Exceptional service in the national interest





Development of a novel thermo-mechanical model for simulating permafrost demise and Arctic coastal erosion

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Outline



- Motivation and background
- The Arctic Coastal Erosion (ACE) project
- Thermo-mechanical finite element model of permafrost
- Numerical results
- Summary
- Ongoing/future work

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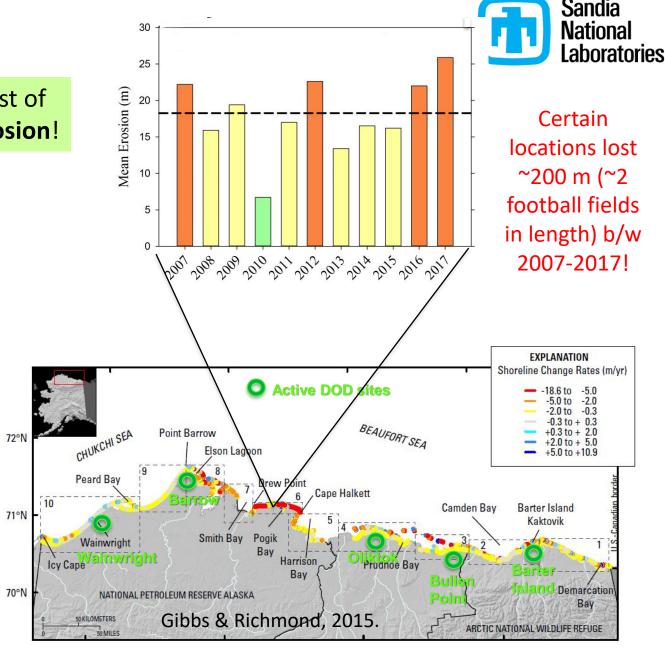
Motivation

The Arctic is warming at **2-3 times** the rate of the rest of the globe resulting in **accelerated rates of coastal erosion**!

- Primary culprit is loss of Arctic sea ice: since 1979
 sea ice has lost 51% in area and 75% in volume
 - > Increasing ice-free season
 - Increasing wave energy and storm surge
 - Increasing sea water temperatures

Erosion is threatening:

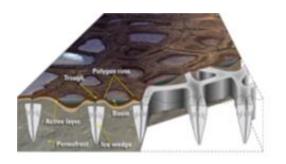
- Coastal communities: threatened with displacement
- Coastal infrastructure: active DoD sites, including toxic waste sites, in northern Alaska
- Global carbon balance: permafrost stores greenhouse gases (CO₂, CH₄, NO₂).



Permafrost erosion

What is permafrost?

- Ground, comprised of soil, rock, silt, clay and sand, held together by ice, that remains frozen for 2+ consecutive years.
- 24% of ice-free land area in Northern Hemisphere and 85% of Alaska Greenland, Canada and Siberia sits on top of permafrost.



Left: schematic illustrating formation of ice wedges and ice-wedge polygon landscapes. Right: map of permafrost distribution in Arctic



Brown et al. 1998.



Unique coastal permafrost erosion process in Arctic:

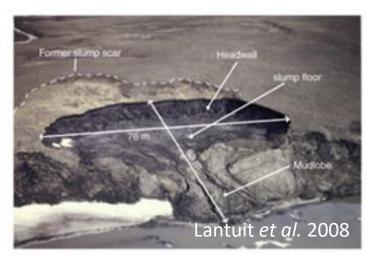
- Predominant geomorphology: ice-wedge polygons
 - > Ice acts to **bind** unconsolidated soils in permafrost forming ice wedges.
 - Ice wedges grow/expand up to ms wide and 10s meters deep.
 - Melting of ice wedges causes permafrost failure.

Permafrost failure mechanisms



- Retrogressive thaw slumping: a slope failure characterized by thaw of exposed ground ice and slumping of thawed soil, typically caused by thermo-denundation¹.
- Active layer detachment: failures are translational landslides that occur in summer in thawing soil overlying permafrost, typically caused by thermo-denundation¹.
- Block failure: a niche (recess at bluff base) progresses landward until the overhanging material fails in a shearing or toppling mode known as block failure, caused by thermo-abrasion².

Fallen blocks can disintegrate in the near-shore environment within 1-2 weeks!



Retrogressive thaw slumping



Active layer detachment

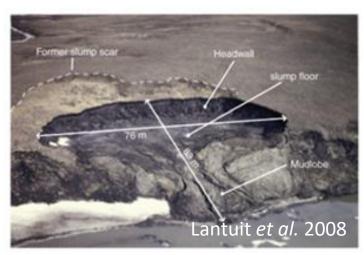


Block failure

Permafrost failure mechanisms



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Retrogressive thaw slumping



Active layer detachment



Example of bluff erosion during 2019 UAV surveys*







Fallen blocks can disintegrate in near-shore environment within 1-2 weeks!



*Images courtesy of Ben Jones, UAF

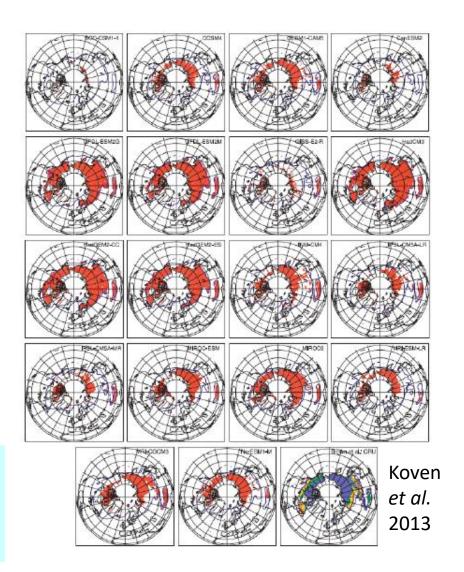
State-of-the-art in permafrost modeling



When this project began in 2017, tools to accurately predict Arctic coastal erosion did not exist!

- Most existing models* (including Earth System Model-, or ESM-, coupled models) are primitive:
 - Most models were based on trend projection and/or empirical relationships
 - Limited PDE-based models: primarily thermal models, e.g., 1D steady state heat flow (no mechanics/deformation)
 - Most models assumed a **particular type** of **erosion** (e.g., block failure)
 - Models did not include realistic boundary conditions and did not account for permafrost geomorphologies or geophysics.

Premise behind the ACE project/model: an accurate, predictive Arctic coastal erosion model must couple the influences of evolving wave dynamics, thermodynamics and mechanics.



Outline



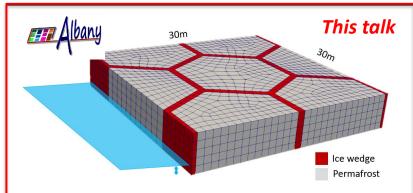
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Proposed solution: multi-scale approach



Goal of the Arctic Coastal Erosion (ACE) project is to deliver a field-validated predictive model of thermo-abrasive erosion for the permafrost Arctic coastline





Micro-Scale Model

10's of meters & storm duration

One set of input variables defining the geomorphology and geophysics of the terrestrial model.

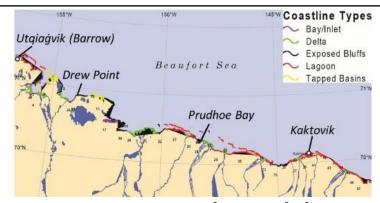
- 3D heat transfer + mechanics-based plastic deformation
- Wave circulation BCs representing time-varying realizations of individual storm events.



Meso-Scale Model

10's of kilometers & monthly duration

A number of micro-scale models that represent the stochastic distributions of input variables along a confined coastline.



Macro-Scale Model

100's of kilometers & annual (+) durations

A number of meso-scale models representing different coastline types (delta, exposed bluffs, lagoons, etc.) along the AK coastline.

Longer term vision: upscale micro-scale model to meso- and macro-scales

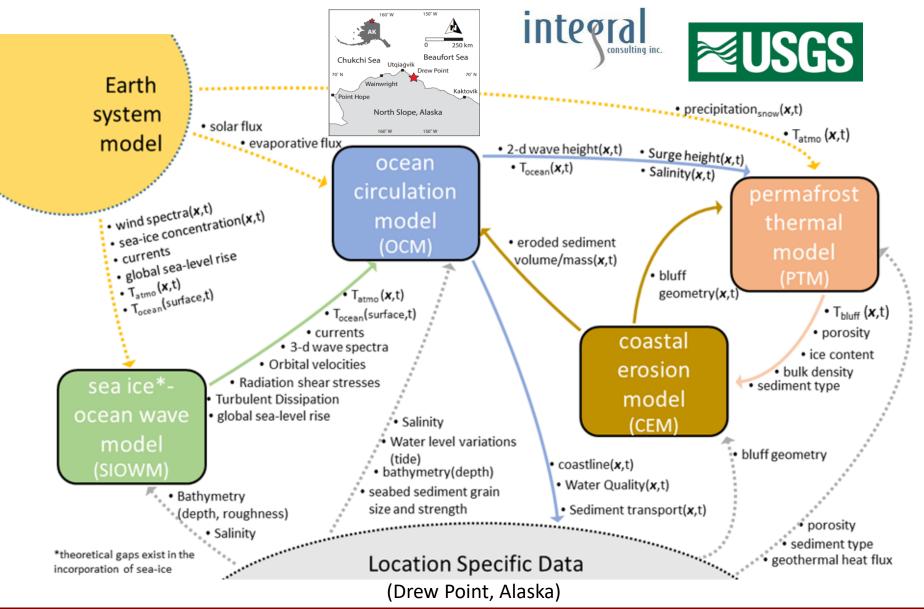
Create "catalog" of smaller-scale models for diff. Arctic locations, use catalog to derive (physics-based) statistical parameterizations of things like aggregate retreat rates

ACE Model Component Coupling









ACE project has many pieces!

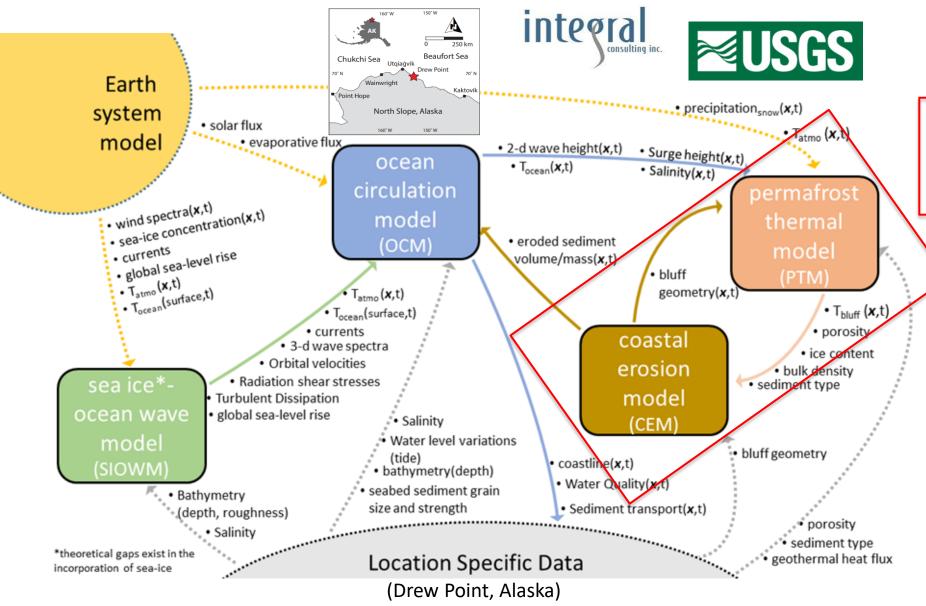
- <u>Terrestrial model</u>: thermomechanical coupled FEM model that can simulate transient niche development.
- Oceanographic model: WW3 + SWAN + Delft3D wave models for providing oceanic BCs (ocean temp/height) to terrestrial model.
- Geomechanical testing: for characterization of permafrost parameters in terrestrial model.
- <u>Field campaign</u>: offshore oceanographic measurements, bathymetric survey, niche measurements, etc.

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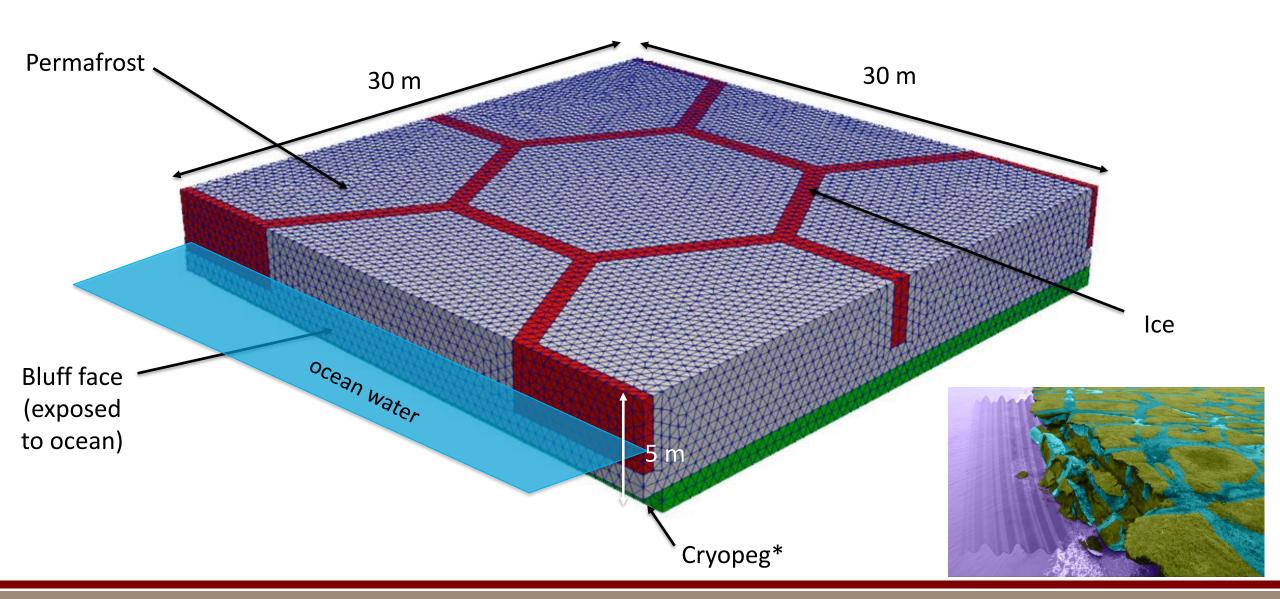
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Anatomy of a canonical computational domain





^{*} Layer of unfrozen ground that is perennially cryotic (forming part of the permafrost) in which freezing is prevented.

Mechanical model



 Finite deformation time-dependent variational formulation for solid mechanics problem obtained by minimizing the energy functional:

$$\Phi[\boldsymbol{\varphi}] \coloneqq \int_{\Omega} A(\boldsymbol{F}, \boldsymbol{Z}) \, dV - \int_{\Omega} \rho \boldsymbol{B} \cdot \boldsymbol{\varphi} \, dV - \int_{\partial_{\boldsymbol{T}} \Omega} \boldsymbol{T} \cdot \boldsymbol{\varphi} \, dS$$

A(F, Z): Helmholtz free-energy density

Z: material variables

F: deformation gradient $(\nabla \varphi)$

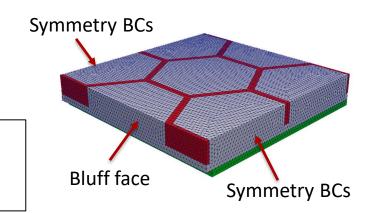
 ρ : density

B: body force

T: prescribed traction

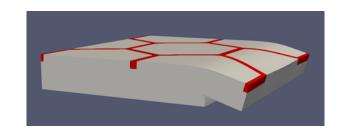
- > Computes *displacements* and *new computational geometry* (following erosion)
- J_2 plasticity extended to large-deformation regime constitutive model for ice and permafrost
 - Incorporates all mechanisms that lead to deformation, plastic flow and creep of polycrystalline materials like ice; minimal calibration parameters; simplest material model w/ plastic behavior.
- Boundary conditions:
 - > Symmetry BCs on lateral sides
 - > Wave pressure Neumann BC on bluff face* (from wave model).
- Yield stress: $\sigma_0(T) := S_s \sigma_Y^{\text{soil}} + S_f f(T) \sigma_Y^{\text{ice}}$
 - > Used in erosion failure criteria

f: ice saturation (\in [0,1]) $\sigma_Y^{\rm soil}/\sigma_Y^{\rm ice}$: yield stress of soil/ice S_S/S_f : soil/ice volume fraction



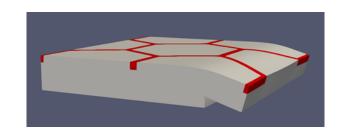


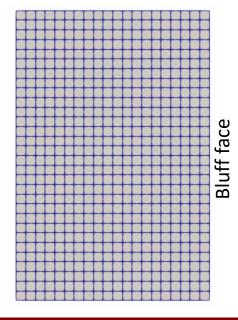
- Erosion criterion: when material exposed to water reaches a critical exposure time.
- Stress criterion: when material reaches a critical value of the yield stress.
- **Kinematic criterion:** when material has tilted excessively, it is assumed to have fallen as part of block erosion.





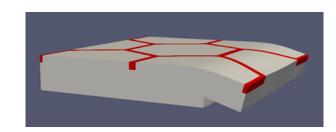
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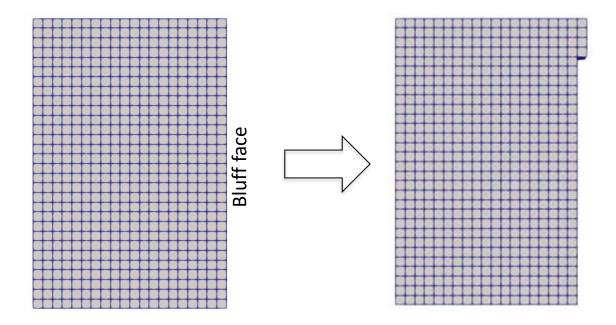






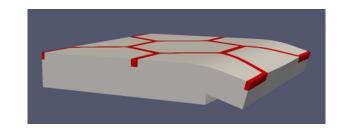
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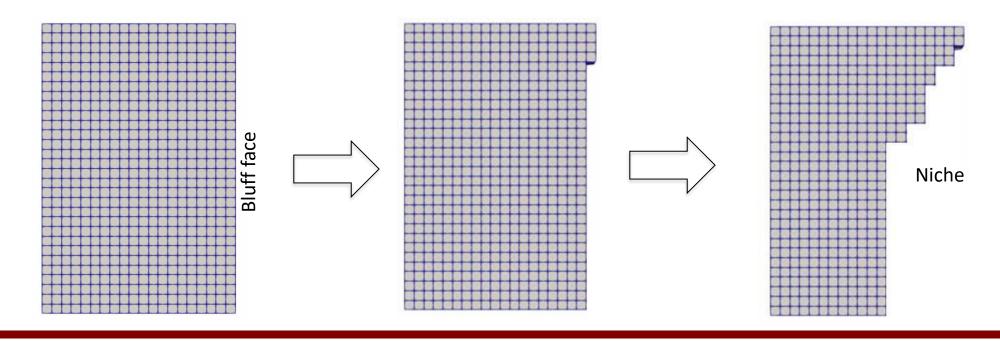






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Thermal model

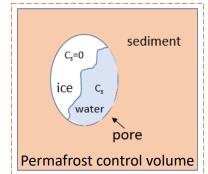


• Transient heat conduction in a non-homogeneous porous

media with water-ice phase change:

$$(\overline{\rho c_p} + \widetilde{\Theta}) \frac{\partial T}{\partial t} = \nabla \cdot (\mathbf{K} \cdot \nabla T)$$

where $\widetilde{\Theta} \coloneqq \rho_f L_f \frac{\partial f}{\partial T}$ incorporates phase changes through soil freezing curve, $\frac{\partial f}{\partial T}$.



 $\bar{\rho}$: density from mixture model

 $\overline{c_p}$: specific heat from mixture model

K: thermal diffusivity tensor

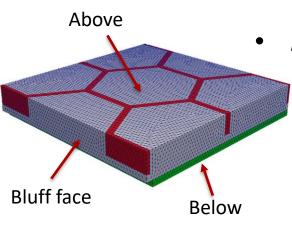
 ρ_f : ice density

 L_f : latent heat of water-ice phase change

f: ice saturation ($\in [0,1]$)

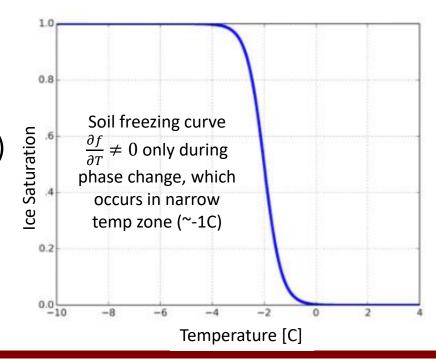
 $\frac{\partial f}{\partial T}$: soil freezing curve (depends on salinity)





Boundary conditions (from wave model/data)

- ➤ Local geothermal heat flux from below
- Mean annual air temp from above
- > Air/ocean temp at bluff face



Parameters & inputs

Parameters estimated from lab experiments:

- Elastic modulus, Poisson's ratio, yield stress
- Sand/silt/clay fractions with depth
- Porosity with depth

Parameters from literature:

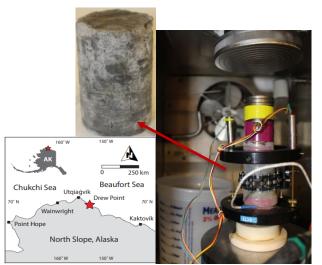
- Ice/water/sediment densities, thermal conductivities, heat capacities
- Freezing curve/width as function of sediment type
- Bluff salinity with depth

Parameters estimated from observational data at Drew Point, AK:

- Skin temp w/ time, initial bluff temp (USGS weather station data)
- Geothermal heat flux (borehole at Barrow, AK)
- Polygon dimension, ice wedge thickness and depth, bluff height, living organic layer thickness (Aug. 2019 field campaign)

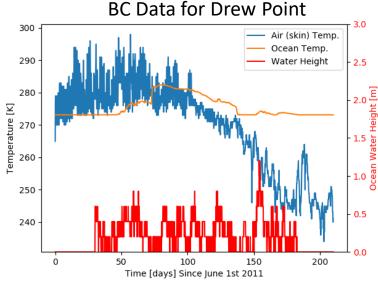
Parameters from wave model (WW3+SWAN+Delft3D):

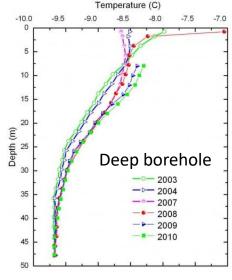
Ocean temperature, salinity and sea-level w/ time (for thermal & wave pressure BCs)



integral









ce saturation

Coupled thermo-mechanical formulation

geometry



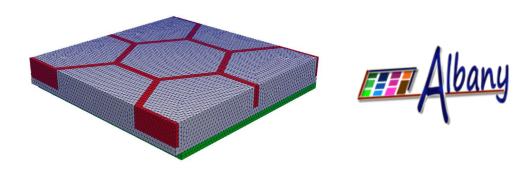
Potential key advantages:

- Failure modes develop from constitutive relationships in FEM model (no empirical relationships!)
- 3D unsteady heat flow can include chemistry
- Thermal and mechanical problems can be advanced using different time-steppers (e.g., implicit-explicit coupling)
- Tightly coupled strength + thermal states

Unique characteristic of coupled model: coupling happens at the level of material model

Thermal:

Inputs: geometry, sediment type, ice volume, water volume, pore size, salinity *Outputs:* temperature field, ice saturation



Mechanical:

Inputs: ice saturation, strength relationship as function of thermal state, stress-strain relationships of permafrost and ice

Outputs: displacements, eroded geometry

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Finite element implementation within Albany-LCM



The *thermo-mechanical Arctic Coastal Erosion (ACE)* model is implemented within the *LCM project* in Sandia's open-source parallel, C++, multi-physics, finite element code, *Albany*.

- Component-based design for rapid development.
- Contains a wide variety of constitutive models.
- Extensive use of libraries from the open-source Trilinos project.
 - ➤ Use of the *Phalanx* package to decompose complex problem into simpler problems with managed dependencies.
 - > Use of the **Sacado** package for **automatic differentiation**.
- Coupled to the DOE's Energy Exascale Earth System Model (E3SM)
 through MPAS Albany Land Ice (MALI) component.
- All software available on GitHub.



https://github.com/ SNLComputation/LCM



https://github.com/trilinos/ trilinos



Numerical results summary



Mechanics-only simulation¹



Scientific knowledge and engineering tools for predicting coastal erosion are largely confined to temperate climate zones that are dominated by non-cohesive sediments. The pattern of erosion exhibited by the ice-bonded permafrost bluffs in Arctic Alaska, however, is not well-explained by these tools. Investigation of the oceanographic, thermal, and mechanical processes that are relevant to permafrost bluff failure along Arctic coastlines is needed. We conducted physics-based numerical simulations of mechanical response that focus on the impact of geometric and material variability on permafrost bluff stress states for a coastal setting in Arctic Alaska that is prone to toppling mode block failure. Our three-dimensional geomechanical boundary-value problems output static realizations of compressive and tensile stresses. We use these results to

Thermo-mechanical simulations²



Mechanics-only simulation



Mechanics-only simulation*



ORIGINAL RESEARCH

published: 12 May 2020 doi: 10.3389/feart.2020.00143

Geometric and Material Variability Influences Stress States Relevant to Coastal Permafrost Bluff Failure

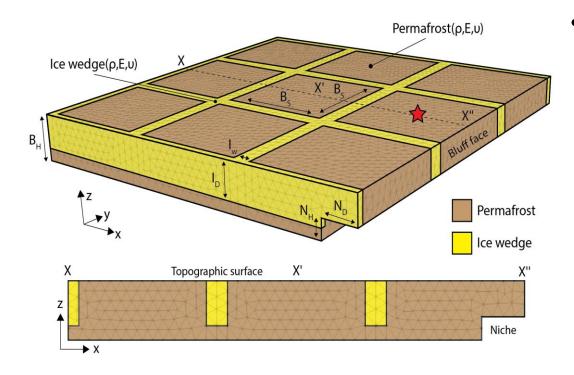
Matthew A. Thomas **1, Alejandro Mota², Benjamin M. Jones³, R. Charles Choens², Jennifer M. Frederick² and Diana L. Bull²

¹ U.S. Geological Survey, Geologic Hazards Science Center, Golden, CO, United States, ² Sandla National Laboratories, Albuquerque, NIM, United States, ³ Institute of Northern Engineering, College of Engineering and Mines, University of Alaska Fairbanks, Fairbanks, AK, United States

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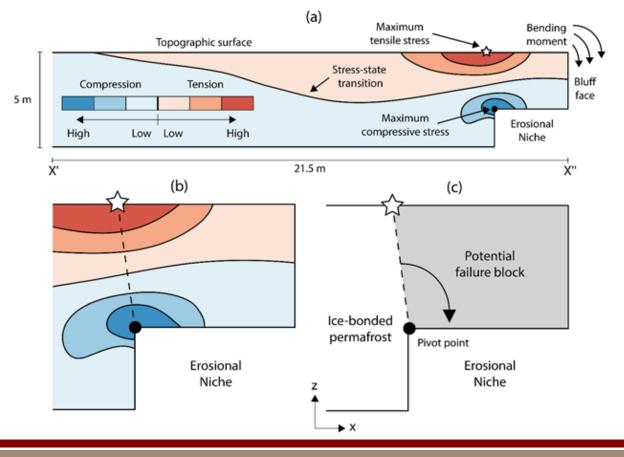
Mechanics-only simulation*





- 3D elastic mechanics-only simulations assessed impact of bluff geometry and material variability on stress states leading up to bluff failure
 - Only load is gravitational.

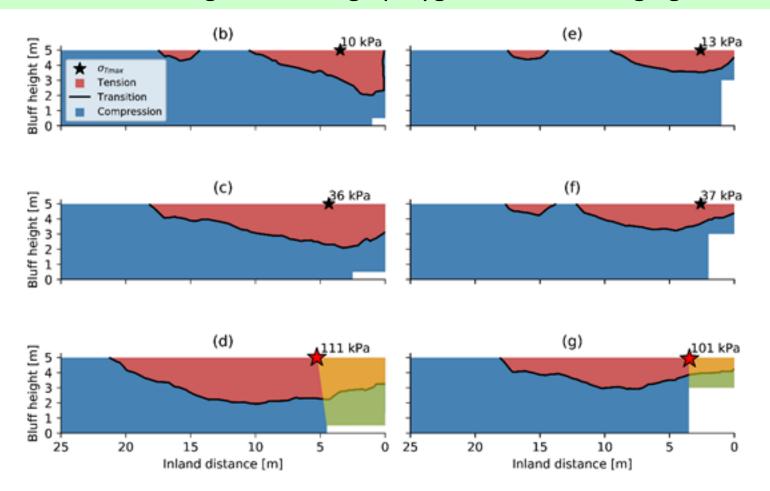
• Simulations facilitated examination of stress patterns within bluff and identification of location and magnitude of max tensile stress $(\sigma_{T_{\max}})$



Mechanics-only simulation*: main takeaways



Niche dimension affects location and magnitude of simulated max tensile stress ($\sigma_{T_{\text{max}}}$) more than the bluff height, ice wedge polygon size, ice wedge geometry, bulk density and Poisson's ratio



 Inland extent of niche was advanced for 6 erosional niche heights from 0.1-3 m

Taller and **narrower** erosional **niches** promote smaller failure masses compared to those with shorter and deeper niches

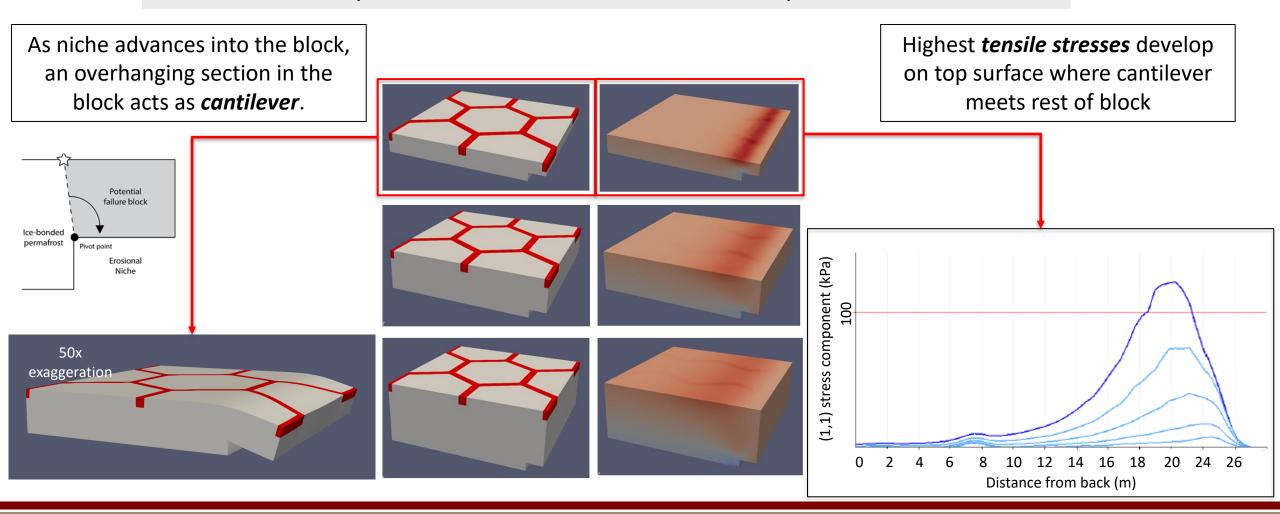
- Lower bound for tensile stress from lab measurements: 100 kPa
- Orange/green shading highlights potential failure areas.

^{*} M. Thomas et al. Frontiers in Earth Science 8, April 2020.

Mechanics-only simulation*: main takeaways



Taller and **narrower** erosional **niches** promote smaller failure masses compared to those with shorter and deeper niches



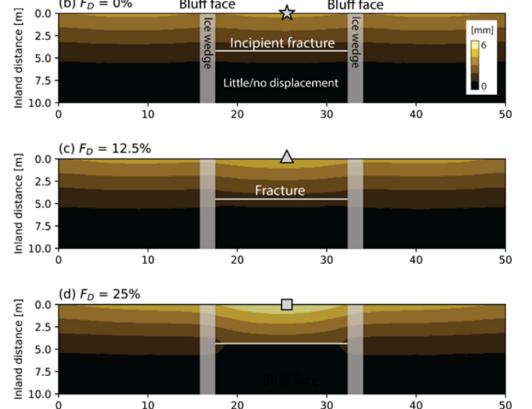
^{*} M. Thomas et al. Frontiers in Earth Science 8, April 2020.

Mechanics-only simulation*: main takeaways



It has been observed that failure can occur along tension cracks in ice wedge polygon centers.

Bluff face



Bluff face

(b) $F_D = 0\%$

- Simulations suggest tension cracks can form within the range of niche depths/heights considered here.
- Even relatively **shallow** vertical cracks can concentrate strain within ice-bonded permafrost bluffs.

 F_D : fracture depth



Along-bluff distance [m]

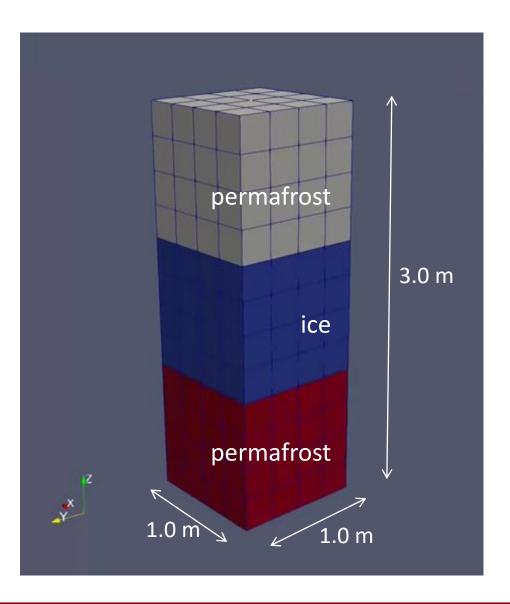
Thermo-mechanical 2.5D slice simulation



Thermo-mechanical simulations*



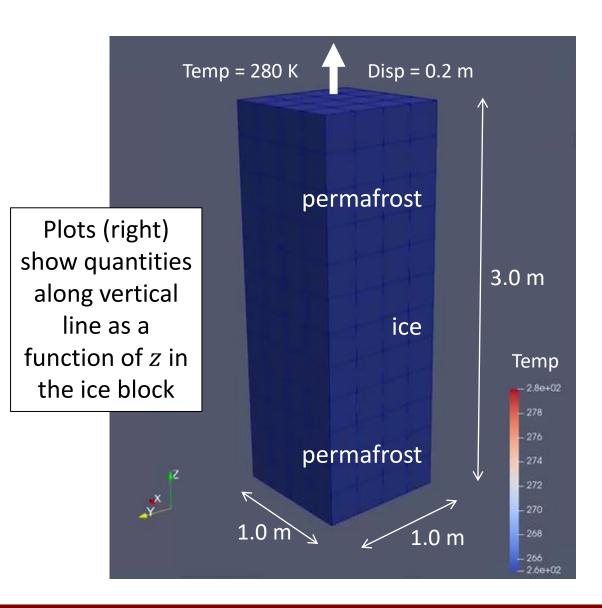


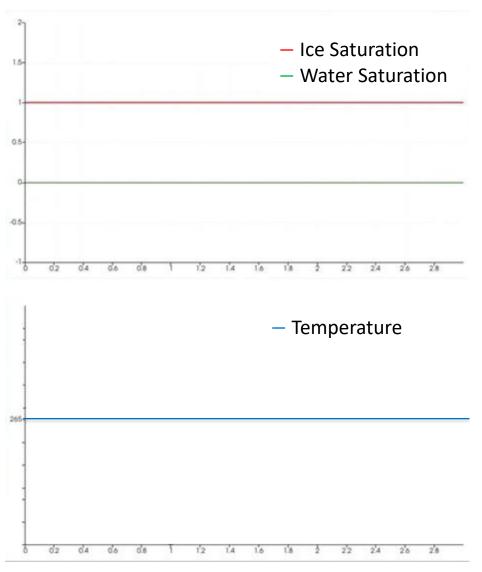


- Cuboid is comprised of block of ice material, wedged between two blocks of permafrost material.
- Cuboid subjected to simultaneous heating and stretching from the top
- Cuboid is affixed to the bottom and with symmetry boundary conditions on the sides.
- **Temperature** is initialized to 265K.

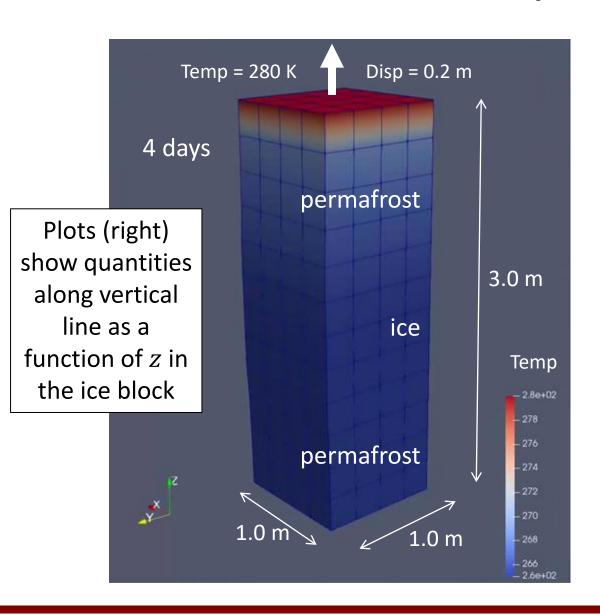


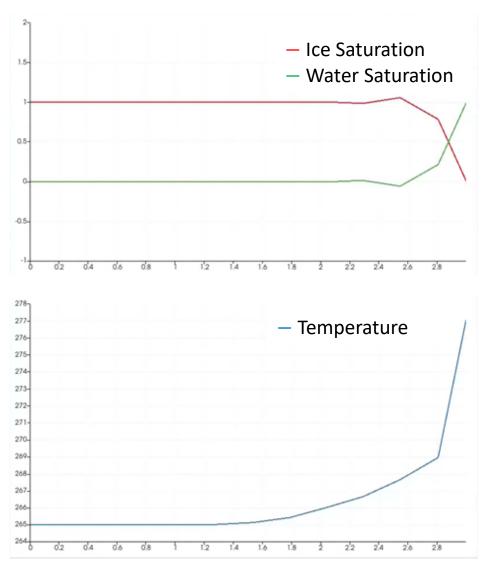




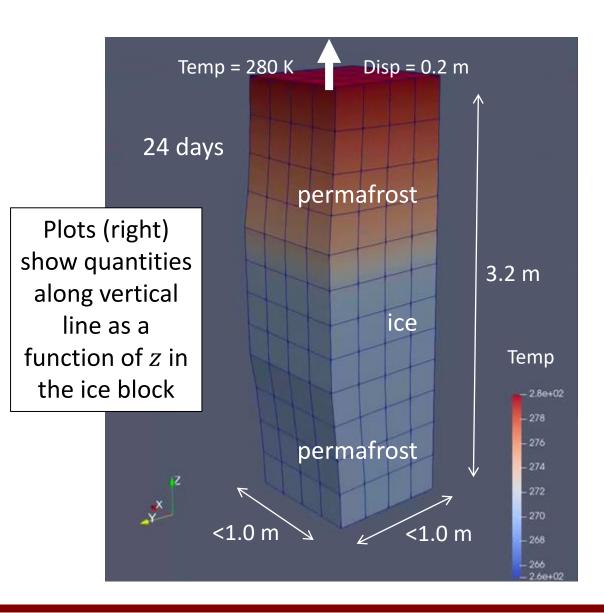


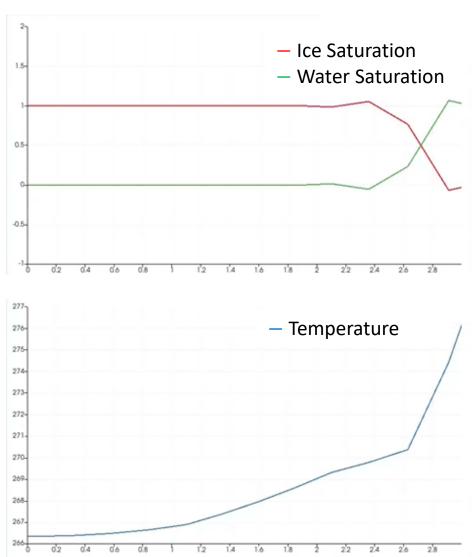






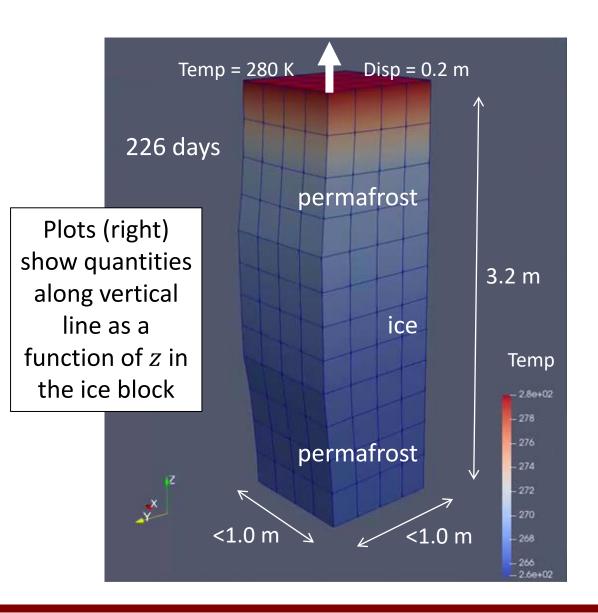


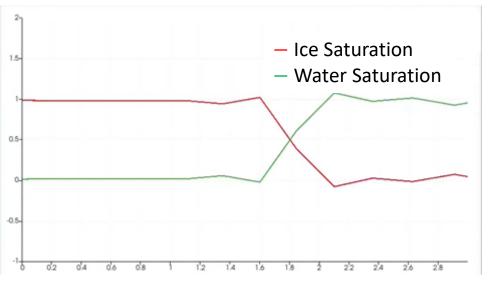


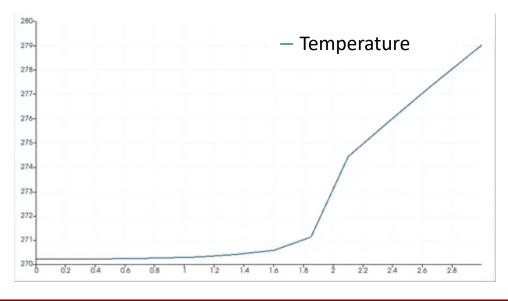


Thermo-mechanical coupling: cuboid problem



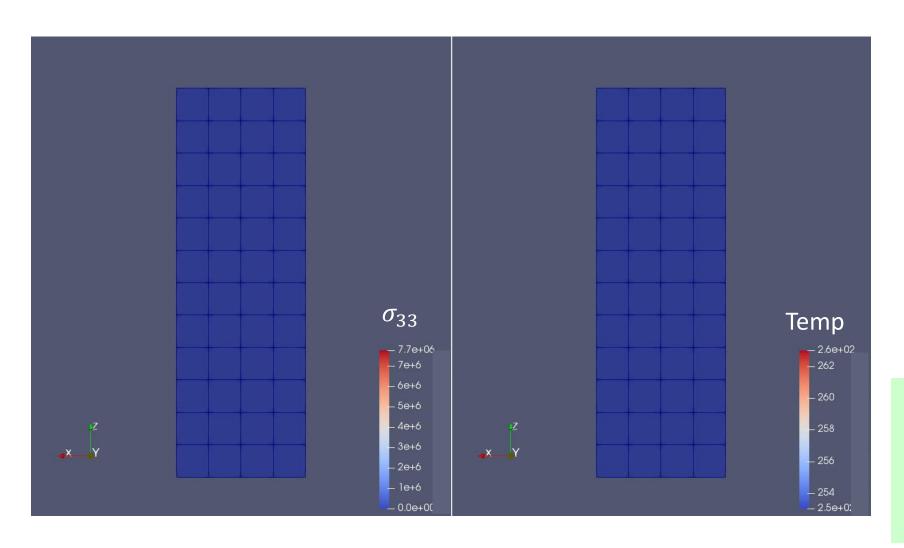


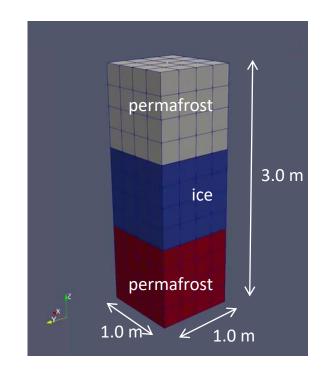




Thermo-mechanical coupling: cuboid problem





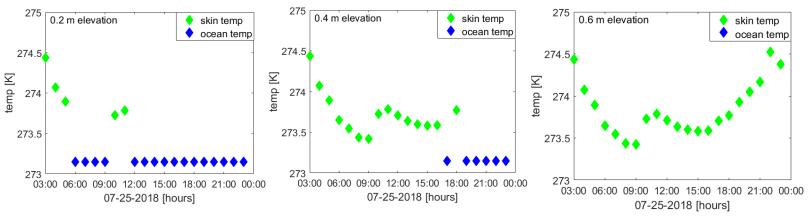


As cuboid is heated and stretched at top, heat propagates down, *melting ice* and causing *failure*.

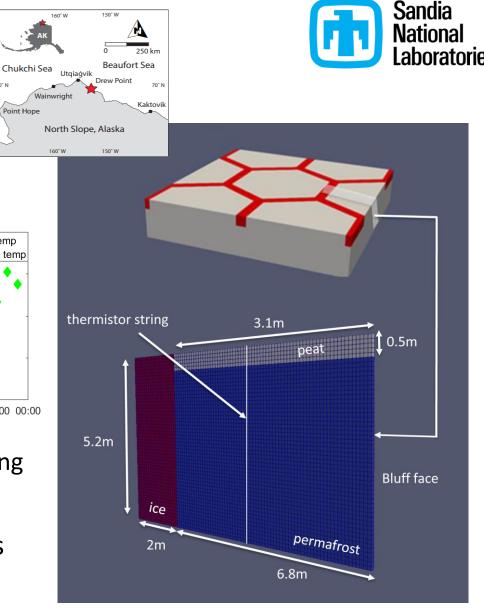
2.5D slice at Drew Point, Alaska*

Computational domain is 2.5D cross-section of archetypal
 3D bluff geometry discretized using a uniform hex grid.

➤ Slice of permafrost is exposed to *realistic BC data* occurring at Drew Point, Alaska in July 2018 (pseudorealistic problem)

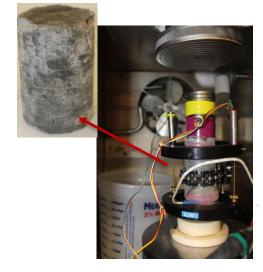


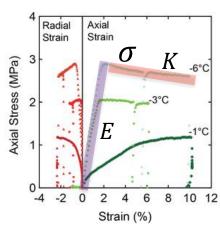
- ➤ Initial temperature field obtained from vertical thermistor string placed into DP1-1 ice core at Drew Point.
- *Material properties* determined from laboratory experiments on frozen soil samples from Drew Point, Alaska (next slide)
- Implicit Newmark for mechanical, explicit forward Euler for thermal (stable $\Delta t = 1$ hour)

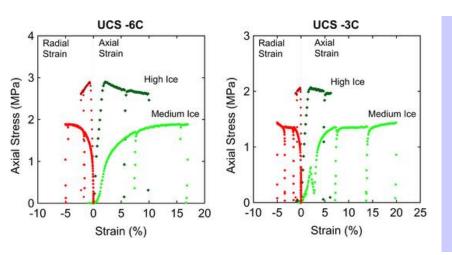


Material Model Calibration to Experimental Data

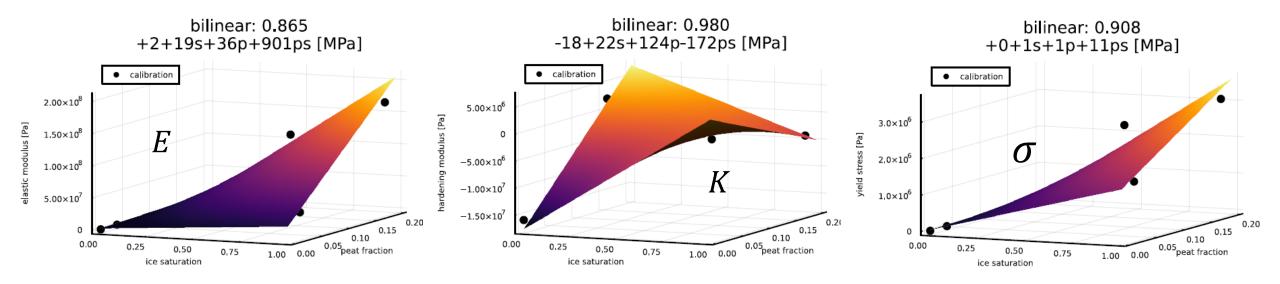




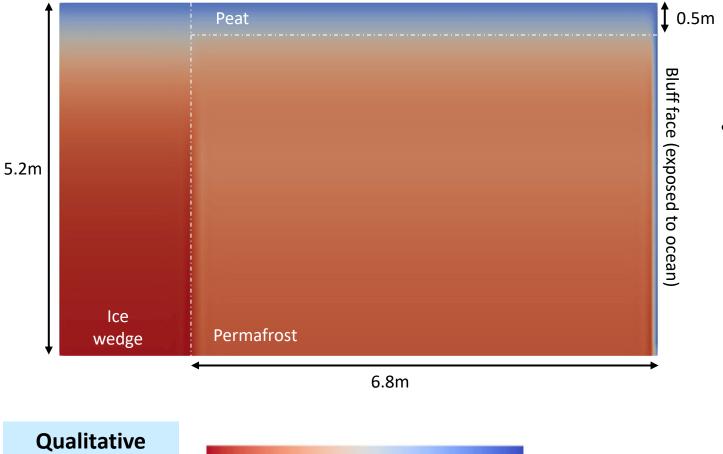




Experimental results on permafrost core samples were analyzed to create fits for parameters* E, K, σ as a function of ice saturation and sediment fractions (peat content).



2.5D slice at Drew Point, Alaska*

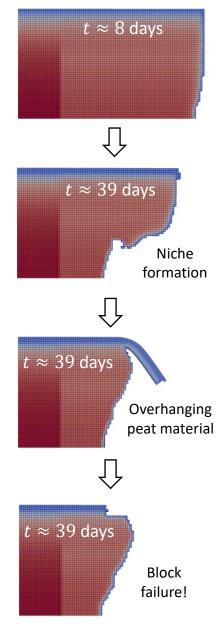


Simulation showing niche progression beginning at the bluff toe and block failure/collapse event*

~3m deep niche forms before a block collapse event similar to observed collapse at Drew Point, Alaska in early fall 2018.



Thermal denudation simultaneously with realistic *niche geometry* development.



0.4

0.6

Ice Saturation

0.8

1.0

0.2

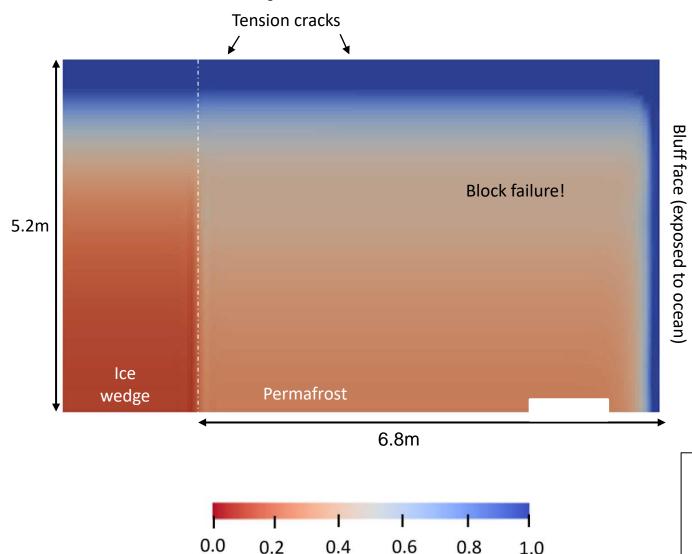
0.0

comparison to

observations

^{*} For details, see: Frederick, Mota, Tezaur, Bull, J. Comput. Appl. Math. 2021.

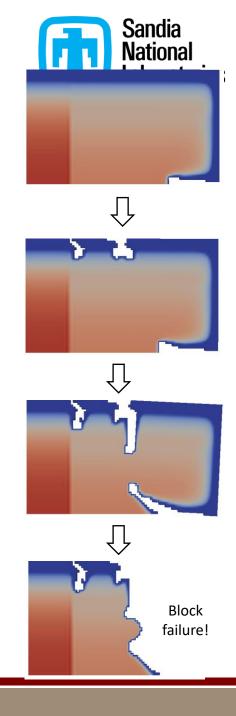
2.5D slice problem variant



Ice Saturation

No-peat variant of the 2.5D slice problem with slightly different material parameters

Once niche advanced far enough, tension crack development in response to niche formation is observed



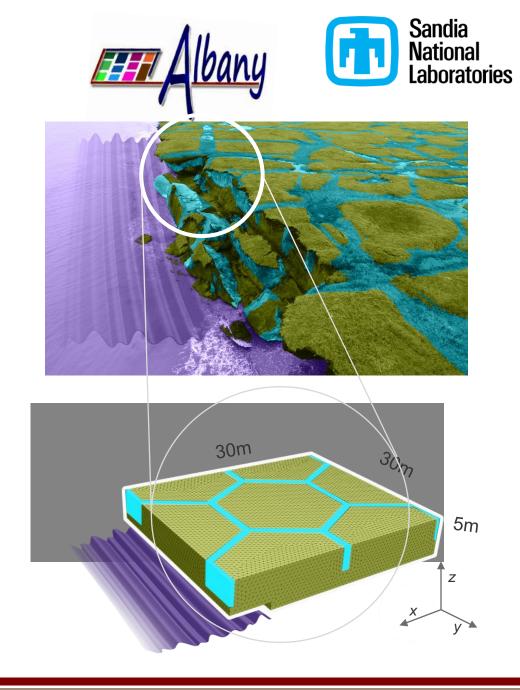
Outline



- Motivation and background
- The Arctic Coastal Erosion (ACE) project
- Thermo-mechanical finite element model of permafrost
- Numerical results
- Summary
- Ongoing/future work

Summary

- We have developed a thermo-mechanical coupled FEM model, ACE, that can simulate transient niche development and permafrost erosion within Albany.
- The model was calibrated using data from a series of experiments on frozen soil samples from Drew Point, Alaska that were performed at Sandia's Geomechanics Laboratory, as well as observational data collected at the same location.
- The model incorporates boundary conditions from the WW3+SWAN+Delft3D wave models and observational data from field campaigns at Drew Point, Alaska.



Outline



- Motivation and background
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Ongoing/future work

Sandia National Laboratories

Near term:

- Quantitative validation study in which the ACE model predictions are compared to available observational data collected during the 2018-2019 summer seasons at Drew Point, Alaska (2.5D slice + 3D).
- Testing/tuning of ACE thermo-denudation simulation capabilities.
- Further **calibration** and **sensitivity studies** using a range of environmental, geomorphological and numerical parameters for thermo-mechanical model.
- Manuscript on above work is in preparation.

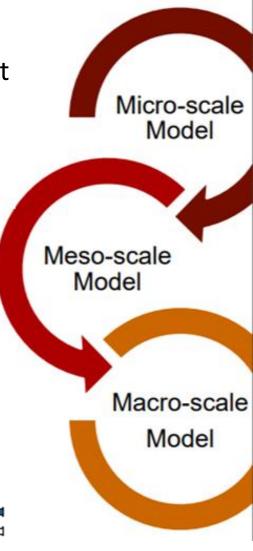
Longer term:

- Integrate chemical transport into thermal model.
- Infer statistical meso-/macro-scale models and relevant physics-based parameterizations from ACE micro-model, towards integration into ESMs.
 - ➤ ACE is member of the DOE- sponsored InteRFACE project* focused on coastal processes in Arctic.





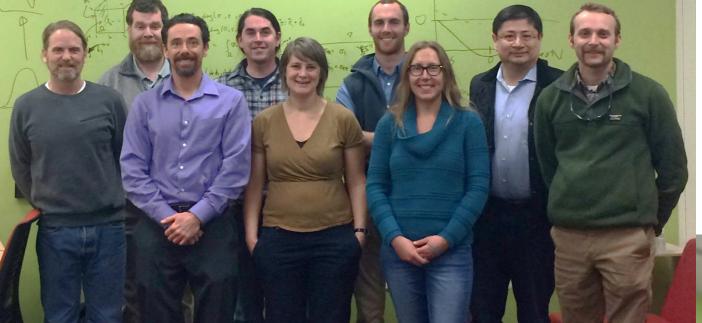




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- [5] H. Lantuit, W. Pollard. Fifty years of coastal erosion and retrogressive thaw slump activity on Herschel Island, southern Beaufort Sea, Yukon Territory, Canada. Geomorphology, 95, 84-102, 2008.
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Acknowledgements

Research Team

SNL: D. Bull (PI), J. Frederick, A. Mota, C.

Choens, I. Tezaur, L. Criscenti

USGS: M. Thomas, B. Jones

UAF: J. Kasper, E. Brown

Integral Consulting: C. Jones, C. Flanary

U Texas: J. McClelland, E. Bristol, C. Connolly





Start of Backup Slides

Potential impacts



- 3D model capable of predicting erosion from the material's constitutive relationships capturing all types of deformation (block & denudation) leading to:
 - Data-driven understanding of the characteristics that cause erosion
 - > A tool to guide **military** and **civil infrastructure** investments
 - > An improved understanding of coastal food web impacts and carbon-climate feedbacks
 - Redistributed eroded sediment in the environment enables:
 - Prediction of deposition locations
 - Estimates of fluxes (biogeochemical, toxins, etc.)

Approach for moving from mechanistic micro-scale to stochastic meso-scale model sets stage for integration into global climate models built upon parametric analyses of input variables



Oceanography in Mechanistic Model



Development of wave field in the Arctic to develop nearshore

BCs

- surface winds
- ice cover
- temperature (surface and ocean)
- solar radiation
- persistent currents

Wave set-up

conditions 2-way

coupled with

circulation

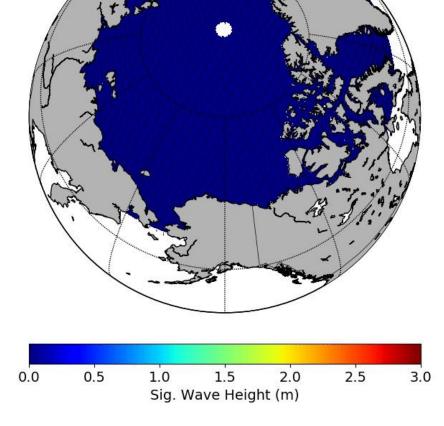
- high resolution near shore environment
- capture set-up (storm surge and runup)
- wave energy inclusive of induced current effects

Circulation and thermodynamic mixing 2-way coupled with waves

- ability to model mixing of temperature and salinity clines
- capture induced currents in nearshore



- Inclusion of ice coverage for fetch limited wave growth
- Knowledge of wave energy along broad coastline
- Set-up determination inclusive of bathymetry and wave energy
- Ability to accurately predict temperature at bluff face through mixing of clines in the ocean



WW3 polar stereographic model initially developed by NRL (Erick Rogers) and NOAA (Arun Chawla)

Proposed solution





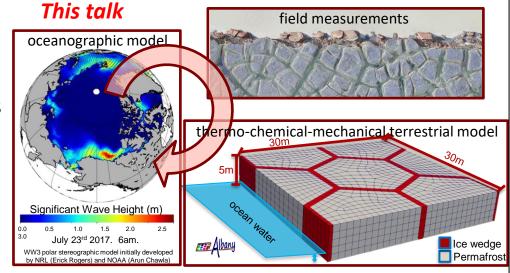
LABORATORY DIRECTED RESEARCH & DEVELOPMENT

Goal of the Arctic Coastal Erosion (ACE) project is to deliver a field-validated predictive model of thermo-abrasive erosion for the permafrost Arctic coastline

2017-2022 Micro-scale Model 10's of meters &

storm duration

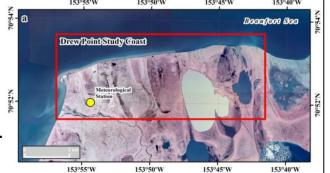
- Multi-physics finite element model of an archetype of the coastline coupled with highfidelity model of storm intensities
 - Input variables define geomorphology & geophysics
 - Plastic deformation model of material (J2 class)
 - Geomechanical testing to determine coupled thermal-mechanical strength characteristics
 - Time-varying ocean BCs (water level, temp, salinity)
 - Eroded sediment and biogeochemical flux tracking



2023+ Meso-scale Model

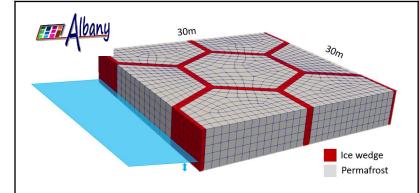
10's of km's & seasonal duration

- A "catalog" of micro-scale models that represent the statistical distributions of input variables along a ~10km stretch of coastline.
 - Probability distribution functions of geomorphology and geophysics used to weight erosion output
 - Will validate approach with decade long annual measurements at Drew Point.
 - Evaluating ocean "exposure metrics" to represent time-varying ocean



Multi-scale approach





Micro-Scale Model

10's of meters & storm duration

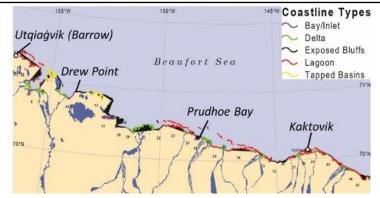
One set of input variables defining the geomorphology and geophysics of the terrestrial model.



Meso-Scale Model

10's of kilometers & monthly duration

A number of micro-scale models that represent the stochastic distributions of input variables along a confined coastline.



Macro-Scale Model

100's of kilometers & annual (+) durations

A number of meso-scale models that represent the diversity of coastline types (delta, exposed bluffs, lagoons, etc.) along the AK coastline.

- Working towards a series of fully coupled studies to determine terrestrial model sensitivities to:
 - > Height of water on bluff face
 - Exposure time of bluff face to water

- Temperature of water
- Salinity of water

Parameters & inputs

- Permafrost properties depend on *ice content*, *unfrozen water content* and *frost susceptibility*.
- Few mathematical relationships exist that describe changes in tensile strength, shear strength and cohesion of ice/permafrost with changes in temperature.
- Series of *experiments* (UCS¹, BTS², DT³) on frozen soil samples at different temps (-6C, -3C, -1C) and ice content from Drew Point, AK were performed at SNL's Geomechanics Laboratory to estimate:

> Strength: 1-3 MPa

> Young's modulus: 0.01-0.16 GPa

➤ Poisson's ratio: 0.1-0.35

➤ Porosity values: 40-95%

