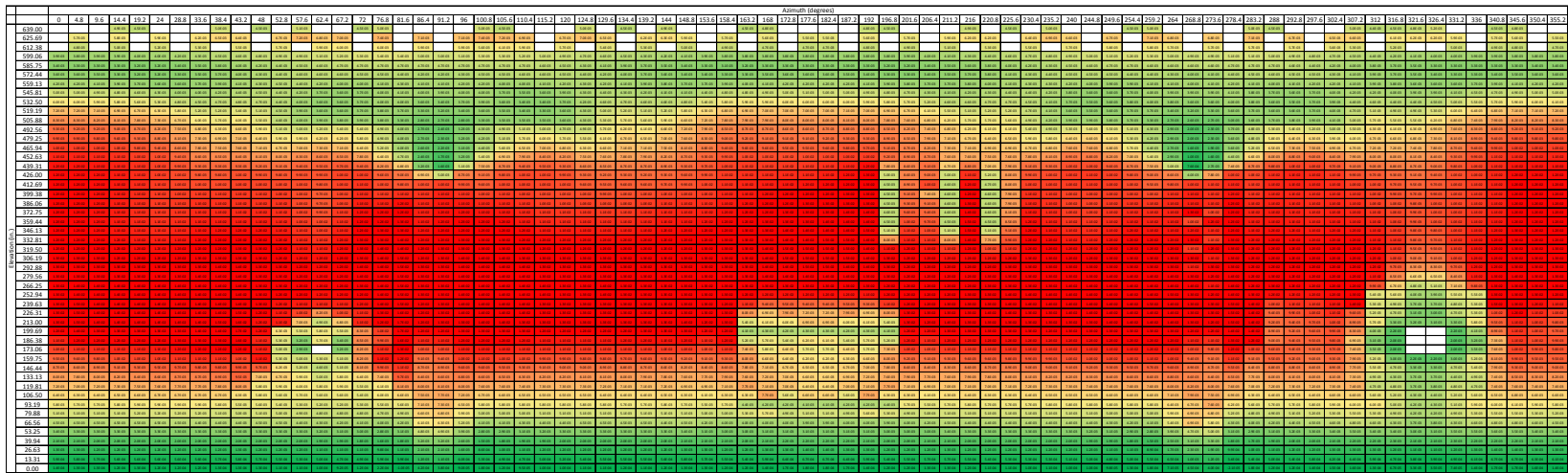
Strain Map of Entire Liner Surface at 3.3xPd



Liner Strain Mapping

Case 2 – Blackout Station

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



Strain Map of Entire Liner Surface at 3.6xPd





ISP #48 Summary of Conclusions (similar for SPE3 Phase 2)

- a. *With addition of temperature, would the onset of leakage occur later in the pressure history and, possibly, closer to the burst pressure?***
- Results predict failure at both lower (NNC, DEA, SCANSCOT-1) and higher (FORTUM, SCANSCOT-2) pressure when temperature is considered.
 - Both pressure causing liner tearing (leakage) and structural failure (rupture) are reduced(?)
 - The margin between leak and rupture does not appear to change significantly
 - Change in ‘failure’ pressures are generally small (<10%).
 - Consideration of ‘realistic’ severe accident scenario (Case 2) yields lower ‘failure’ pressure than saturated steam conditions(?).
 - Effects of material degradation are significant for ‘realistic’ severe accident scenarios.
- b. *How would including the effect(s) of accident temperatures change the prediction of failure location and failure mode?***
- While leak or rupture pressures are not significantly changed (reduced?), displacements are significantly greater, especially when considering material property degradation.
 - Case 1: Vertical displacements increase
 - Case 2: Radial displacements increase
 - Failure at penetrations appear more likely, and may control, under combined pressure and temperature loading.





Model 4 Leakage Rate Problem Definition & Leakage Rate Prediction Presentation





Strain-Based Failure Criteria

- **Fracture and tearing of the steel shell is followed by leakage through the tear aperture, and then through cracks in the concrete**
- **Concrete cracks are certain to occur at containment wall strains large enough to tear the steel shell**
- **Strain-failure criterion is the primary method used for this analysis based on its widely used application from previous analysis on concrete containment severe accident studies**





Leak Area Prediction Method

- **The calculation of local strain near discontinuities which cause liner tears requires localized modeling of the liner, concrete, rebar, and liner anchorage using specialized material and computational models**
- **While these techniques have been developed and extensively utilized, their use is not cost effective for examining all possible tearing locations of individual containments on a case-by-case basis**
- **FEA techniques were used in conjunction with a liner tearing criterion, to develop a database of liner strain concentration factors and thereby construct a simplified analysis procedure for predicting leakage in concrete containments**
- **a framework for this developed in 1990-1992 with EPRI funding**





Stepwise Approach from Global Strains to Tear Prediction

1. ‘Global’ strains are transformed to an equivalent peak uniaxial strain at a discontinuity location.

$$- \varepsilon_p = K B \varepsilon_{\text{global}}$$

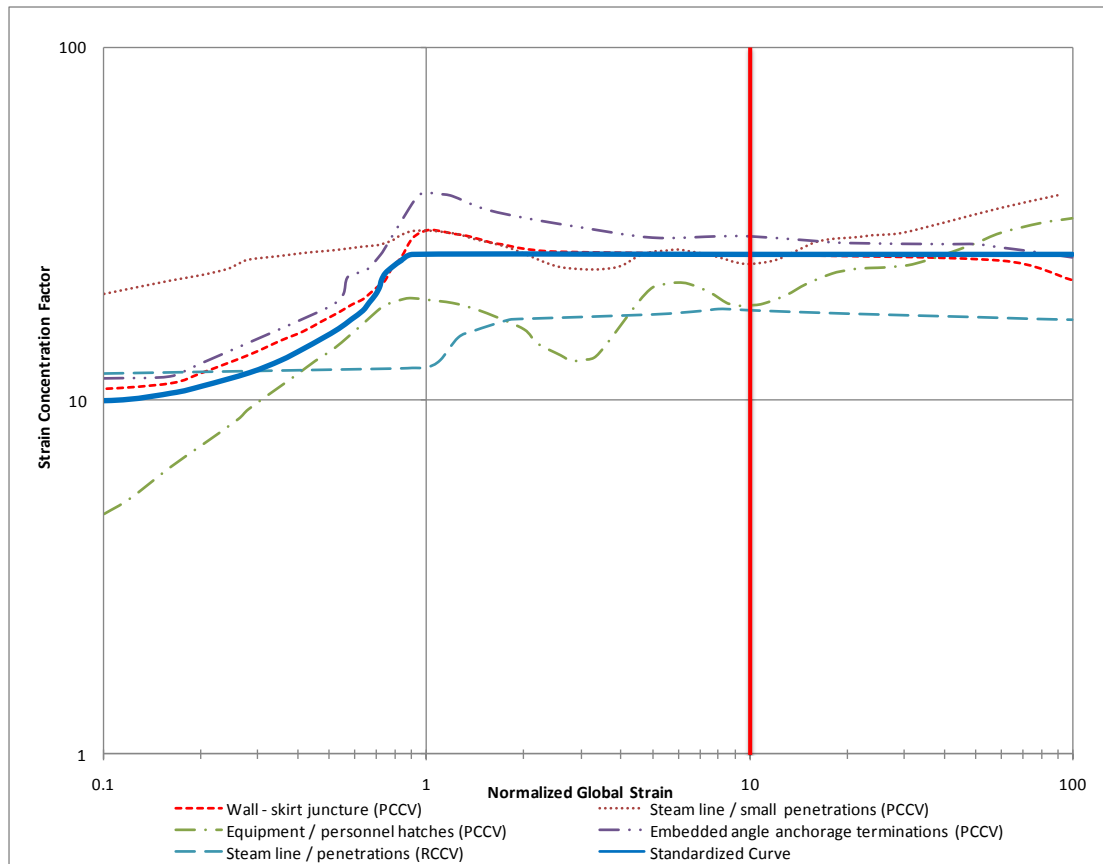
where K is the strain concentration factor

B is a stress biaxiality factor

2. K is associated with stiffness discontinuity. The value we adopted is from five fundamental strain concentration factor curves developed in the EPRI program for typical locations of liners.
3. After global strain begins to yield, the strain concentration versus global strain stabilizes with an average value of $K=25$; we used this to define the shape of the K-curve.



Stepwise Approach from Global Strains to Tear Prediction (cont)



K, Strain Concentration Factors at various locations around the PCCV





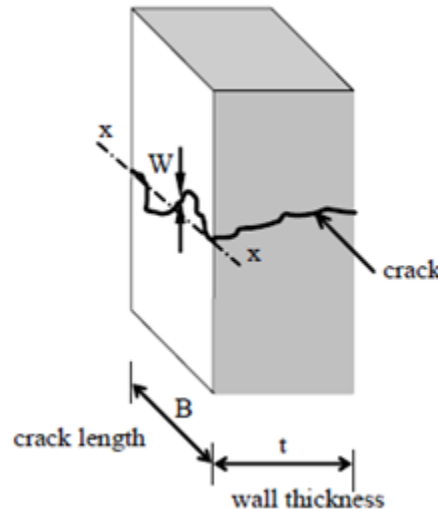
Stepwise Approach from Global Strains to Tear Prediction (cont)

4. **Biaxiality coefficient, B is the reciprocal of the Ductility Ratio which is used to magnify strain:**
 - **$B = 1/\mu = 1/\text{ductility ratio}$**
 - **ranges from $1.0 \leq B \leq 2.0$ where 1.0 is perfectly uniaxial stress state to 2.0 is 1:1 biaxial stress state, $\sigma_3 = 0$**
 - **Ductility ratio is defined by Davis triaxiality factor, TF published by Manjoine:**
 - **$\mu = 2^{(1-TF)}$**
 - **$TF = (\sigma_1 + \sigma_2) / (\sigma_1^2 - \sigma_1\sigma_2 + \sigma_2^2)^{1/2}$**
where σ_1 and σ_2 are the principal stresses
5. **Solve for ϵ_p . If peak strain is $\geq 21\%$, a tear is likely to occur.**

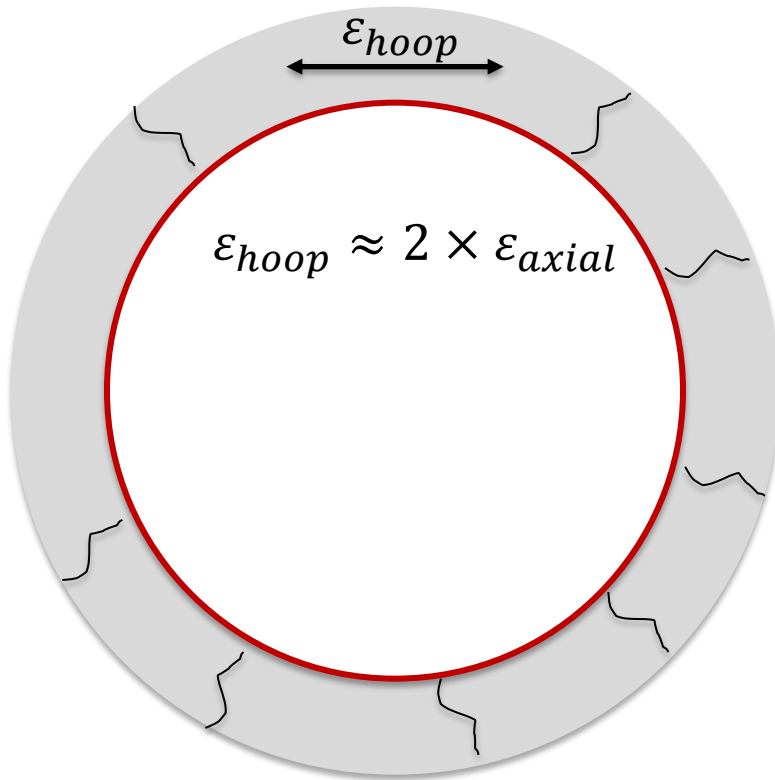


Stepwise Approach from Global Strains to Tear Prediction (cont)

- Determine crack width, assuming average crack width occurs over the spacing between anchors
 - $W_{avg} = \epsilon_{global}$ times spacing between anchors
- Applying the Rizkalla method to transform average crack width to leak area prediction was used as the formula is applicable for wide range of pressure differences

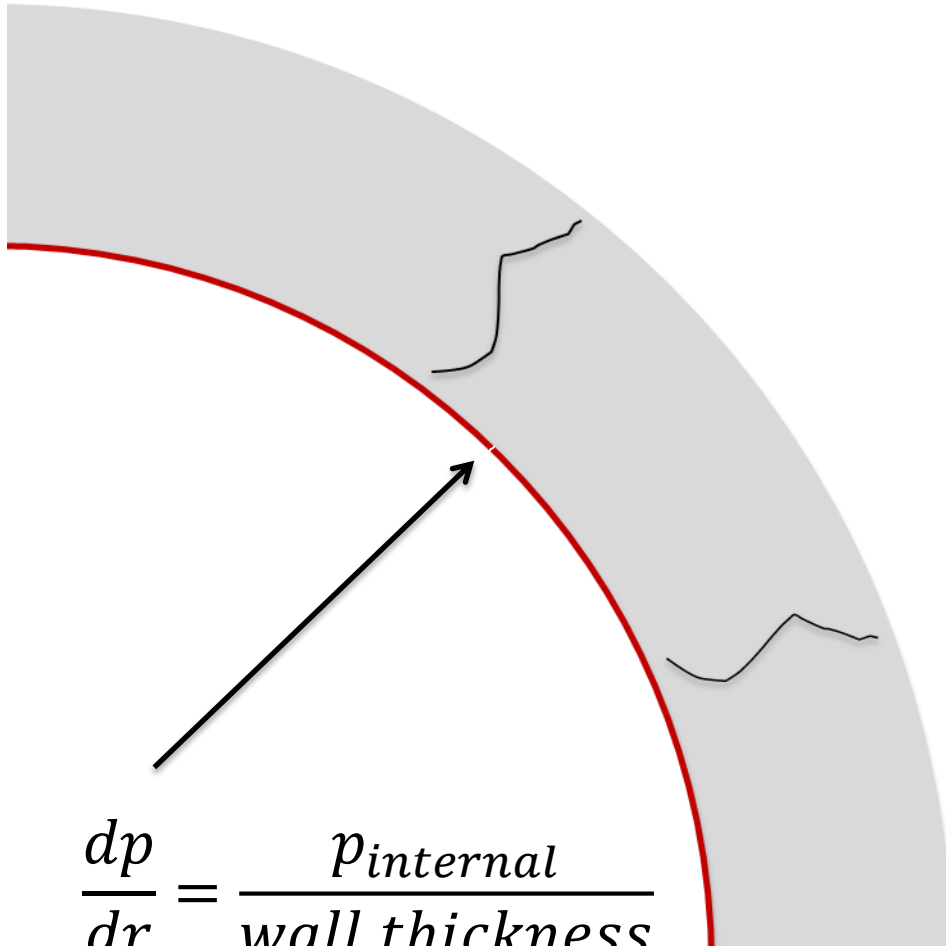


Prior to initial leakage



- **Dilation of the PCCV**
- **Initial cracking of the concrete**
 - Likely coordinated with vertical tendon ducts
 - Hoop tendons carry the load
- **Liner intact**
 - Liner yielding in localized areas

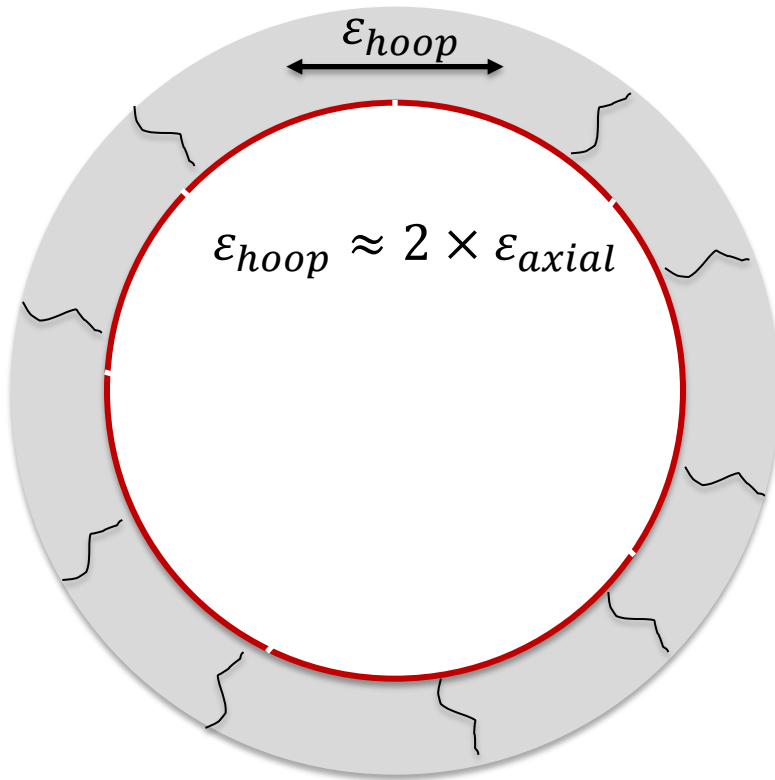
Initial leakage



- Initial tearing of the liner
- Gas flows through the concrete
 - Through the material
 - Through cracks



Terminal leakage



- **Widening of concrete cracks**
- **Flow rate increases with**
 - Wider cracks
 - Greater $\frac{dp}{dr}$
- **Additional liner tearing**
- **Pressurization increases until**
 - $Q_{out} = Q_{in}$



Quantifying 'Q'

- Various sources in the literature to characterize flow
 - Suzuki, et al.
 - Rizkalla, et al.
 - Others
- Rizkalla et al. chosen for accuracy and applicability

$$\frac{p_1^2 - p_2^2}{t} = \left(\frac{k^n}{2}\right) \left(\frac{\mu}{2}\right)^n (RT)^{n-1} \left|\frac{p_2 Q}{B}\right|^{2-n} \frac{1}{\sum_{i=1,j} W_j^3}$$

$$\sum_{i=1,j} W_j^3 = 1.42 NW_{av}^3$$

$$n = \frac{0.195}{(NW_{av}^3)^{0.063}}$$

$$k = 8.702 \times 10^6 (NW_{av}^3)^{0.367}$$

Predicting Leakage Rate Proposed by Rizkalla

$$\frac{p_1^2 - p_2^2}{t} = \left(\frac{k^n}{2}\right) \left(\frac{\mu}{2}\right)^n (RT)^{n-1} \left|\frac{p_2 Q}{B}\right|^{2-n} \frac{1}{\sum_{i=1,j} W_j^3},$$

where, $\sum_{i=1,j} W_j^3 = 1.42 N W_{av}^3$ and $N = \text{number of cracks}$ and $W_{av} = \text{average crack width}$

$$n = \frac{0.133}{(\sum W_i^3)^{0.81}} = \frac{0.195}{(N W_{av}^3)^{0.063}} \text{ and } k = 2.907 \times 10^7 (\sum W_i^3)^{0.428} = 8.702 \times 10^6 (N W_{av}^3)^{0.367}$$

Where, $Q = \text{flux through the wall (ft}^3/\text{s)}$, $B = \text{crack length (ft)}$, $W = \text{crack width (ft)}$, $t = \text{wall thickness}$, $p_1 = \text{upstream pressure (lb/ft}^2)$, $p_2 = \text{downstream pressure (lb/ft}^2)$, $\mu = \text{dynamic viscosity of air or gas used (lb s/ ft}^2)$, $T = \text{absolute temperature (}^\circ \text{ R)}$, $R = \text{gas constant (sqft/s}^2 \text{ }^\circ \text{ R)}$. W_{av} is the average crack width of the total concrete section of interest. Typical values of μ and R are $1.80 \times 10^{-5} \text{ Pa-s}$ and $1716 \text{ sqft/s}^2 \text{ }^\circ \text{ R}$ respectively.





Estimating Leakage Rate

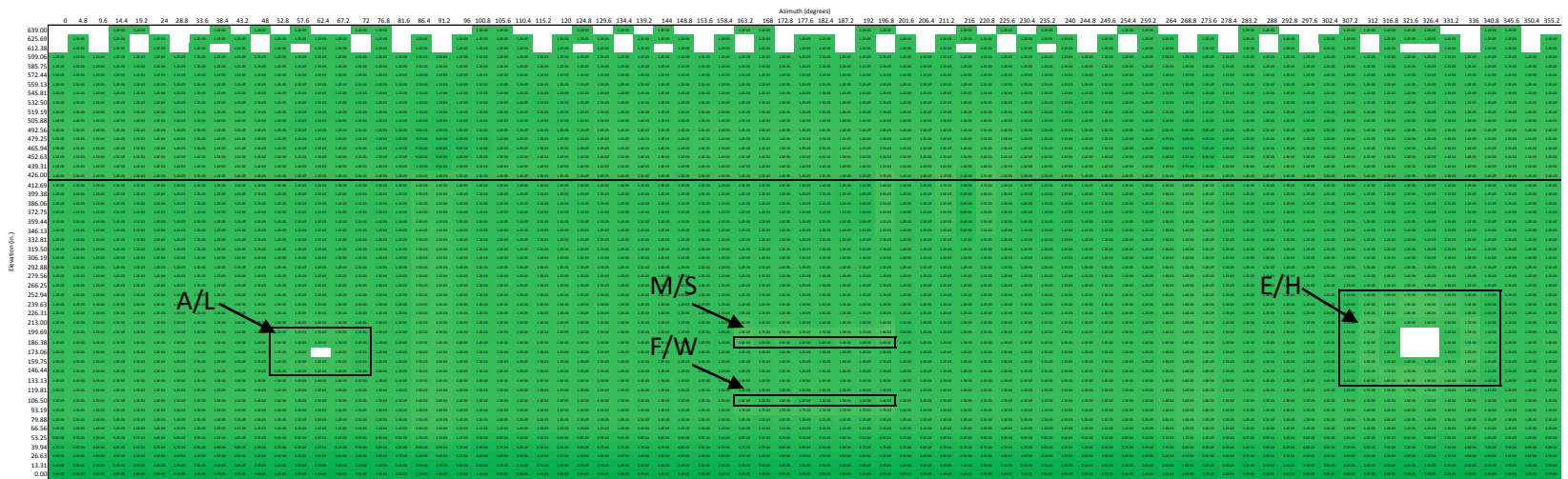
- **Leakage rate is determined for Model 3 and Model 4, Case 1 and 2 at various pressure milestones along the entire liner surface**
- **Color-coded strain mapping and leakage rate mapping is performed through Excel**



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



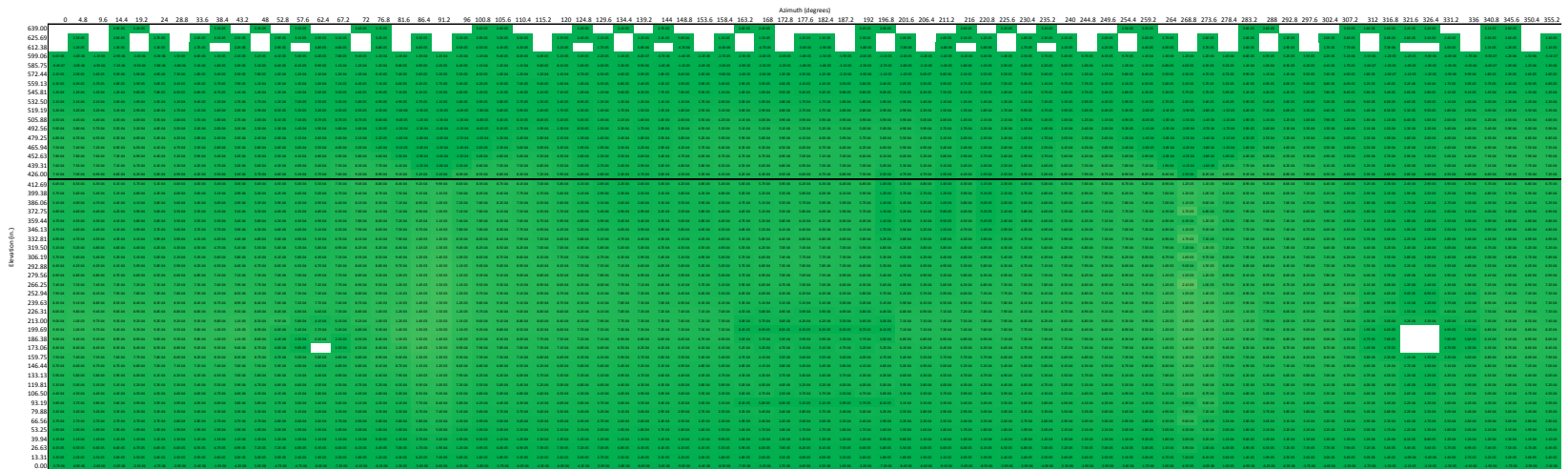
Strain Map of Entire Liner Surface at 1.0xPd



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



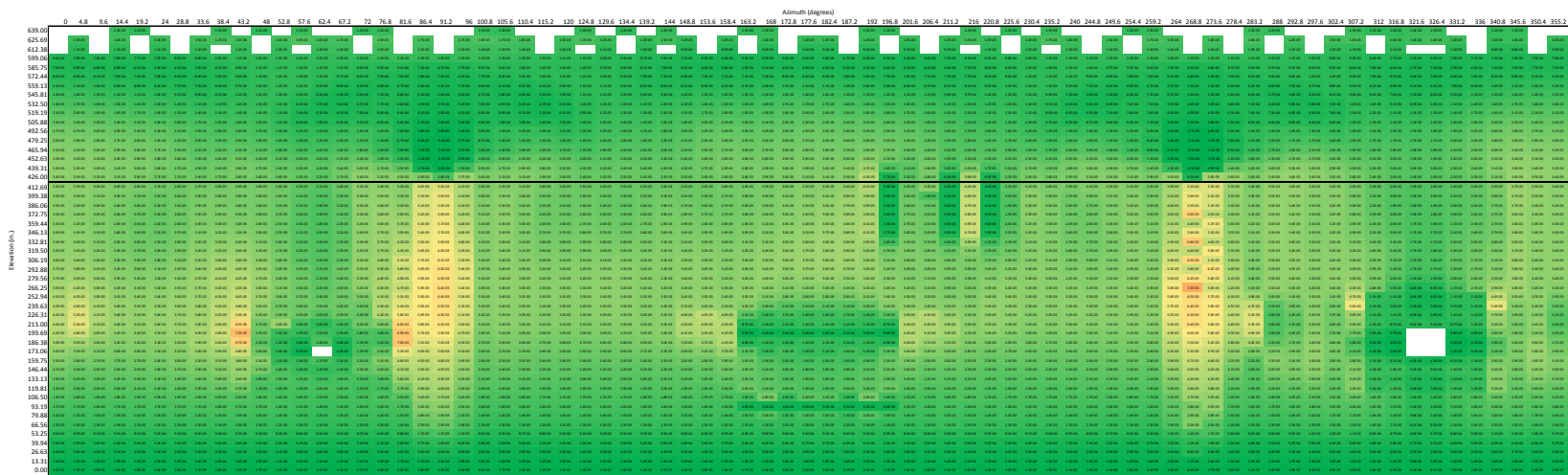
Strain Map of Entire Liner Surface at 2.0xPd



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



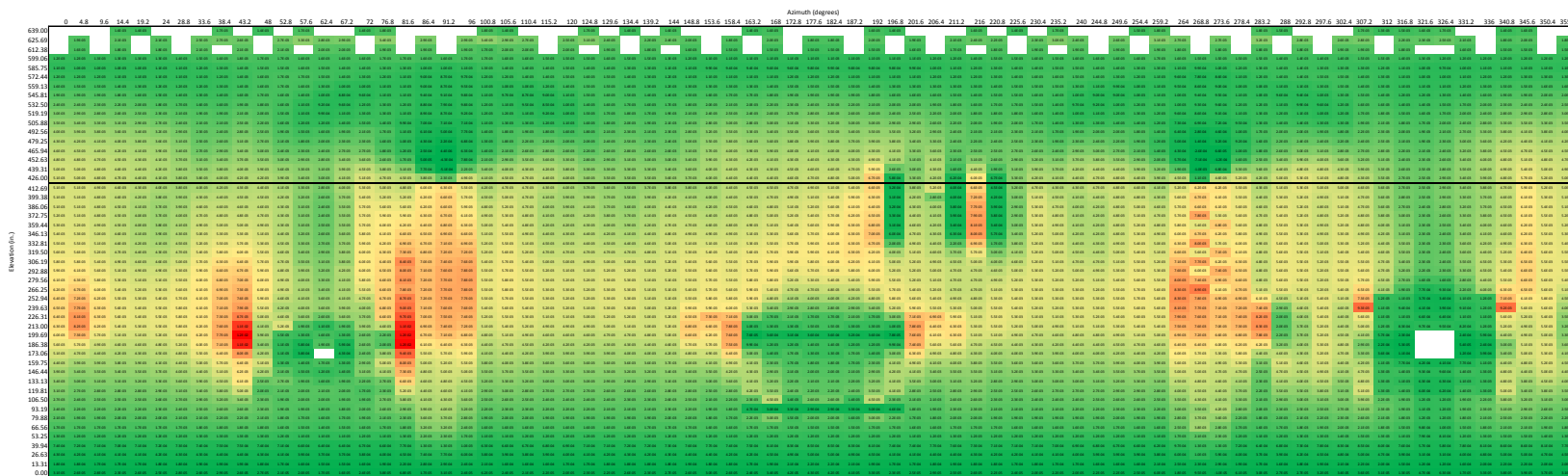
Strain Map of Entire Liner Surface at 3.0xPd



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red



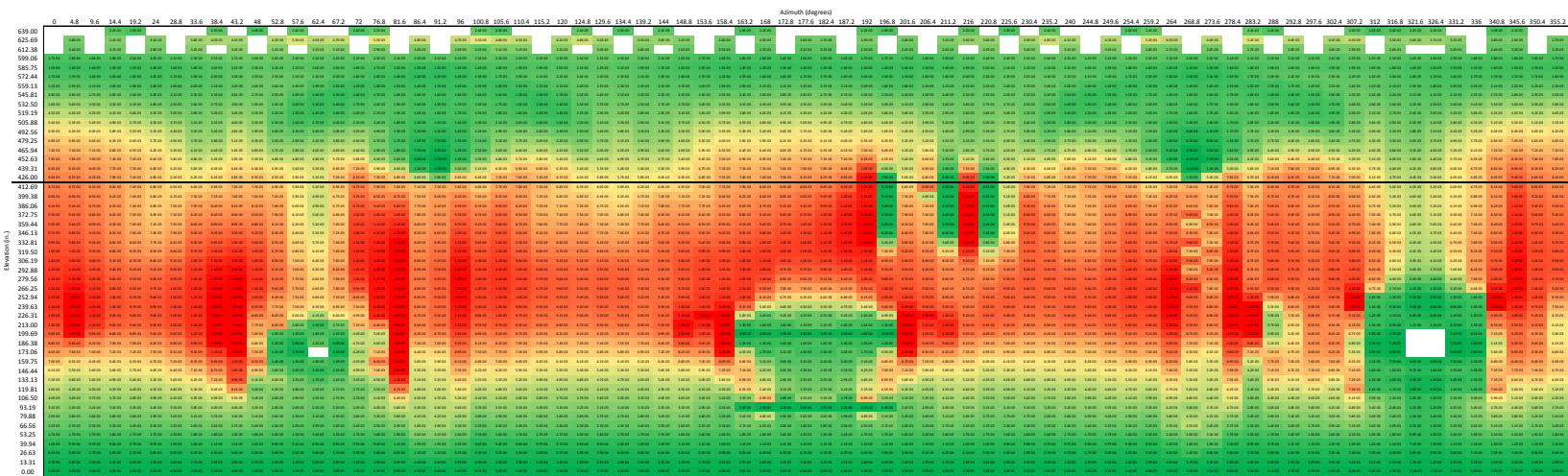
Strain Map of Entire Liner Surface at 3.3xPd



Liner Strain Mapping

Model 3 – Pressure Only Case

Color codes	
Strain	Color
$0 \leq \epsilon < 0.006$	green
$0.006 \leq \epsilon < 0.012$	yellow
$\epsilon \geq 0.012$	red

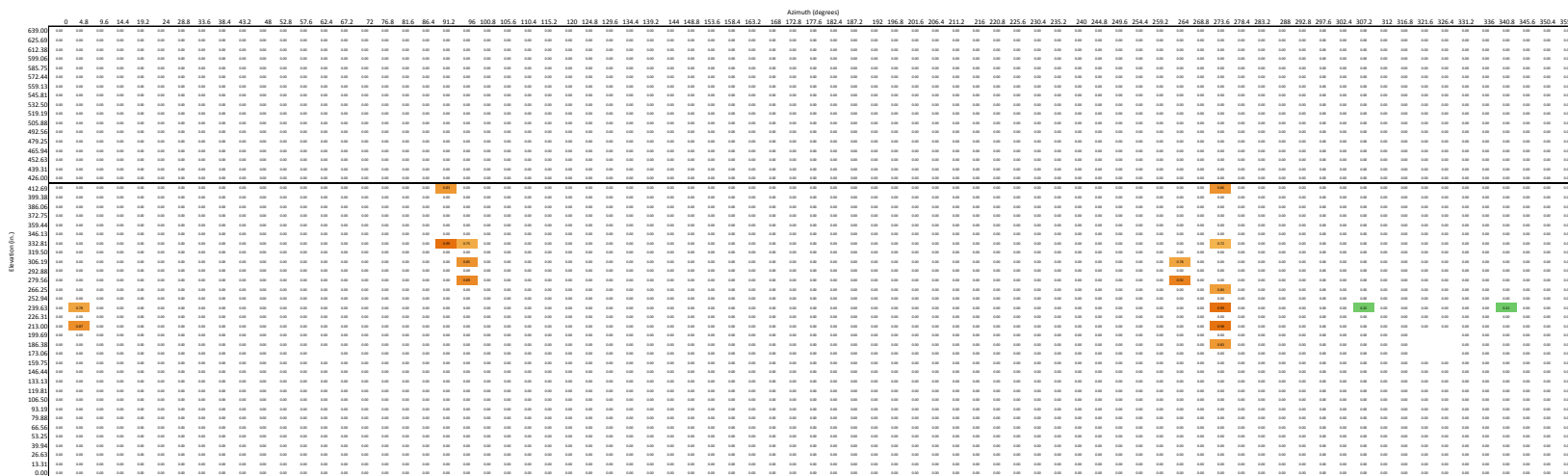


Strain Map of Entire Liner Surface at 3.6xPd



Leakage Rate Mapping Model 3 – Pressure Only Case

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

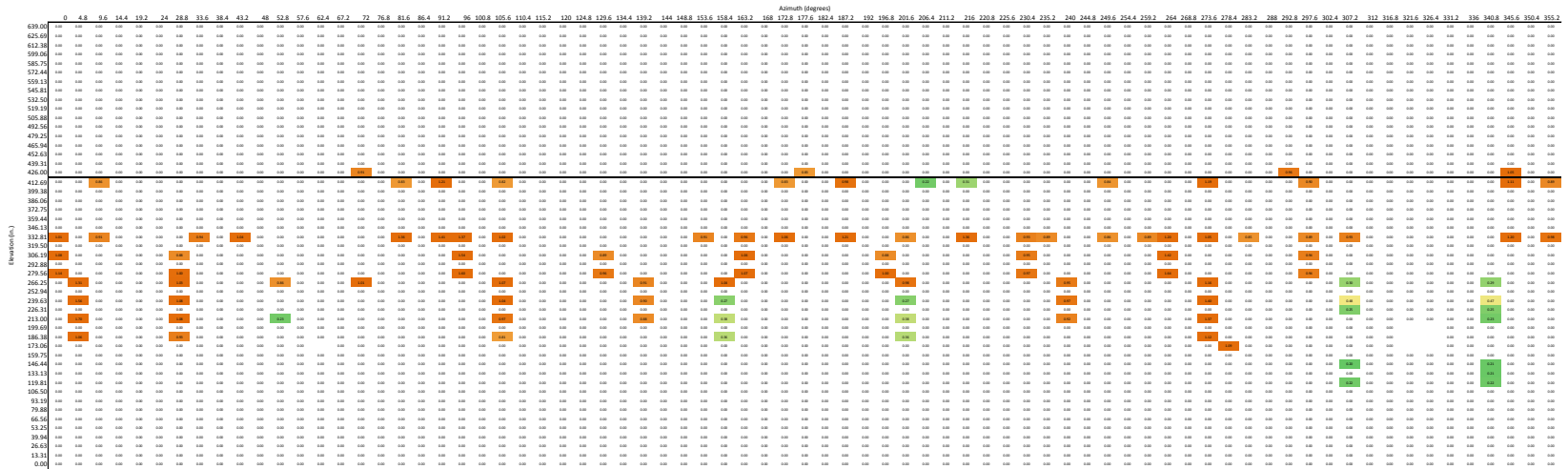


Mapping of Leakage Rate of Entire Liner Surface at 3.0xPd



Leakage Rate Mapping Model 3 – Pressure Only Case

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

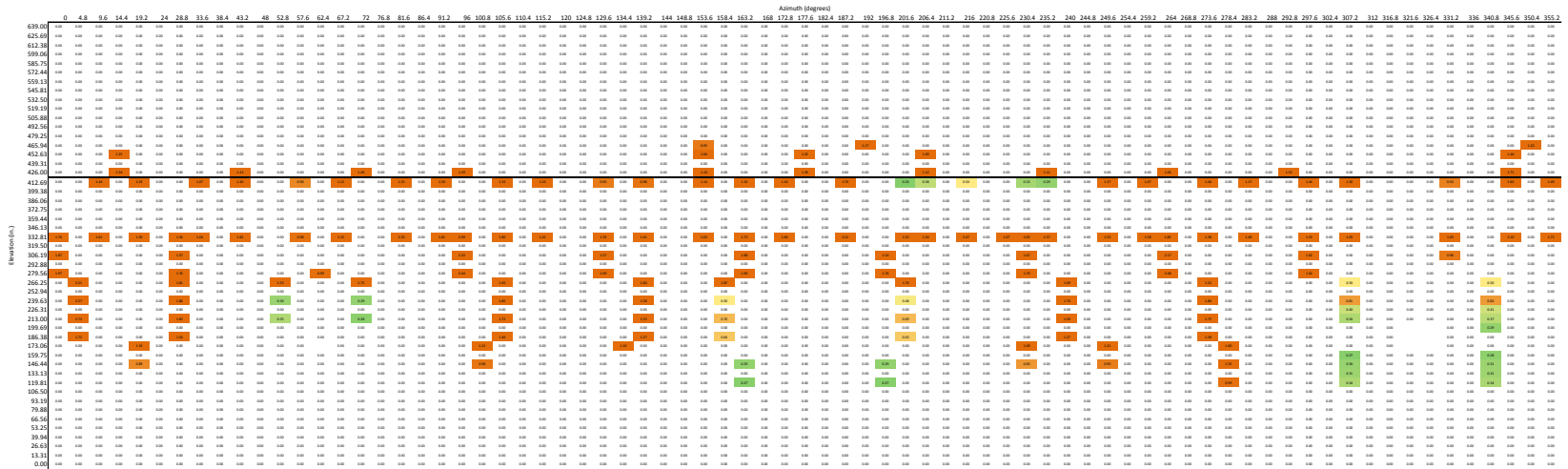


Mapping of Leakage Rate of Entire Liner Surface at 3.3xPd



Leakage Rate Mapping Model 3 – Pressure Only Case

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

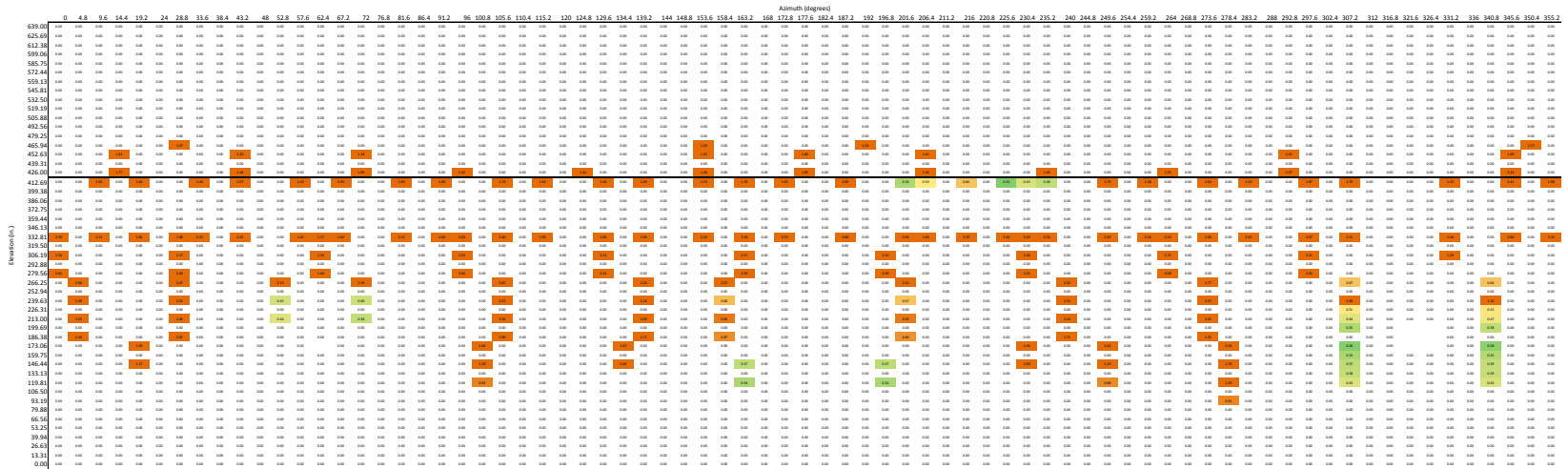


Mapping of Leakage Rate of Entire Liner Surface at 3.5xPd



Leakage Rate Mapping Model 3 – Pressure Only Case

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange



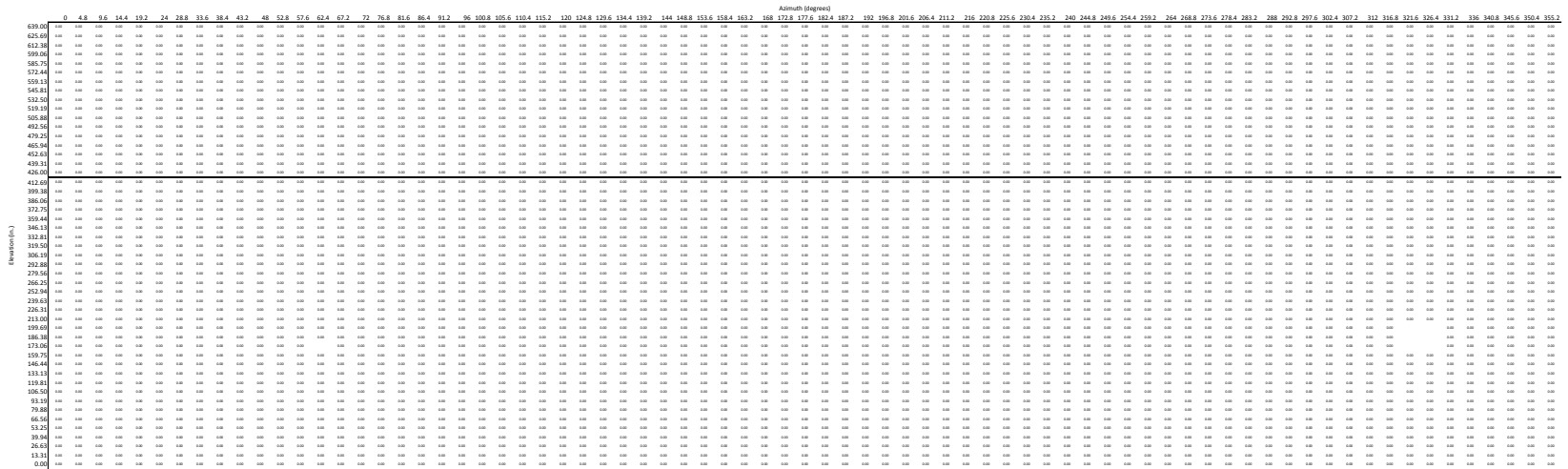
Mapping of Leakage Rate of Entire Liner Surface at 3.6xPd



Leakage Rate Mapping

Case 1 – Saturated Steam Condition

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange



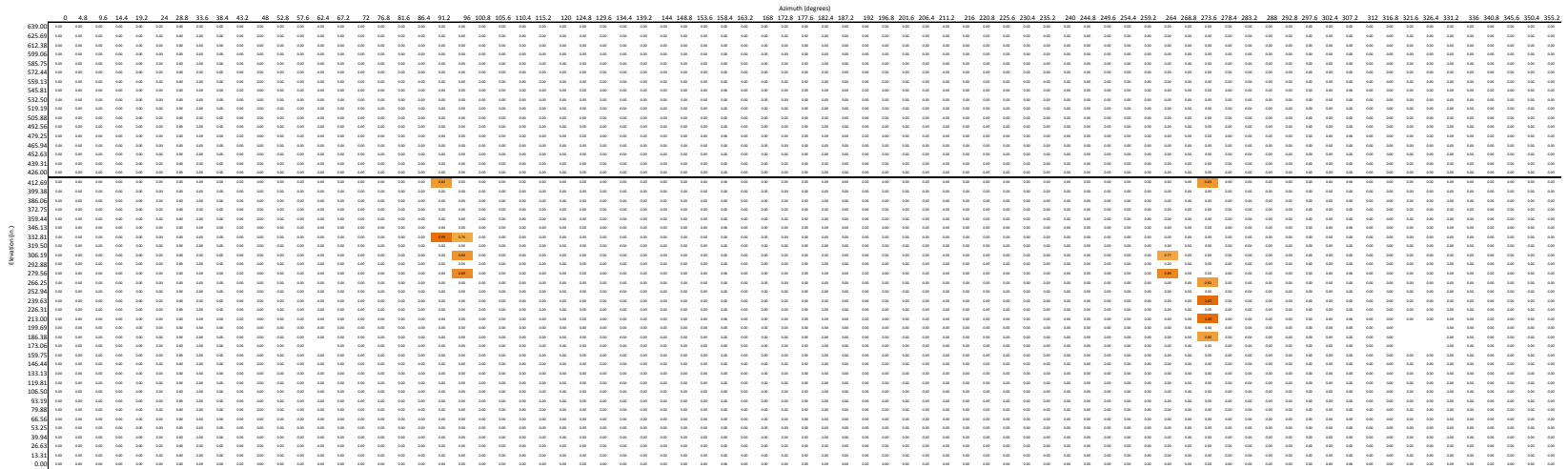
Mapping of Leakage Rate of Entire Liner Surface at 3.0xPd



Leakage Rate Mapping

Case 1 – Saturated Steam Condition

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange



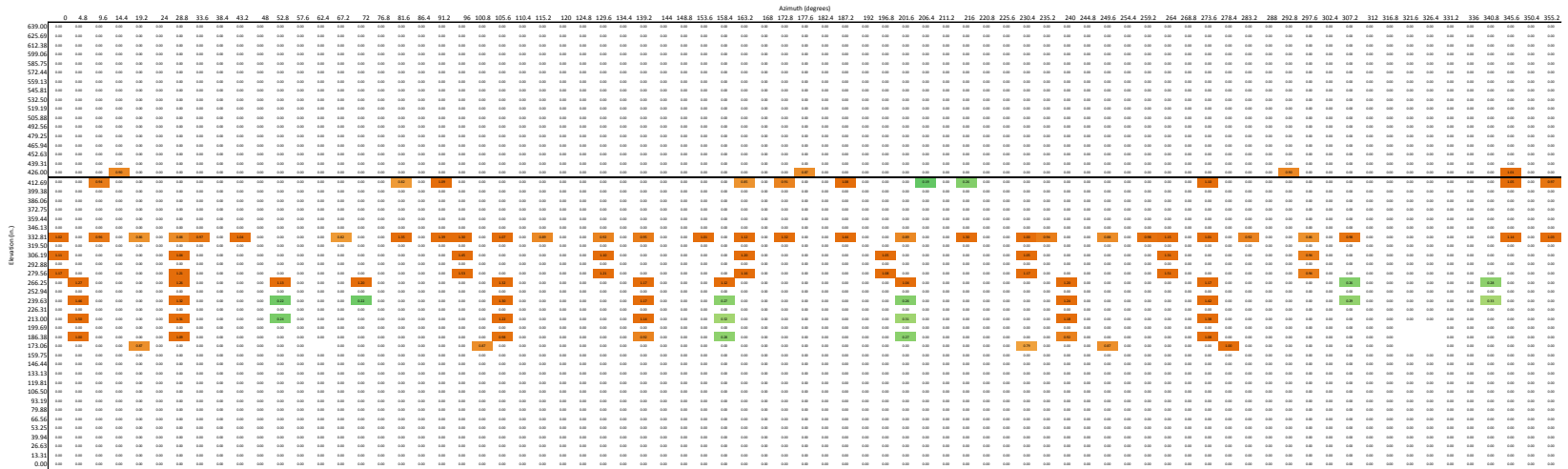
Mapping of Leakage Rate of Entire Liner Surface at 3.3xPd



Leakage Rate Mapping

Case 1 – Saturated Steam Condition

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange



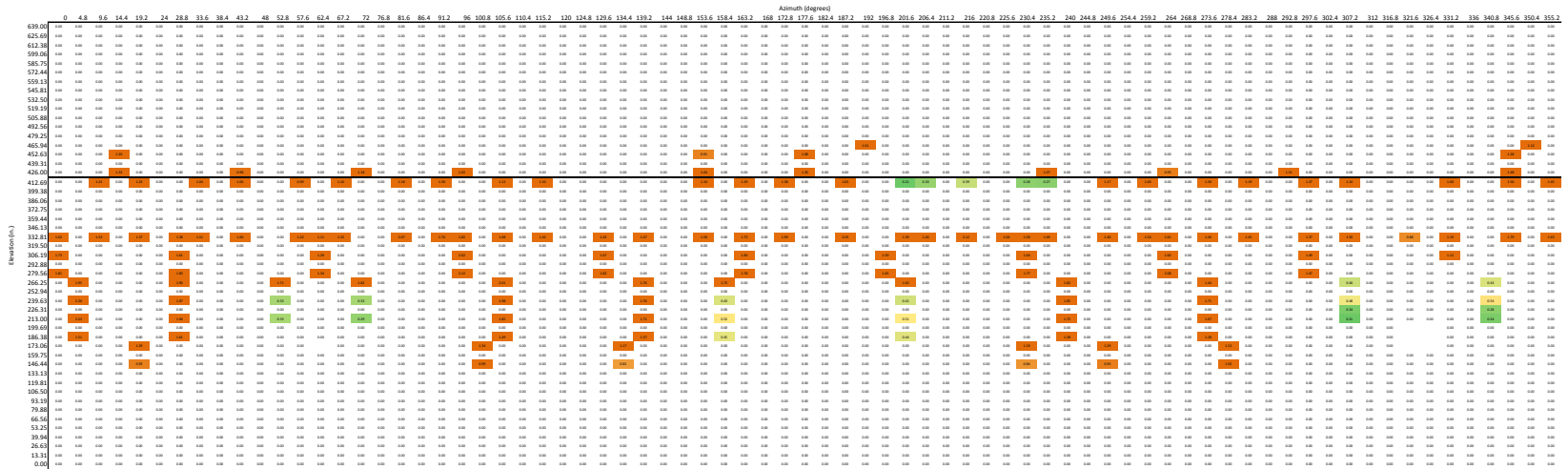
Mapping of Leakage Rate of Entire Liner Surface at 3.5xPd



Leakage Rate Mapping

Case 1 – Saturated Steam Condition

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

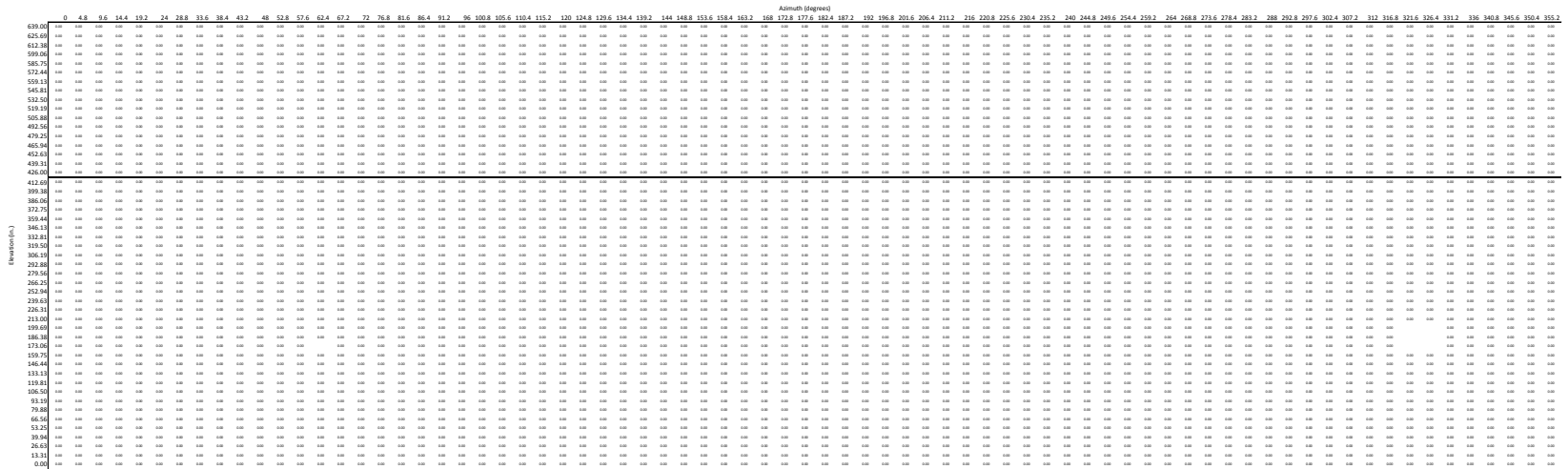


Mapping of Leakage Rate of Entire Liner Surface at 3.6xPd



Leakage Rate Mapping Case 2 – Blackout Station

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

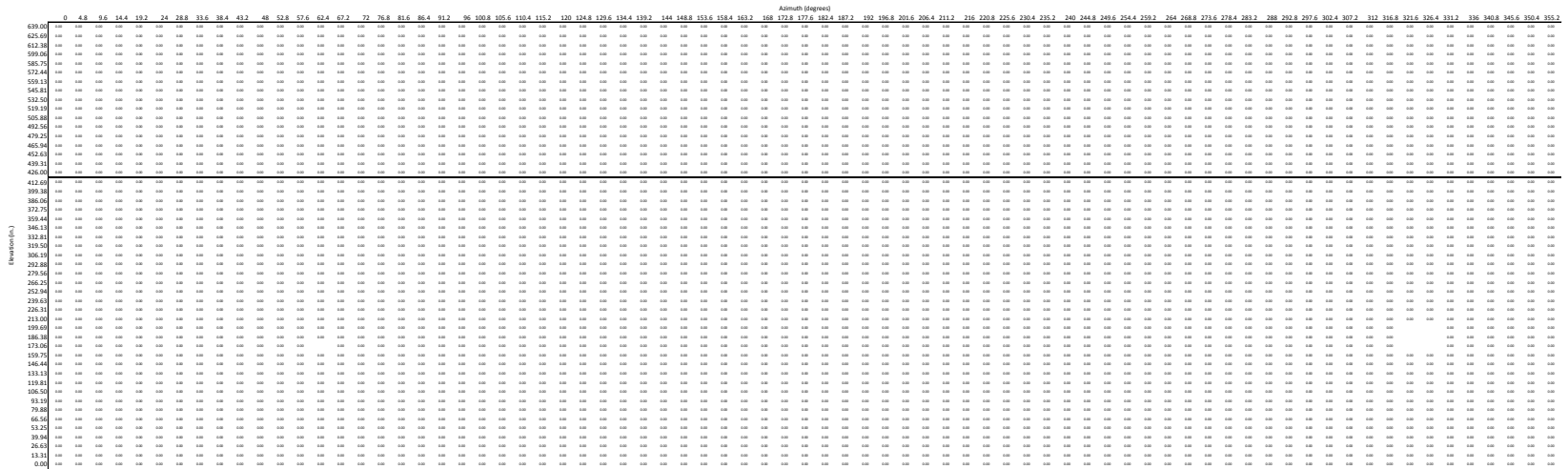


Mapping of Leakage Rate of Entire Liner Surface at 3.0xPd



Leakage Rate Mapping Case 2 – Blackout Station

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

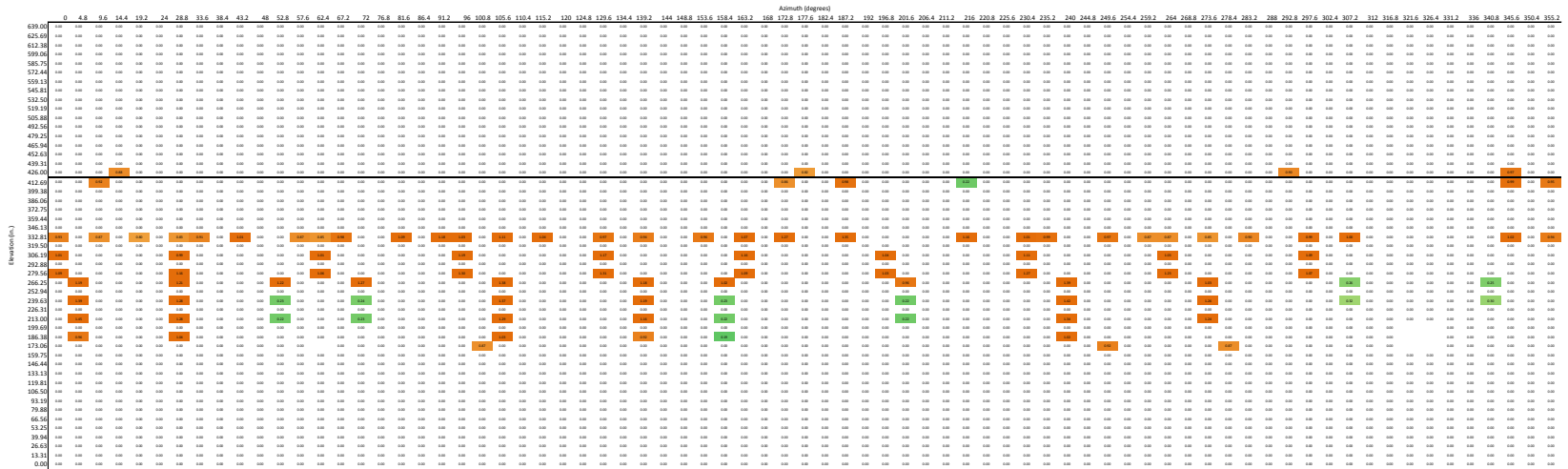


Mapping of Leakage Rate of Entire Liner Surface at 3.3xPd



Leakage Rate Mapping Case 2 – Blackout Station

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange

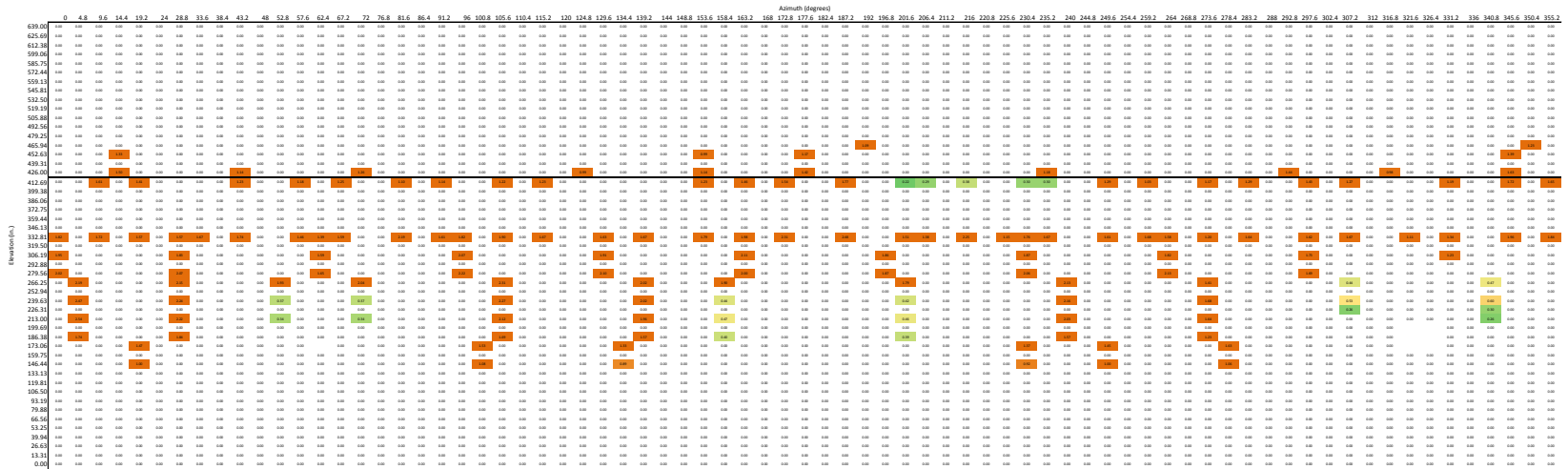


Mapping of Leakage Rate of Entire Liner Surface at 3.5xPd



Leakage Rate Mapping Case 2 – Blackout Station

Color codes	
Leakage rate (ft ³ /s)	Color
$Q \leq 0$	white
$0 < Q < 0.5$	green
$0.5 \leq Q < 1.0$	yellow
$Q \geq 1.0$	orange



Mapping of Leakage Rate of Entire Liner Surface at 3.6xPd

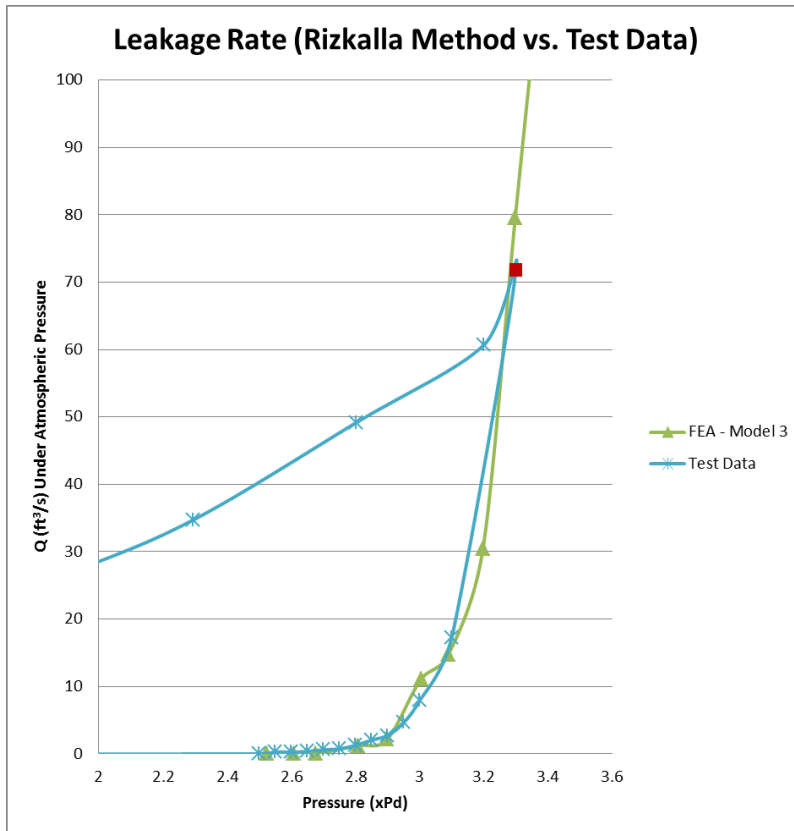


Comparison Amongst Models

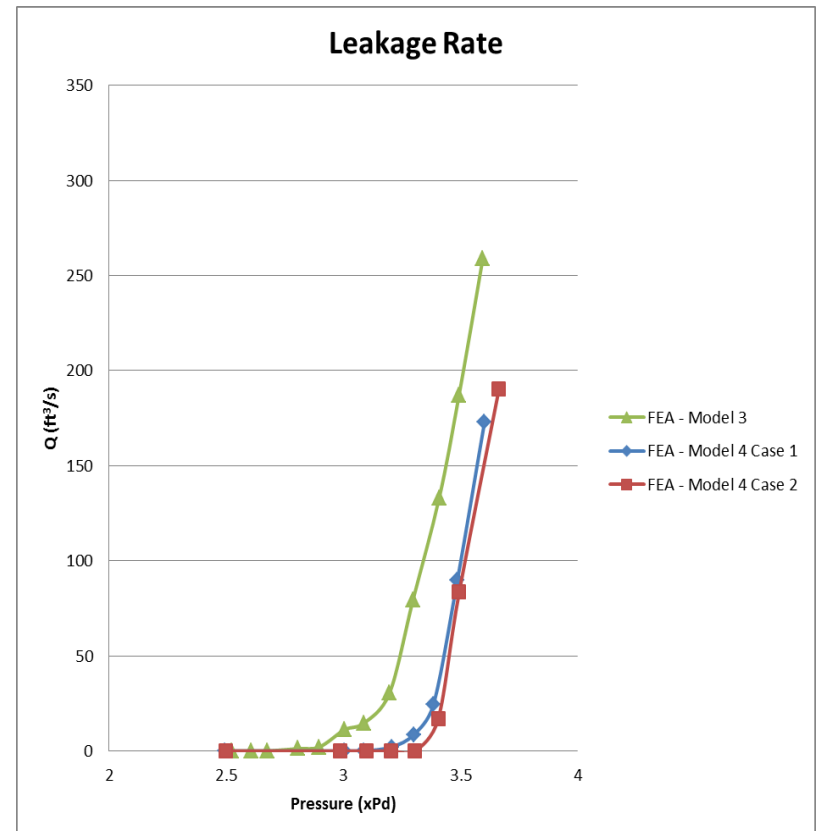
Leakage Rate Comparison			
	Q (ft ³ /s)		
Pressure (xPd)	Model 3 - Pressure Only	Model 4 - Case 1	Model 4 - Case 2
2.5	0	0	0
3.0	13	0	0
3.1	18	0	0
3.2	36	3	0
3.3	95	10	0
3.4	158	29	20
3.5	222	108	101
3.6	308	208	190



Leakage Rate versus Pressure



Leakage Rate Comparison between Rizkalla Method and Test Data



Leakage Rate Comparison amongst Cases



Analysis Results

- **Comparing Model 3 with the test data (peak leakage of 70 cu. ft / sec at 3.3xPd), the leakage rate prediction is reasonably close**
- **For Model 4, the leakage rates actually decrease, which is attributed to temperature effects**
- **As the temperature increases, the steel liner tries to expand at a faster rate than the concrete. The concrete has a lower coefficient, as well as a lower average temperature, so this retards the liner expansion, thus putting some compression into the liner. The compression helps prevent cracks from opening. (Note that mechanical strains, not thermal strains, have been used in the liner tearing prediction.)**
- **Temperature range does not significantly degrade the material properties, so material property degradation was not found to have a significant effect on the structure's capacity**





Liner Weld Irregularities

- **Visual observation showed extensive grinding and weld repair in liner welds where most of tears occurred.**
- **Ultrasonic measurements showed substantial reductions in thickness near these tears. Measurements showed ~23% thickness reductions in many locations, and more (up to 40% in a few locations).**
- **Localized plastic deformation occurred in association with many of the vertical field welds, particularly in the vicinity if the tears. No evidence of brittle fracture was seen**
- **Photos of the back side of the liner revealed irregularities (missing segments of back-up bars, discontinuous in horizontal stiffeners) associated with a number of the tears**



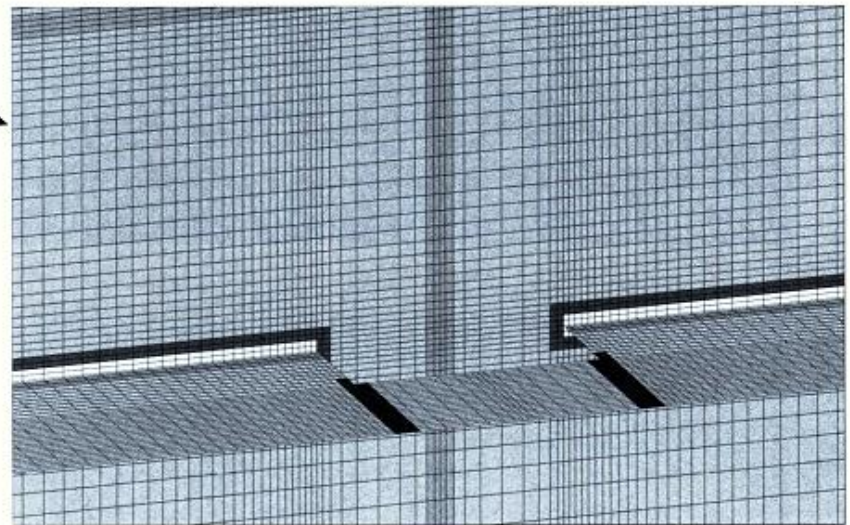
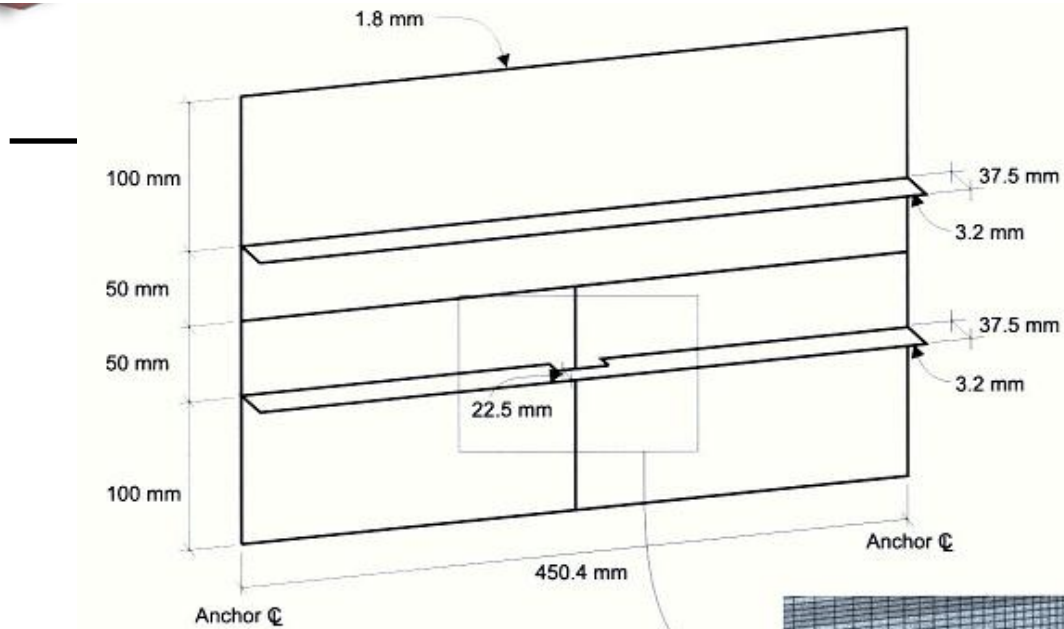
LST - Typical Tear Location

Liner Tear #16



(Image reversed for comparison)

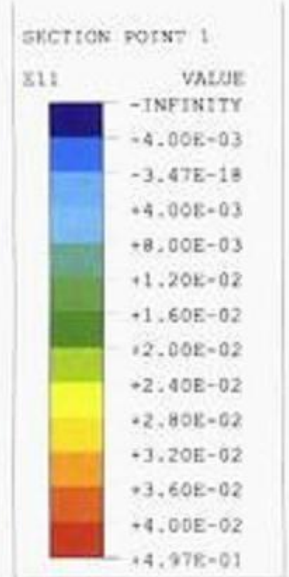
2001-2002 work: Local Line Seam Analysis Model



**Variations in Weld Zone,
HAZ Properties, Grinding
Thickness,
Stiffener Configurations**

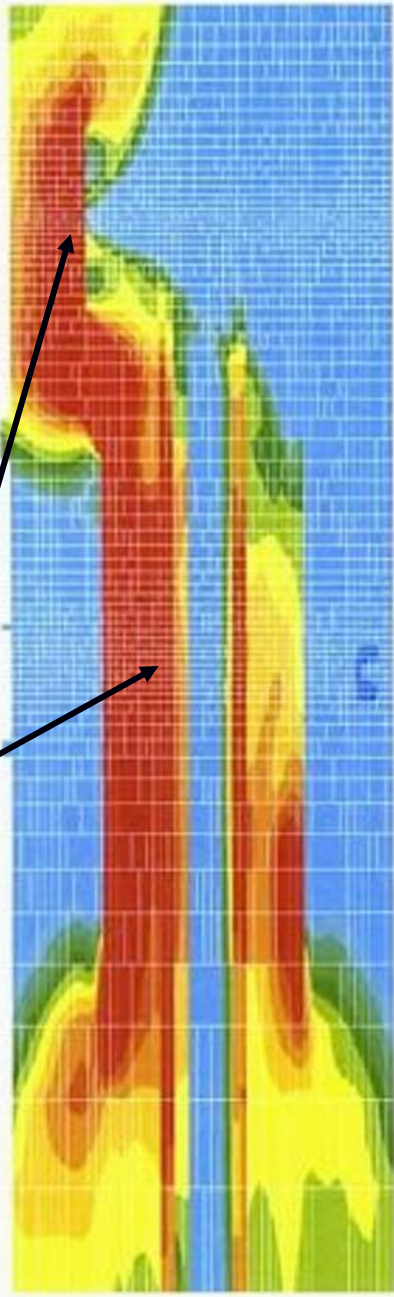
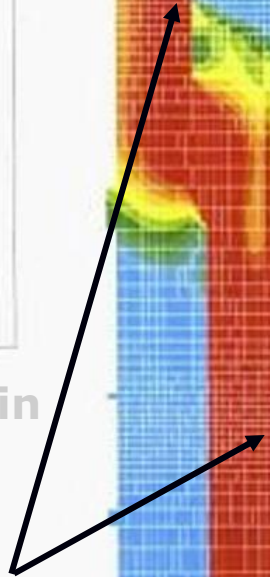


**2001-2002
Local Liner
Seam Analysis
Model
(Simulation
of Tear 16)**



49.7% Strain

**Strains Exceeding
Tear Criteria (~20%
Eff. Plastic strain)**





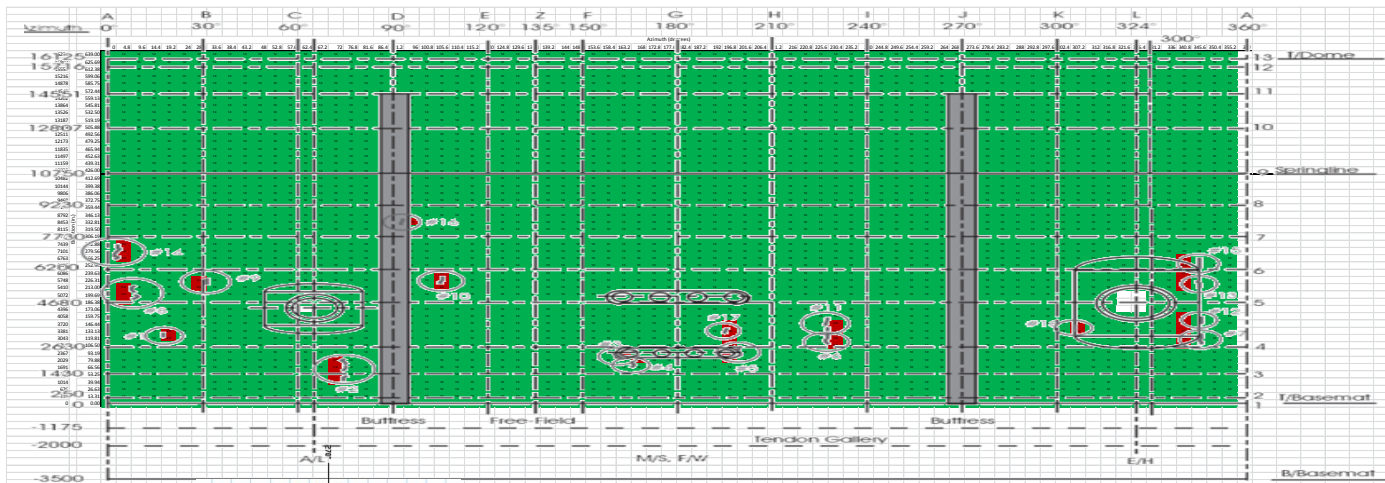
Liner Weld Irregularities (cont)

- **Mechanical testing showed only small strain localization in the weld heat affected zones – much less than observed in the liner base metal. Ultimate strength (~72 ksi) was not degraded by welding**
- **No evidence found of material problems that could account for premature tearing of the liner. Only one tear (1) was associated with a weld defect. This was a lack-of-fusion defect, not porosity in the fusion zone**
- **Metallography showed that nearly all of the tear areas had been ground at least 23%, both in repair welding and following repair welding**



Incorporating Liner Flaws

- One viable way of incorporating these defects is to modify K
- 1:4 Scale PCCV liner weld defects (grinding, inconsistent back-up bars, etc.) have the effect of approximately doubling “K”
- To show how this can be implemented, K has been doubled at all the observed tear locations

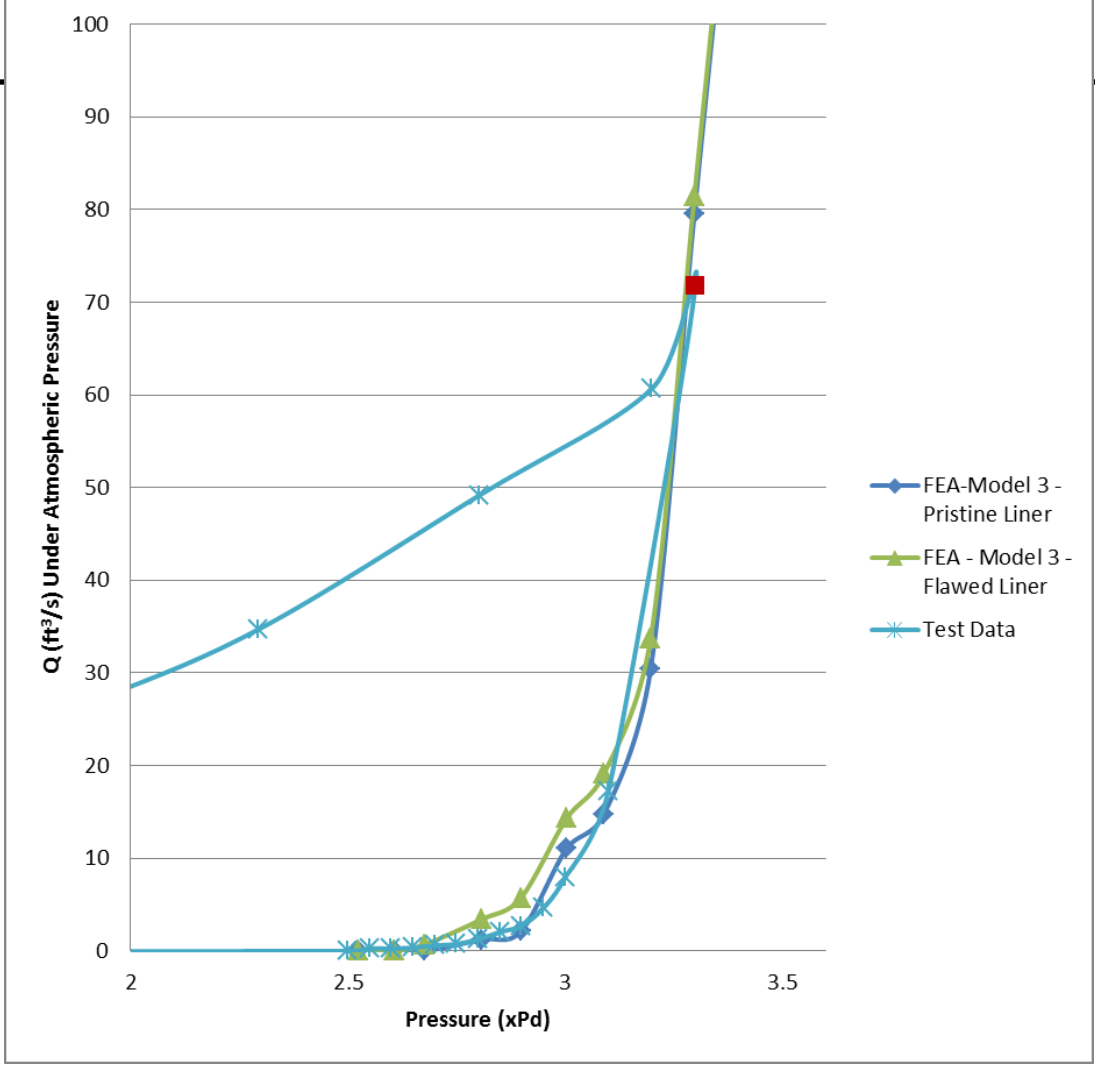


Double K Factor for Liner Flaws





Leakage Rate (Rizkalla Method vs. Test Data)





Adding Probabilistic Basis

- **The method lends itself well to adding a probabilistic basis**
 - similar to the preliminary developments in the EPRI work
 - first steps taken will be discussed in probabilistic presentation
- **All variables can be assumed to have lognormal distribution, then randomness and variability coefficients assigned through**
 - Statistical assessment of Liner material measurements and tests
 - Engineering judgment on the level of uncertainty in analysis

