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A minimal subspace rotation approach for extreme model reduction in fluid mechanics

Irina Tezaur¹, Maciej Balajewicz²

¹ Extreme Scale Data Science & Analytics Department, Sandia National Laboratories ² Aerospace Engineering Department, University of Illinois Urbana-Champaign

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Outline

- 1. Introduction
 - Targeted application
 - POD/Galerkin approach to MOR
 - Extreme model reduction
 - Mode truncation instability in MOR
- 2. Accounting for modal truncation
 - Traditional linear eddy-viscosity approach
 - New proposed approach via subspace rotation
- 3. Applications
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 - Moderate Reynolds (*Re*) number channel driven cavity
- 4. Extension to Least-Squares Petrov-Galerkin (LSPG) ROMs
- 5. Summary & future work



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- Of <u>primary interest</u> are *long-time predictive simulations*: ROM run at same parameters as FOM but much longer in time.
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 <u>Secondary interest</u>: ROMs robust w.r.t. *parameter changes* (e.g., Reynolds, Mach number) for enabling *uncertainty quantification*.

POD/Galerkin Method to MOR





Extreme Model Reduction



- Most realistic applications (e.g., high *Re* compressible cavity): basis that captures
 >99% snapshot energy is required to accurately reproduce snapshots.
 - \rightarrow leads to n > O(1000) except for **toy problems** and/or **low-fidelity** models.
- Higher order modes are in general *unreliable for prediction*, so including them in the basis is unlikely to improve the *predictive* capabilities of a ROM.

Figure (right) shows projection error for POD basis constructed using 800 snapshots for cavity problem. Dashed line = end of snapshot collection period.



We are looking for an approach that enables <u>extreme model reduction</u>: ROM basis size is O(10) or O(100).

3D Compressible Navier-Stokes Equations

• We start with the 3D compressible Navier-Stokes equations in *primitive specific volume form:*

[PDEs]

$$\zeta_{,t} + \zeta_{,j}u_j - \zeta u_{j,j} = 0$$

$$u_{i,t} + u_{i,j}u_j + \zeta p_{,i} - \frac{1}{Re}\zeta\tau_{ij,j} = 0$$

$$p_{,t} + u_j p_{,j} + \gamma u_{j,j}p - \left(\frac{\gamma}{PrRe}\right)\left(\kappa(p\zeta)_{,j}\right)_{,j} - \left(\frac{\gamma - 1}{Re}\right)u_{i,j}\tau_{ij} = 0$$
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• Spectral discretization $(\boldsymbol{q}(\boldsymbol{x},t) \approx \sum_{i=1}^{n} a_i(t) \boldsymbol{U}_i(\boldsymbol{x})) + \text{Galerkin projection}$ applied to (1) yields a system of <u>*n* coupled quadratic ODEs</u>:

[PDEs]

$$\frac{d\boldsymbol{a}}{dt} = \boldsymbol{C} + \boldsymbol{L}\boldsymbol{a} + [\boldsymbol{a}^T \boldsymbol{Q}^{(1)} \boldsymbol{a} + \boldsymbol{a}^T \boldsymbol{Q}^{(2)} \boldsymbol{a} + \dots + \boldsymbol{a}^T \boldsymbol{Q}^{(n)} \boldsymbol{a}]^T$$
(2)

where $\boldsymbol{C} \in \mathbb{R}^{n}$, $\boldsymbol{L} \in \mathbb{R}^{n \times n}$ and $\boldsymbol{Q}^{(i)} \in \mathbb{R}^{n \times n}$ for all i = 1, ..., n.





Stability can be a real problem for compressible flow ROMs!

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This talk focuses on remedying "*mode truncation instability*" problem for projection-based (POD/Galerkin) compressible flow ROMs.



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For a low-dimensional ROM to be stable and accurate, the <u>truncated/unresolved subspace</u> must be accounted for.



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• Dissipative dynamics of truncated higher-order modes are modeled using an additional linear term:

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 - Inherently a <u>linear model</u> → cannot be expected to perform well for all classes of problems (e.g., nonlinear).

Proposed new approach: basis rotation



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Illustrative example

- <u>Standard approach</u>: retain only the most energetic POD modes, i.e., U₁, U₂, U₃.
- <u>Proposed approach</u>: add some higher order basis modes to increase dissipation, i.e., $a_1U_1 + b_1U_6 + c_1U_8$, $a_2U_2 + b_2U_{11} + c_2U_{18}$, $a_3U_3 + b_3U_{21} + c_3U_{28}$
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- <u>More generally</u>: approximate the solution using a linear superposition of n + p (with p > 0) most energetic modes:

$$\widetilde{\boldsymbol{U}}_{i} = \sum_{j=1}^{n+p} X_{ij} \, \boldsymbol{U}_{j}, \quad i = 1, \dots, n,$$
(3)

where $X \in \mathbb{R}^{(n+p) \times n}$ is an orthonormal ($X^T X = I_{n \times n}$) "rotation" matrix.

Goals of proposed new approach



Find **X** such that:

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 $\begin{array}{l} \text{minimize}_{\boldsymbol{X} \in \mathcal{V}_{(n+p),n}} f(\boldsymbol{X}) \\ \text{subject to} \quad g(\boldsymbol{X}, \boldsymbol{L}) = 0 \end{array}$

where $\mathcal{V}_{(n+p),n} \in \{ \mathbf{X} \in \mathbb{R}^{(n+p) \times n} : \mathbf{X}^T \mathbf{X} = \mathbf{I}_n, p > 0 \}$ is the <u>Stiefel manifold</u>.

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• Once *X* is found, the result is a system of the form:

$$\frac{d\boldsymbol{a}}{dt} = \boldsymbol{C} + \boldsymbol{L}\boldsymbol{a} + [\boldsymbol{a}^T \boldsymbol{Q}^{(1)}\boldsymbol{a} + \boldsymbol{a}^T \boldsymbol{Q}^{(2)}\boldsymbol{a} + \dots + \boldsymbol{a}^T \boldsymbol{Q}^{(n)}\boldsymbol{a}]^T$$

with:

$$Q^{(i)}_{jk} \leftarrow \sum_{s,q,r=1}^{n+p} X_{si} Q^{(s)}_{qr} X_{qr} X_{rk}, \quad \boldsymbol{L} \leftarrow \boldsymbol{X}^T \boldsymbol{L} \boldsymbol{X}, \quad \boldsymbol{C} \leftarrow \boldsymbol{X}^T \boldsymbol{C}^*$$
(4)



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• Maximize resolved *turbulent kinetic energy (TKE)*

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- TKE objective (7) comes from earlier work (Balajewicz *et al.,* 2013) involving stabilization of incompressible flow ROMs
 - POD modes associated with low KE are important *dynamically* even though they contribute little to overall energy of the fluid flow.

* In (7), Σ denotes the square of second moments of ROM modal coefficients (Balajewicz et al., 2013).



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 Numerical experiments reveal objective (6) produces better results than objective (7) for compressible flow.



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minimize_{$$X \in \mathcal{V}_{(n+p),n}$$} $f(X)$
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We use the traditional <u>linear eddy-viscosity closure model ansatz</u> for the constraint g(X, L) = 0 in (5):

$$g(\boldsymbol{X}, \boldsymbol{L}) = \operatorname{tr}(\boldsymbol{X}^T \boldsymbol{L} \boldsymbol{X}) - \eta$$
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 - $\eta = \text{proxy}$ for the balance between linear energy production and energy dissipation.
- Constraint comes from property that <u>averaged total power</u> (= tr(X^TLX) + energy transfer) has to vanish.

Optimization problem summary



(9)

Minimal subspace rotation: trace minimization on Stiefel manifold

minimize_{$$X \in \mathcal{V}_{(n+p),n}$$} $- \operatorname{tr}(X^T I_{(n+p) \times n})$
subject to $\operatorname{tr}(X^T L X) = \eta$

- $\eta \in \mathbb{R}$: proxy for the balance between linear energy production and energy dissipation (calculated iteratively using modal energy).
- $\mathcal{V}_{(n+p),n} \in \{ X \in \mathbb{R}^{(n+p) \times n} : X^T X = I_n, p > 0 \}$ is the <u>Stiefel manifold</u>.
- Equation (9) is solved efficiently offline using the method of Lagrange multipliers (Manopt MATLAB toolbox).
- See (Balajewicz, <u>Tezaur</u>, Dowell, 2016) and Appendix slide for Algorithm.





Proposed approach may be interpreted as an <u>*a priori consistent*</u> formulation of the eddy-viscosity turbulence modeling approach.

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- <u>Disadvantages of proposed approach</u>:
 - 1. Off-line calibration of free parameter η is required.



- <u>Advantages of proposed approach</u>:
 - Retains <u>consistency</u> between ROM and Navier-Stokes equations → no additional turbulence terms required.
 - 2. Inherently a <u>nonlinear</u> model \rightarrow should be expected to outperform linear models.
 - 3. Works with <u>any</u> basis and Petrov-Galerkin projection.
- <u>Disadvantages of proposed approach</u>:
 - 1. Off-line calibration of free parameter η is required.
 - 2. Stability cannot be proven like for incompressible case.



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Flow over square cavity at Mach 0.6, Re = 1453.9, Pr = $0.72 \Rightarrow$ n = 4 ROM (91% snapshot energy).



Figure 1: Domain and mesh for viscous channel driven cavity problem.



• Minimizing subspace rotation:

$$f(\mathbf{X}) = \|\mathbf{X} - \mathbf{I}_{(n+p),n}\|_F = -\mathrm{tr}(\mathbf{X}^T \mathbf{I}_{(n+p)\times n})$$



Figure 2: (a) evolution of modal energy, (b) phase plot of first and second temporal basis $a_1(t)$ and $a_2(t)$, (c) illustration of stabilizing rotation showing that rotation is small: $\frac{\|X - I_{(n+p),n}\|_F}{n} = 0.188, X \approx I_{(n+p),n}$





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Figure 3: Pressure power spectral density (PSD) at location x = (2, -1); stabilized ROM minimizes subspace rotation.



• <u>Maximizing resolved TKE</u>:

$$f(\boldsymbol{X}) = -||\boldsymbol{\Sigma} - \boldsymbol{X}\boldsymbol{X}^T\boldsymbol{\Sigma}||_F$$



Figure 4: Pressure power spectral density (PSD) at location x = (2, -1); stabilized ROM maximizes resolved TKE.



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Figure 5: Channel driven cavity Re \approx 1500 contours of *u*-velocity at time of final snapshot.



Flow over square cavity at Mach 0.6, Re = 5452.1, Pr = $0.72 \Rightarrow$ n = 20 ROM (71.8% snapshot energy).



Figure 6: Domain and mesh for viscous channel driven cavity problem.



• Minimizing subspace rotation:

$$f(\mathbf{X}) = \|\mathbf{X} - \mathbf{I}_{(n+p),n}\|_F = -\mathrm{tr}(\mathbf{X}^T \mathbf{I}_{(n+p)\times n})$$



Figure 7: (a) evolution of modal energy, (b) illustration of stabilizing rotation showing that rotation is small: $\frac{\|X - I_{(n+p),n}\|_F}{n} = 0.038, X \approx I_{(n+p),n}$



Figure 8: Pressure cross PSD of of $p(x_1, t)$ and $p(x_2, t)$ where $x_1 = (2, -0.5)$, $x_2 = (0, -0.5)$

Power and phase lag at fundamental frequency, and first two super harmonics are predicted accurately using the fine-tuned ROM (Δ = stabilized ROM, \Box = FOM)





<u>Minimizing subspace rotation</u>:

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Figure 9: Channel driven cavity Re \approx 5500 contours of *u*-velocity at time of final snapshot.

CPU times (CPU-hours) for offline and online computations*

offline

online



	Procedure	Low Re Cavity	Moderate Re Cavity
	FOM # of DOF	288,250	243,750
•	Time-integration of FOM	72 hrs	179 hrs
	Basis construction (size $n + p$ ROM)	0.88 hrs	3.44 hrs
	Galerkin projection (size $n + p$ ROM)	5.44 hrs	14.8 hrs
	Stabilization	14 sec	170 sec
-	ROM # of DOF	4	20
-	Time-integration of ROM	0.16 sec	0.83 sec
	Online computational speed-up	1.6e6	7.8e5

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Significant online computational speed-up!

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- Solving ROM amounts to solving *non-linear least-squares problem*:

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- POD/LSPG ROMs are *more stable* than POD/Galerkin ROMs.
 → Nevertheless, *low-dimensional* LSPG ROMs can benefit from basis stabilization.

Stabilization of Inviscid Pulse in Uniform <a>Flow Low Order LSPG ROM

Preliminary Workflow

- 1. Run LSPG ROM in SPARC \rightarrow output POD basis.
- 2. Use POD/Galerkin ROM code Spirit to produce C, L, and $Q^{(i)}$ matrices in (2).
- 3. Stabilize POD basis using stabilization approach described in this talk.
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- Figure (left) shows *generalized coordinates* for mode 2 compared to FOM projection.
- Our approach effectively *stabilizes* LSPG ROM.

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- Figure (left) shows *generalized coordinates* for mode 2 compared to FOM projection.
- Our approach effectively *stabilizes* LSPG ROM.
- Preliminary approach needs improvement, as there are *inconsistencies* between SPARC and Spirit codes.

We are currently working on extending our stabilization/enhancement approach to ROMs with *generic nonlinearities*.



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Summary



- We have developed a non-intrusive approach for <u>stabilizing</u> and <u>fine-</u> <u>tuning</u> projection-based ROMs for compressible flows.
- The standard POD modes are "<u>rotated</u>" into a more dissipative regime to account for the dynamics in the higher order modes truncated by the standard POD method.
- The new approach is <u>consistent</u> and does not require the addition of empirical turbulence model terms unlike traditional approaches.
- Mathematically, the approach is formulated as a *<u>quadratic matrix</u> program* on the Stiefel manifold.
- The constrained minimization problem is solved <u>offline</u> and <u>small</u> enough to be solved in MATLAB.
- The method is demonstrated on several compressible flow problems and shown to deliver *stable* and *accurate* ROMs.





• Application to *higher Reynolds number* problems.



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- Extension of the proposed approach to problems with <u>generic nonlinearities</u>, where the ROM involves some form of hyper-reduction (e.g., DEIM, gappy POD).



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- Extension of the method to *minimal-residual-based* nonlinear ROMs.
- Extension of the method to <u>predictive applications</u>, e.g., problems with varying Reynolds number and/or Mach number.



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- Extension of the proposed approach to problems with <u>generic nonlinearities</u>, where the ROM involves some form of hyper-reduction (e.g., DEIM, gappy POD).
- Extension of the method to *minimal-residual-based* nonlinear ROMs.
- Extension of the method to <u>predictive applications</u>, e.g., problems with varying Reynolds number and/or Mach number.
- Selecting different <u>goal-oriented</u> objectives and constraints in our optimization problem:

minimize_{$$X \in \mathcal{V}_{(n+p),n}$$} $f(X)$
subject to $g(X, L) = 0$

e.g.,

- Maximize parametric robustness: $f = \sum_{i=1}^{k} \beta_i \| \boldsymbol{U}^*(\mu_i) \boldsymbol{X} \boldsymbol{U}^*(\mu_i) \|_F$.
- ODE constraints: $g = ||\mathbf{a}(t) \mathbf{a}^*(t)||$.

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Appendix: Accounting for modal truncation Sandia Laboratories

Stabilization algorithm: returns stabilizing rotation matrix X.

Inputs: Initial guess $\eta^{(0)} = tr(L(1:n,1:n))$ ($\mathbf{X} = \mathbf{I}_{(n+p) \times n}$), ROM size n and $p \ge 1$, ROM matrices associated with the first n + p most energetic POD modes, convergence tolerance *TOL*, maximum number of iterations k_{max} .

for $k = 0, \cdots, k_{max}$

Solve constrained optimization problem on Stiefel manifold:

$$\begin{array}{ll} \underset{\boldsymbol{X}^{(k)} \in \mathcal{V}_{(n+p),n}}{\text{minimize}} & -\operatorname{tr}\left(\boldsymbol{X}^{(k)\mathrm{T}}\boldsymbol{I}_{(n+p)\times n}\right)\\ \\ \underset{\text{subject to}}{\text{subject to}} & \operatorname{tr}(\boldsymbol{X}^{(k)\mathrm{T}}\boldsymbol{L}\boldsymbol{X}^{(k)}) = \eta^{(k)}. \end{array}$$

Construct new Galerkin matrices using (4). Integrate numerically new Galerkin system. Calculate "modal energy" $E(t)^{(k)} = \sum_{i}^{n} (a(t)_{i}^{(k)})^{2}$. Perform linear fit of temporal data $E(t)^{(k)} \approx c_{1}^{(k)} t + c_{0}^{(k)}$, where $c_{1}^{(k)} =$ energy growth. Calculate ϵ such that $c_{1}^{(k)}(\epsilon) = 0$ (no energy growth) using root-finding algorithm. Perform update $\eta^{(k+1)} = \eta^{(k)} + \epsilon$. if $||c_{1}^{(k)}|| < TOL$ $\mathbf{X} := \mathbf{X}^{(k)}$. terminate the algorithm. end

end

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• We are interested in the *compressible captive-carry problem*.



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- Desired numerical properties of ROMs:
 - *Consistency* (w.r.t. the continuous PDEs).
 - **Stability:** if full order model (FOM) is stable, ROM should be stable.
 - *Convergence:* requires consistency and stability.
 - Accuracy (w.r.t. FOM).
 - Efficiency.
 - *Robustness* (w.r.t. time or parameter changes).

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Stability can be a real problem for compressible flow ROMs!