



# Energy-Stable Galerkin Reduced Order Models for Prediction and Control of Fluid Systems

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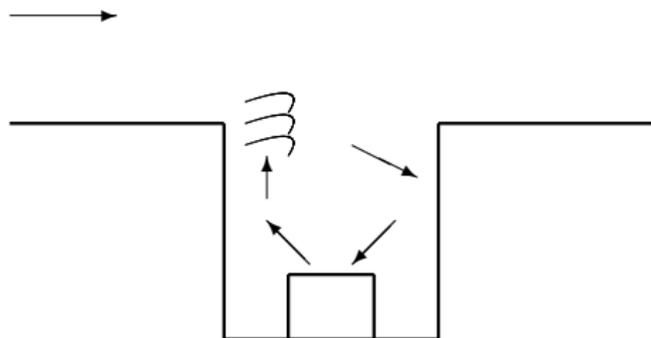
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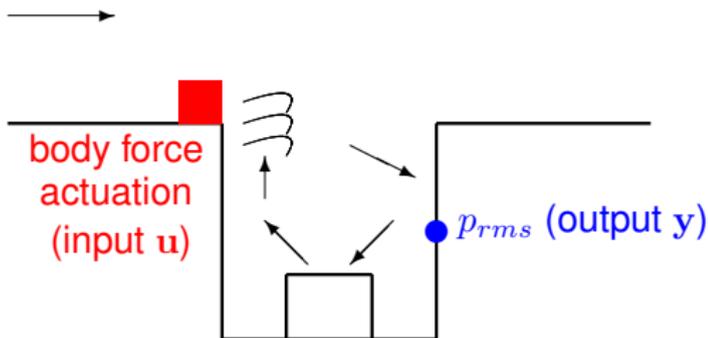
# Target Cavity Flow Control Problem



- **Configuration/Plant:** compressible non-linear fluid flow over open cavity containing components.



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- **Configuration/Plant:** compressible non-linear fluid flow over open cavity containing components.
- **Physical Control Problem:** using upstream actuation, control oscillations within cavity caused by pressure fluctuations propagating between downstream wall and shear layer.
- **Mathematical Control Problem:** compute optimal body-force actuation input  $\mathbf{u}_{opt}$  to minimize the RMS pressure halfway up the downstream wall.

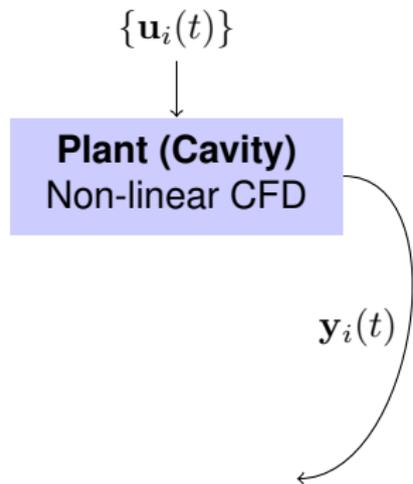
$$\text{input } \mathbf{u} : \mathbf{q}^T = ( 0, f(t), 0 \ 0 \ 0 )^T$$
$$\text{output } y : p_{rms} = \sqrt{\frac{1}{K} \sum_{i=1}^K (p(t_k) - \bar{p})^2}$$

# ROM-Based Cavity Flow Control Road Map

- 1 Collect snapshots from non-linear high-fidelity CFD cavity simulation

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}_i), \quad \mathbf{y}_i = \mathbf{h}(\mathbf{x}, \mathbf{u}_i)$$

for some set of inputs  $\{\mathbf{u}_i(t)\}$ , and construct empirical basis (POD, BPOD) from this snapshot set.



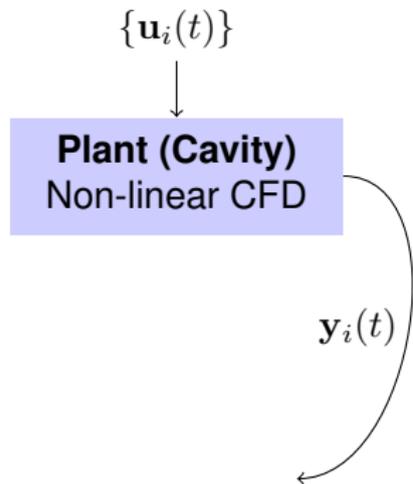
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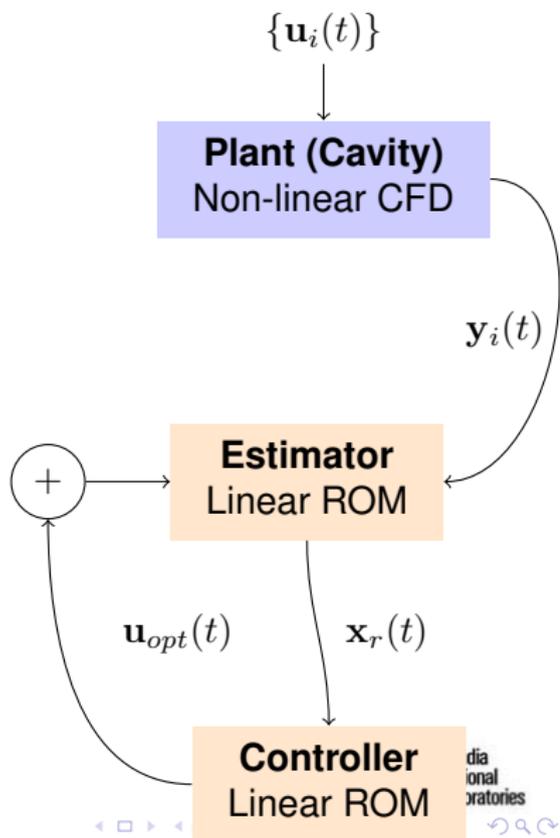
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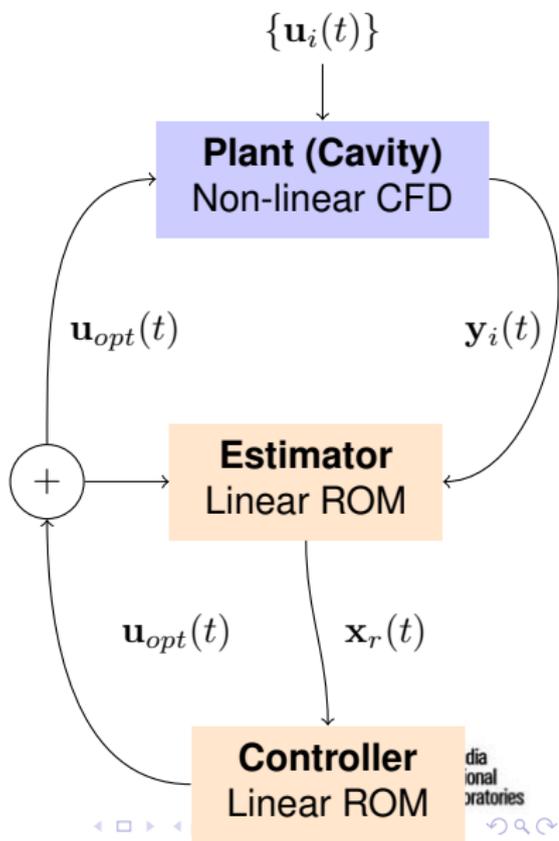
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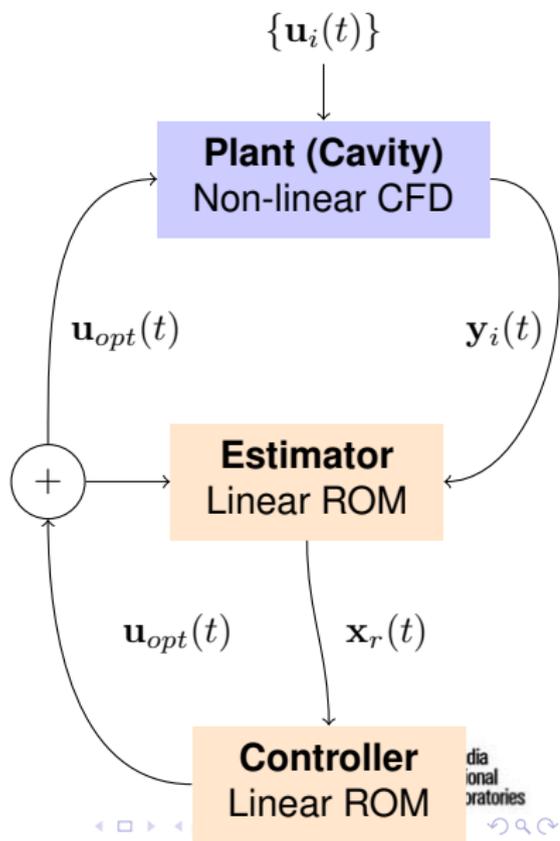
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- 2 Build a ROM for the fluid system, or ***approximation of fluid system.***
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# 3D Full (Non-Linear) Compressible Navier-Stokes Equations

- 3D compressible Navier-Stokes equations:

$$\begin{aligned}\rho \frac{Du_1}{dt} &= -\frac{\partial p}{\partial x_1} + \sum_{j=1}^3 \frac{\partial}{\partial x_j} \left\{ \mu \left( \frac{\partial u_1}{\partial x_j} + \frac{\partial u_j}{\partial x_1} \right) + \lambda \delta_{1j} \nabla \cdot \mathbf{u} \right\}, \\ \rho \frac{Du_2}{dt} &= -\frac{\partial p}{\partial x_2} + \sum_{j=1}^3 \frac{\partial}{\partial x_j} \left\{ \mu \left( \frac{\partial u_2}{\partial x_j} + \frac{\partial u_j}{\partial x_2} \right) + \lambda \delta_{2j} \nabla \cdot \mathbf{u} \right\}, \\ \rho \frac{Du_3}{dt} &= -\frac{\partial p}{\partial x_3} + \sum_{j=1}^3 \frac{\partial}{\partial x_j} \left\{ \mu \left( \frac{\partial u_3}{\partial x_j} + \frac{\partial u_j}{\partial x_3} \right) + \lambda \delta_{3j} \nabla \cdot \mathbf{u} \right\}, \\ \rho C_v \frac{DT}{dt} &= -p \nabla \cdot \mathbf{u} + \sum_{i=1}^3 \frac{\partial}{\partial x_i} \left( \kappa \frac{\partial T}{\partial x_i} \right), \\ \frac{D\rho}{dt} &= -\rho \nabla \cdot \mathbf{u}.\end{aligned}\tag{1}$$

- ROM approach is based on local linearization of full non-linear equations (1):
  - ▶ Full non-linear equations (1) are solved to generate snapshots in high-fidelity code.
  - ▶ Linearized approximation of (1) is projected onto reduced basis modes in building the ROM.

# 3D Linearized Compressible Navier-Stokes Equations

- Appropriate when a compressible fluid system can be described by viscous, small-amplitude perturbations about a steady-state mean (or base) flow.
- Linearization of full compressible Navier-Stokes equations:

$$\mathbf{q}^T(\mathbf{x}, t) \equiv (u_1, u_2, u_3, T, \rho) \equiv \underbrace{\bar{\mathbf{q}}^T(\mathbf{x})}_{\text{mean}} + \underbrace{\mathbf{q}'^T(\mathbf{x}, t)}_{\text{fluctuation}} \in \mathbb{R}^5$$

- ▶ **Simplest linearization:** neglect  $\nabla \bar{\mathbf{q}}$  terms (uniform base flow)

$$\mathbf{q}'_{,t} + \mathbf{A}_i(\bar{\mathbf{q}})\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} = \mathbf{F}$$

- ▶ **More accurate linearization:** retain  $\nabla \bar{\mathbf{q}}$  terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla \bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla \bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

$\mathbf{A}_i(\bar{\mathbf{q}})$  : convective flux matrices  
 $\mathbf{K}_{ij}(\bar{\mathbf{q}})$  : diffusive flux matrices  
 $\mathbf{K}_i^{vw}(\bar{\mathbf{q}})$  : viscous work matrices



# Outline

This talk focuses on how to construct a Galerkin ROM that is **stable** *a priori*

- 1 Stability Definitions
- 2 POD/Galerkin Approach to Model Reduction
- 3 Energy-Stable ROMs for Linearized Compressible Flow
  - Stability via Continuous Projection
  - Stability via Discrete Projection
- 4 Numerical Experiments
  - Implementation
  - Driven Pulse in Uniform Base Flow
  - Laminar Viscous Driven Cavity
- 5 Summary & Future Work
- 6 References
- 7 Appendix

# Energy-Stability

- **Practical Definition:** Numerical solution does not “blow up” in finite time.

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Numerical solutions **must** maintain a proper energy balance





# Connection to Lyapunov Stability\*

$$\dot{\mathbf{x}}_N = \mathbf{f}_N(\mathbf{x}_N), \quad \mathbf{x}_N \in \mathbb{R}^N$$

- **Lyapunov Stability:** If there exists a **Lyapunov function**  $V$  such that
  - ▶  $V > 0$  (positive-definite), and
  - ▶  $\frac{dV}{dt} = \frac{dV}{dx} \mathbf{f}(\mathbf{x}) \leq 0$  (negative semi-definite along system trajectories)in  $B_r(\mathbf{x}_s)$ , then  $\mathbf{x}_s$  is **locally stable in the sense of Lyapunov** [8].

- **Energy Stability:** Let

$$E_N \equiv \frac{1}{2} \|\mathbf{x}_N\|^2$$

denote the system energy. If

$$\frac{dE_N}{dt} \leq 0$$

the system is **energy-stable**.

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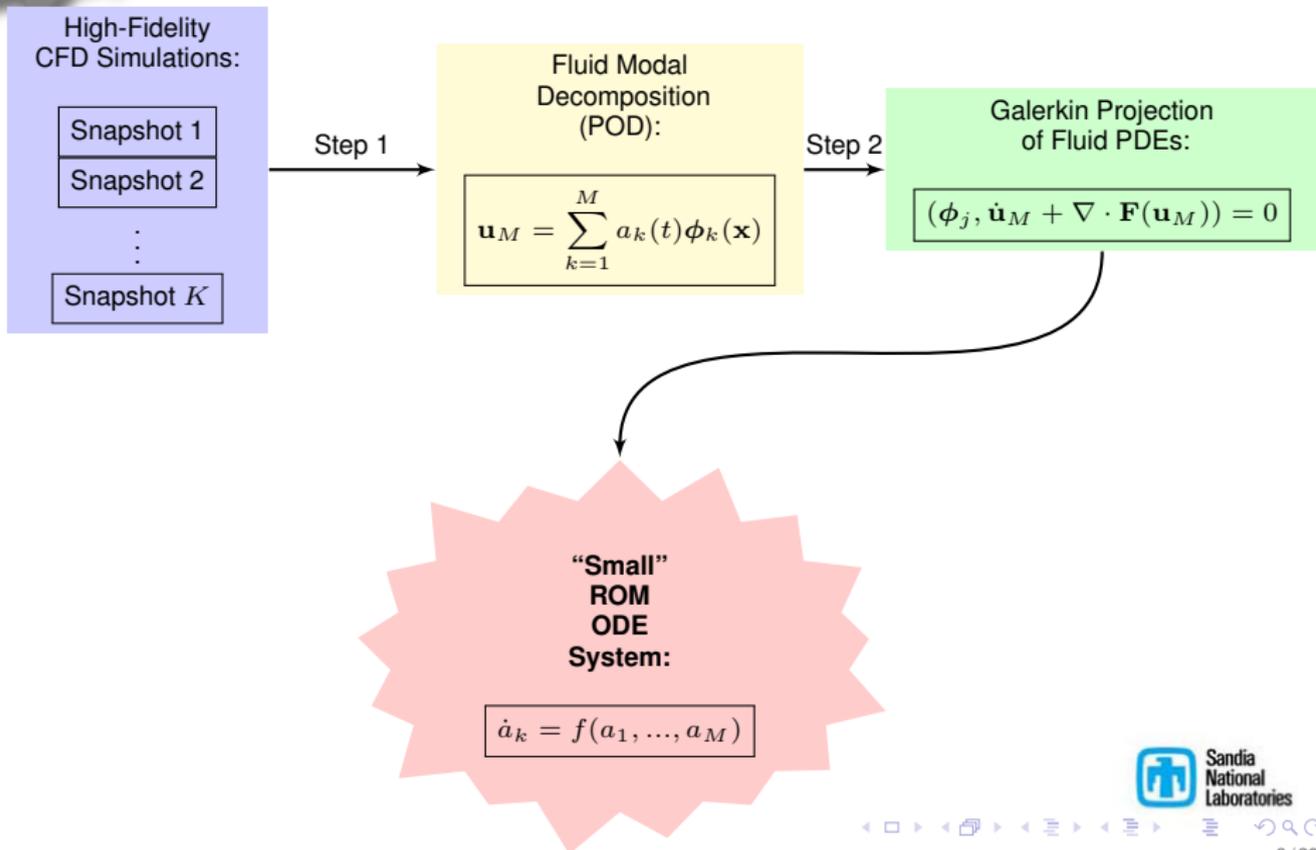
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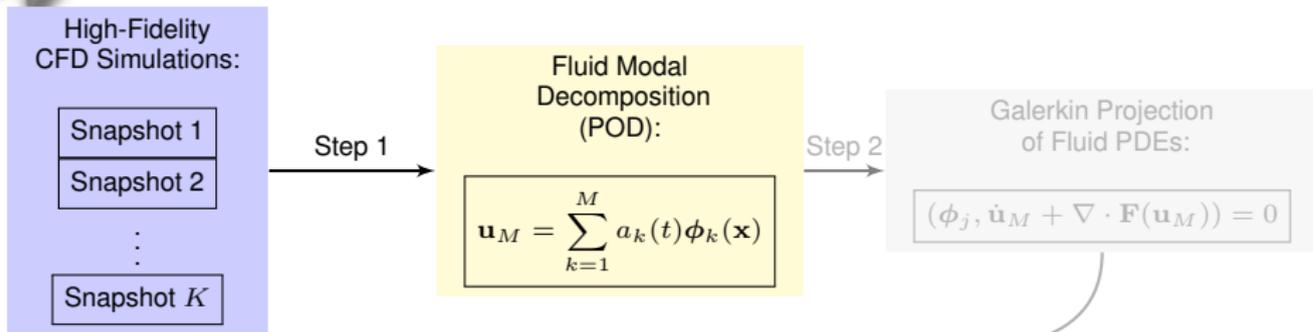
**Remark:** System energy  $E_N$  satisfies the definition of a Lyapunov function!

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# Model Reduction Approach



# Step 1: Constructing the Modes



- **POD basis**  $\{\phi_i\}_{i=1}^M$  with  $M \ll K$  maximizes the energy in the projection of snapshots onto  $\text{span}\{\phi_i\}$ .

- **POD SVD problem:**

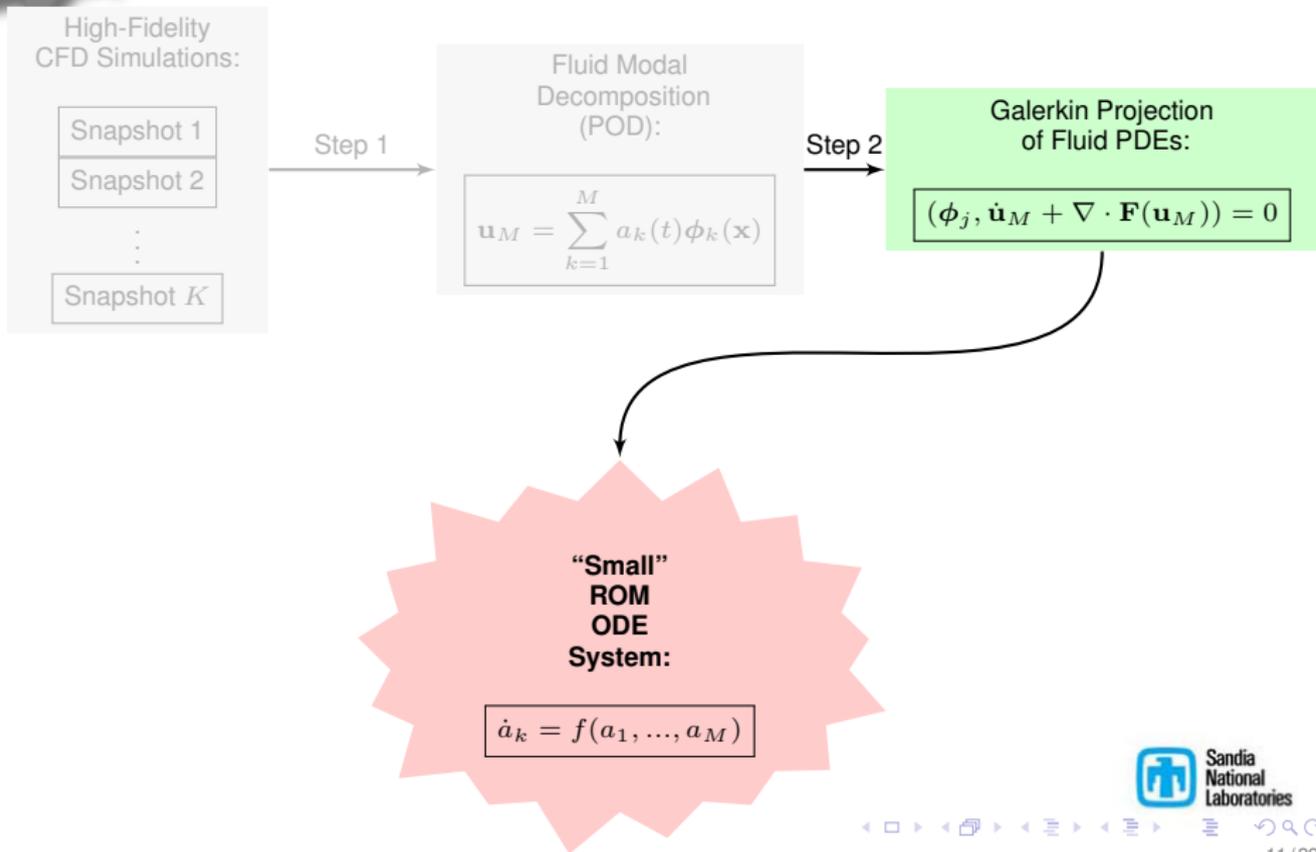
$$\mathbf{X} = \mathbf{U}\Sigma\mathbf{V}^T$$

$$(\phi_1, \dots, \phi_M) = \mathbf{U}(:, 1 : M)$$

“Small”  
ROM  
ODE  
System:

$$\dot{a}_k = f(a_1, \dots, a_M)$$

# Step 2: Galerkin Projection



# Discrete vs. Continuous Projection

## DISCRETE APPROACH

Governing Equations

$$\mathbf{u}_t = \mathcal{L}u$$



CFD Model

$$\dot{\mathbf{u}}_N = \mathbf{A}_N \mathbf{u}_N$$



Discrete Modal Basis  $\Phi$



Projection of CFD Model  
(Matrix Operation)



ROM

$$\dot{\mathbf{a}} = \Phi^T \mathbf{A}_N \Phi \mathbf{a}$$

## CONTINUOUS APPROACH

Governing Equations

$$\mathbf{u}_t = \mathcal{L}u$$



CFD Model

$$\dot{\mathbf{u}}_N = \mathbf{A}_N \mathbf{u}_N$$



Continuous Modal Basis\*  $\phi_j(\mathbf{x})$



Projection of Governing Equations  
(Numerical Integration)



ROM

$$\dot{a}_j = (\phi_j, \mathcal{L}\phi_k) a_k$$

\* Continuous functions space is defined using finite elements.

# Energy-Stable ROM via Continuous Projection

Energy stability of the Galerkin ROM can be proven [1] following “symmetrization” the linearized compressible Navier-Stokes equations.

- Linearized compressible Navier-Stokes system is “symmetrizable” [5].
- Pre-multiply equations by symmetric positive definite matrix:

$$\mathbf{H} \equiv \begin{pmatrix} \bar{\rho} & 0 & 0 & 0 & 0 \\ 0 & \bar{\rho} & 0 & 0 & 0 \\ 0 & 0 & \rho & 0 & 0 \\ 0 & 0 & 0 & \frac{\bar{\rho}R}{T(\gamma-1)} & 0 \\ 0 & 0 & 0 & 0 & \frac{R\bar{T}}{\bar{\rho}} \end{pmatrix} \Rightarrow \mathbf{H}\mathbf{q}'_{,t} + \mathbf{H}\mathbf{A}_i \mathbf{q}'_{,i} - \mathbf{H}[\mathbf{K}_{ij}\mathbf{q}'_{,i}]_{,j} + \dots = \mathbf{F}$$

- $\mathbf{H}$  is called the “symmetrizer” of the system:
  - ▶ The convective flux matrices  $\mathbf{H}\mathbf{A}_i$  are all symmetric.
  - ▶ The following augmented viscosity matrix

$$\mathbf{K}^S \equiv \begin{pmatrix} \mathbf{H}\mathbf{K}_{11} & \mathbf{H}\mathbf{K}_{12} & \mathbf{H}\mathbf{K}_{13} \\ \mathbf{H}\mathbf{K}_{21} & \mathbf{H}\mathbf{K}_{22} & \mathbf{H}\mathbf{K}_{23} \\ \mathbf{H}\mathbf{K}_{31} & \mathbf{H}\mathbf{K}_{32} & \mathbf{H}\mathbf{K}_{33} \end{pmatrix},$$

is symmetric positive semi-definite.

# Symmetry Inner Product & A Stable Galerkin ROM

- Define the “symmetry” inner product and “symmetry” norm:

$$(\mathbf{q}'^{(1)}, \mathbf{q}'^{(2)})_{(\mathbf{H}, \Omega)} \equiv \int_{\Omega} [\mathbf{q}'^{(1)}]^T \mathbf{H} \mathbf{q}'^{(2)} d\Omega, \quad \|\mathbf{q}'\|_{(\mathbf{H}, \Omega)} \equiv (\mathbf{q}', \mathbf{q}')_{(\mathbf{H}, \Omega)} \quad (2)$$

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- Uniform base flow case:** non-increasing energy in Galerkin approximation

$$\mathbf{q}'_M = \sum_{i=1}^M a_k(t) \phi_k(\mathbf{x})$$

$$\frac{dE_M}{dt} \equiv \frac{1}{2} \frac{d}{dt} \|\mathbf{q}'_M(\mathbf{x}, t)\|_{(\mathbf{H}, \Omega)} \leq 0$$

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- General case:** Galerkin approximation satisfies same energy expression as solutions to the continuous PDEs

$$\|\mathbf{q}'_M(\mathbf{x}, t)\|_{(\mathbf{H}, \Omega)} \leq e^{\beta t} \|\mathbf{q}'_M(\mathbf{x}, 0)\|_{(\mathbf{H}, \Omega)}$$

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## Practical Implication:

Symmetry inner product ensures Galerkin projection step of the ROM is stable (provided system is in stable state) for **any** basis!

# Energy-Stable ROM via Discrete Projection

Symmetry inner product has discrete analog!

- Consider linear discrete (i.e., discretized in space) stable full order system

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} \quad (3)$$

- Lyapunov function for (3):  $V(\mathbf{x}) = \mathbf{x}^T \mathbf{P}\mathbf{x}$  where  $\mathbf{P}$  is the solution of the Riccati equation:

$$\mathbf{A}^T \mathbf{P} + \mathbf{P}\mathbf{A} = -\mathbf{Q} \quad (4)$$

- S.p.d. solution to (4) exists if  $\mathbf{Q}$  is s.p.d. and  $\mathbf{A}$  is stable [8].
- Solution to (4) can be obtained using MATLAB control toolbox:

$$P = \text{lyap}(A', Q, [] \text{speye}(n, n));$$

- Discrete analog of symmetry inner-product: **Lyapunov inner product**

$$(\mathbf{x}_1, \mathbf{x}_2)_P \equiv \mathbf{x}_1^T \mathbf{P}\mathbf{x}_2$$

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$$(\mathbf{x}_1, \mathbf{x}_2)_{\mathbf{P}} \equiv \mathbf{x}_1^T \mathbf{P}\mathbf{x}_2$$

- Can show: if ROM for (3) is constructed in Lyapunov inner product,

$$\frac{dE_M}{dt} \equiv \frac{1}{2} \frac{d}{dt} \|\mathbf{x}_M\|_2^2 \leq 0$$

# Energy-Stable ROM via Discrete Projection: vs. Continuous Projection

## Symmetry Inner Product (Continuous)

$$(\mathbf{q}'^{(1)}, \mathbf{q}'^{(2)})_{(\mathbf{H}, \Omega)} \equiv \int_{\Omega} [\mathbf{q}'^{(1)}]^T \mathbf{H} \mathbf{q}'^{(2)} d\Omega$$

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$$\mathbf{q}'_{,t} + \mathbf{A}_i \mathbf{q}'_{,i} - [\mathbf{K}_{ij} \mathbf{q}'_{,i}]_{,j} + \dots = \mathbf{F}$$

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- Equation-specific ( $\Rightarrow$  embedded algorithm).
- Known analytically in closed form.

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- Undefined for unstable systems.
- Induced by Lyapunov function for system.
- Black-box.
- Computed numerically by solving Riccati equation ( $\mathcal{O}(N^3)$  ops).

## • Stability-Preserving Discrete Implementation of ROM:

- ▶ ROM is implemented in a C++ code that uses distributed vector and matrix data structures and parallel eigensolvers from the `Trilinos` project [7].
- ▶ POD modes defined using piecewise smooth finite elements.
- ▶ Gauss quadrature rules of sufficient accuracy are used to compute exactly inner products with the help of `libmesh` library.

ROM code is potentially compatible with any CFD code that can output a mesh and snapshot data stored at the nodes of this mesh.

## • High-fidelity CFD Code: SIGMA CFD

- ▶ Sandia in-house finite volume flow solver derived from LESLIE3D [6], a LES flow solver originally developed in the Computational Combustion Laboratory at Georgia Tech.
- ▶ Solves the turbulent compressible flow equations using an explicit 2-4 MacCormack scheme.
- ▶ A hybrid scheme coupling the MacCormack scheme to flux difference splitting schemes is employed to capture shocks.

# Driven Pulse in a Uniform Base Flow

- Uniform base flow in  $\Omega = (-1, 1)^2$ :

$$\bar{p} = 10.1325 \text{ Pa}$$

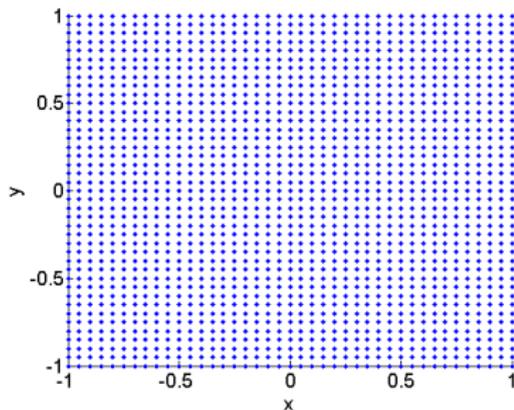
$$\bar{T} = 300 \text{ K}$$

$$\bar{\rho} = \frac{\bar{p}}{RT} = 1.17 \times 10^{-4} \text{ kg/m}^3$$

$$\bar{u}_1 = \bar{u}_2 = \bar{u}_3 = 0.0 \text{ m/s}$$

$$\bar{c} = 347.9693 \text{ m/s.}$$

- Slip wall boundary conditions applied on all boundaries of  $\Omega$ .



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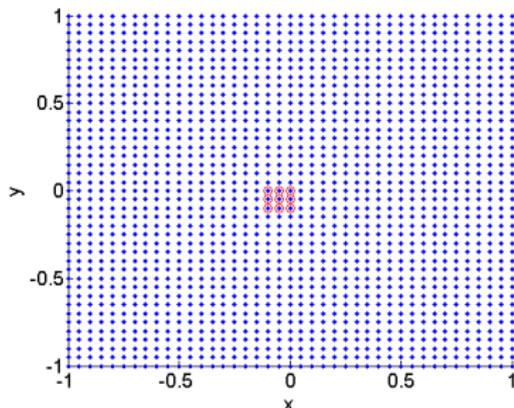
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- Slip wall boundary conditions applied on all boundaries of  $\Omega$ .
- Force for  $y$ -momentum equation drives the flow:

$$F_v(\mathbf{x}, t) = (1 \times 10^{-4}) \cos(2000\pi t), \quad \mathbf{x} \in (-0.1, 0)^2$$



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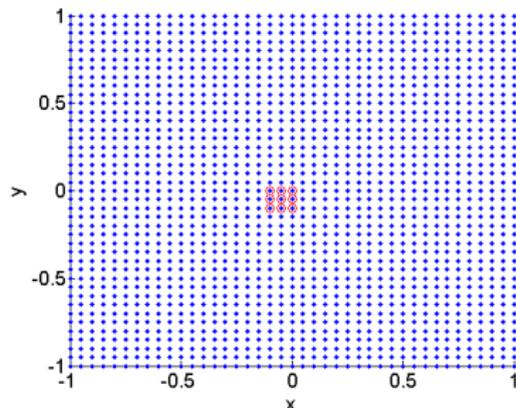
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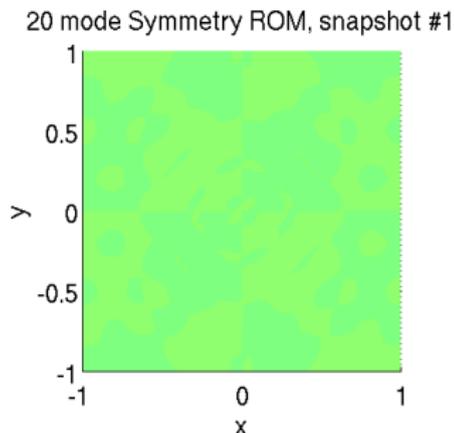
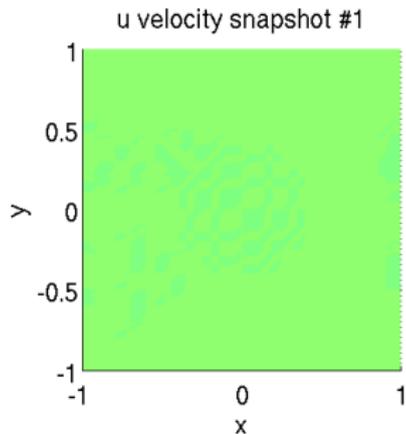
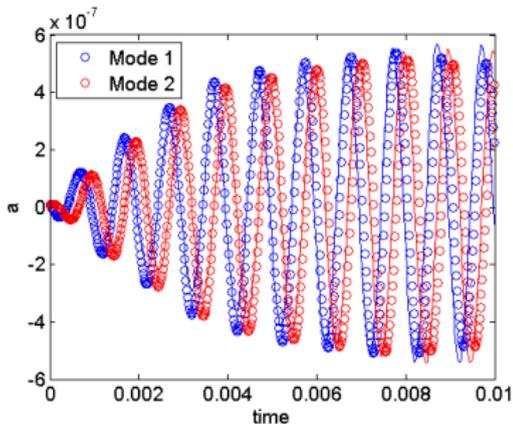
$$F_v(\mathbf{x}, t) = (1 \times 10^{-4}) \cos(2000\pi t), \quad \mathbf{x} \in (-0.1, 0)^2$$

- High-fidelity CFD simulation run on 3362 node mesh until time  $T = 0.5$  seconds.
- 2500 snapshots (saved every  $2 \times 10^{-5}$  seconds), used to construct a 20 mode POD basis.



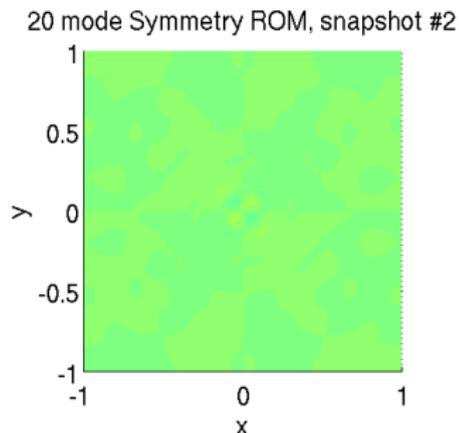
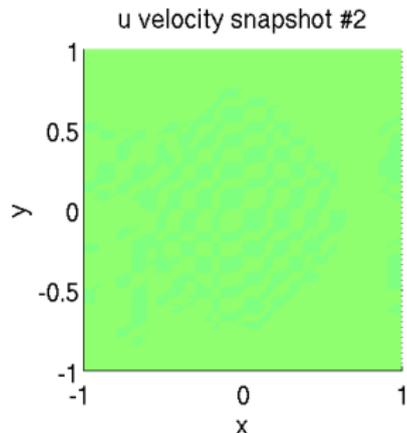
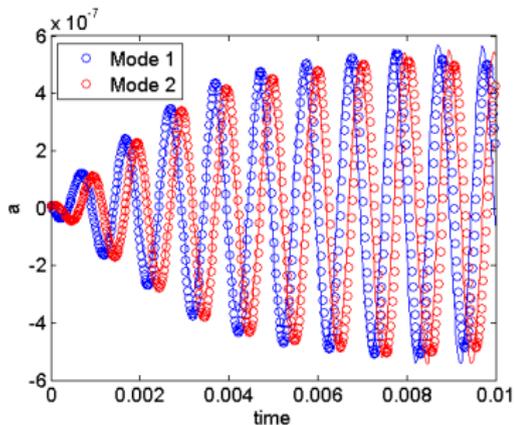
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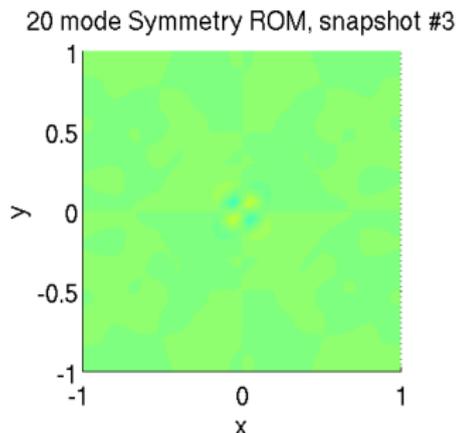
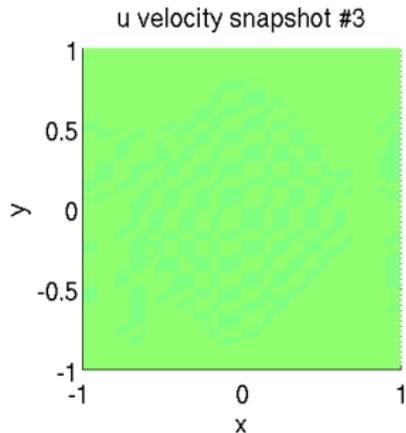
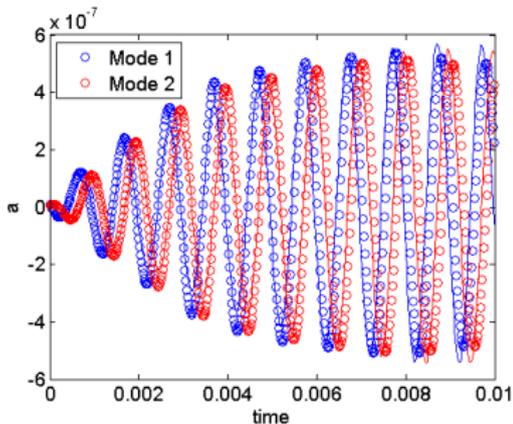
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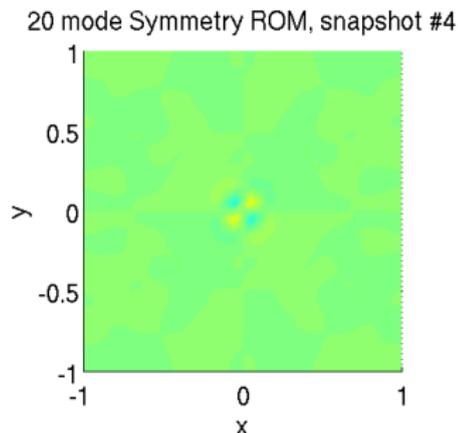
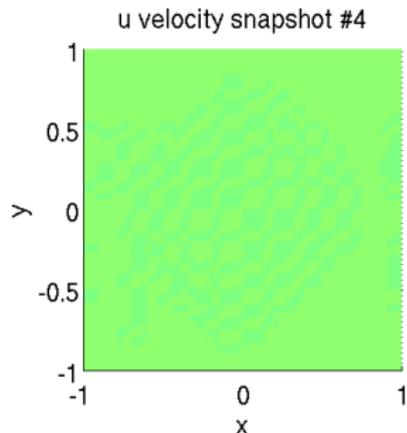
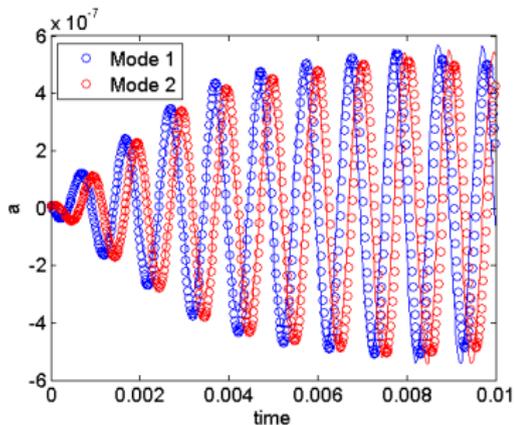
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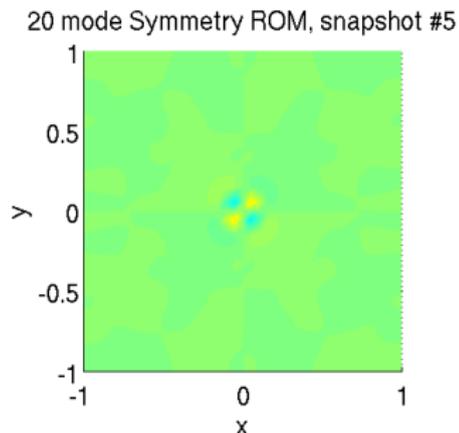
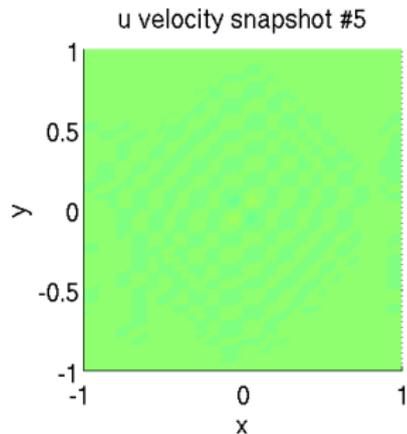
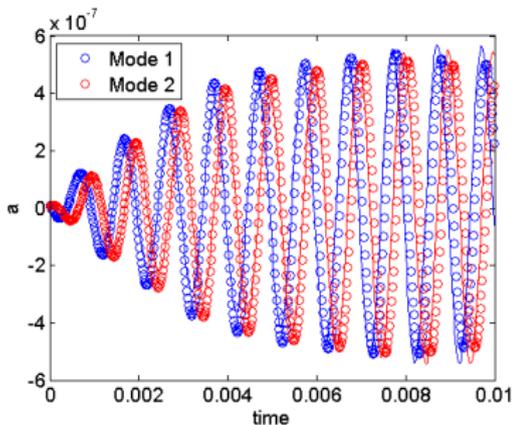
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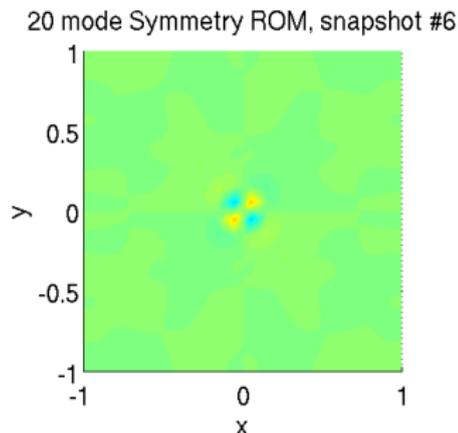
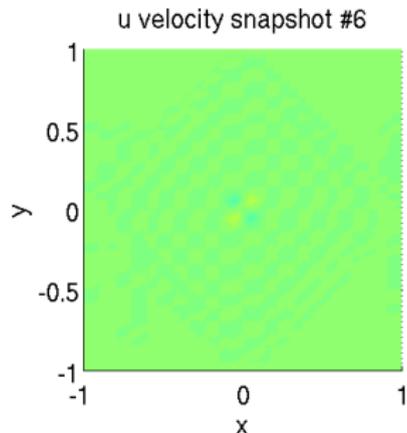
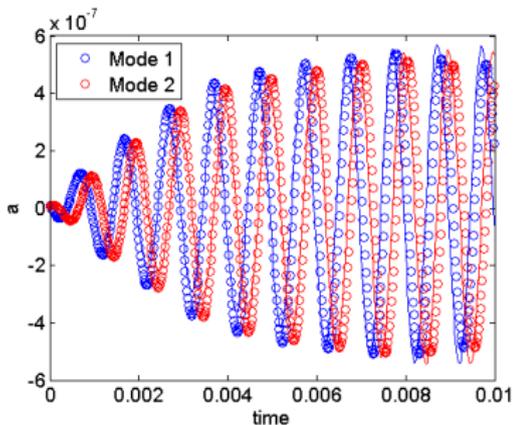
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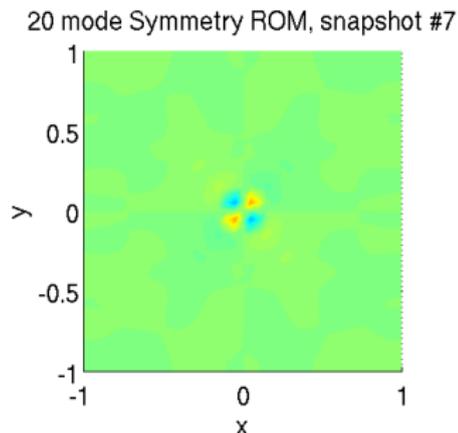
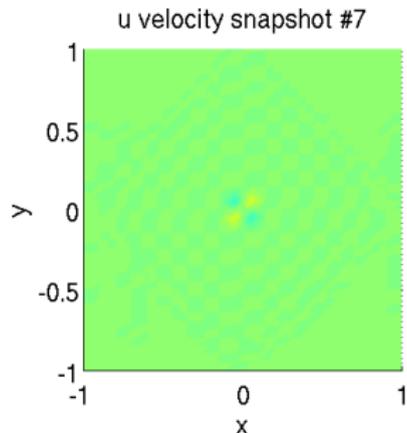
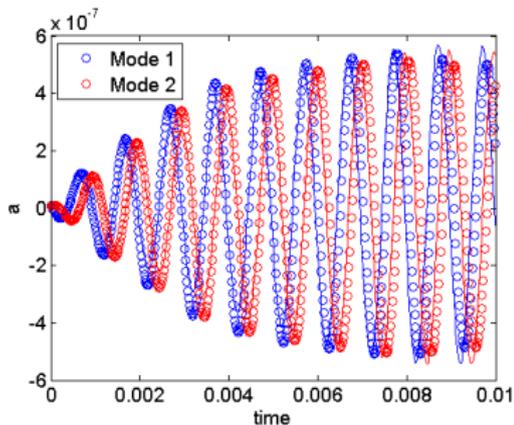
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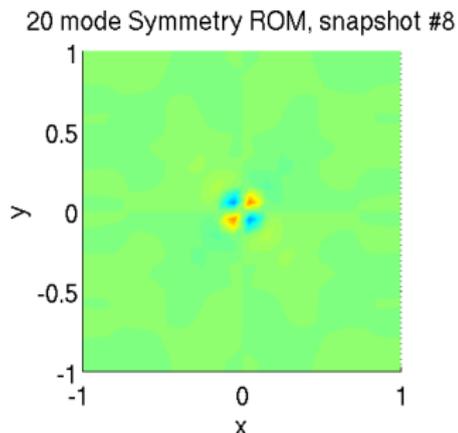
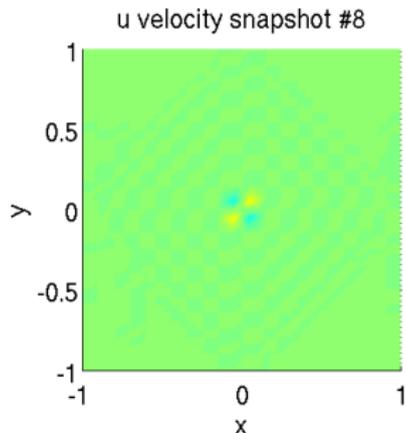
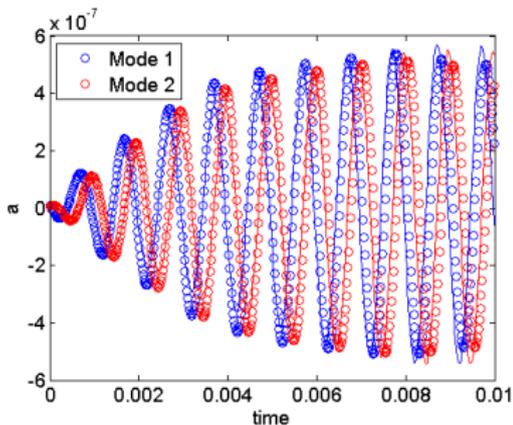
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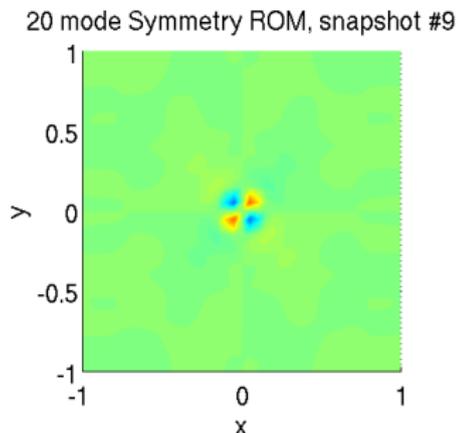
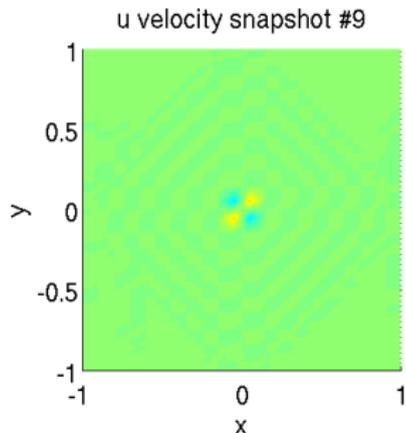
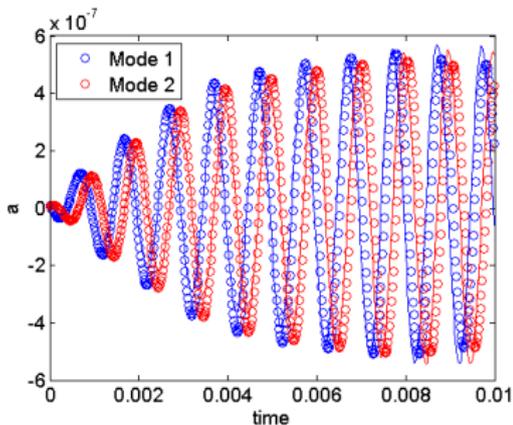
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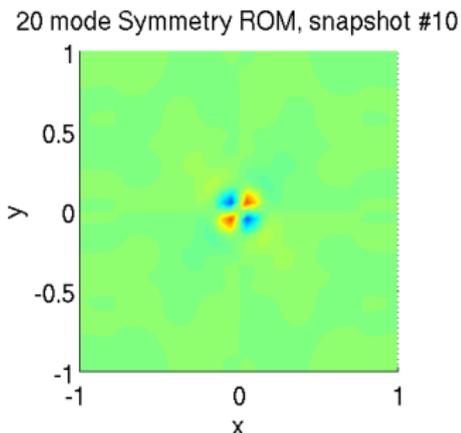
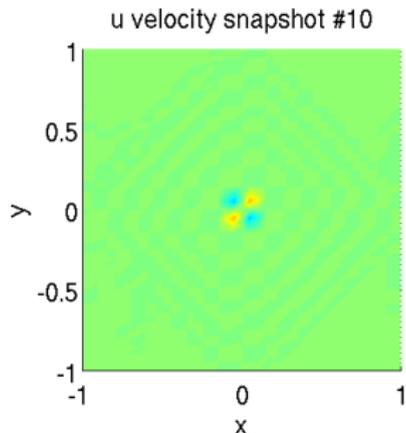
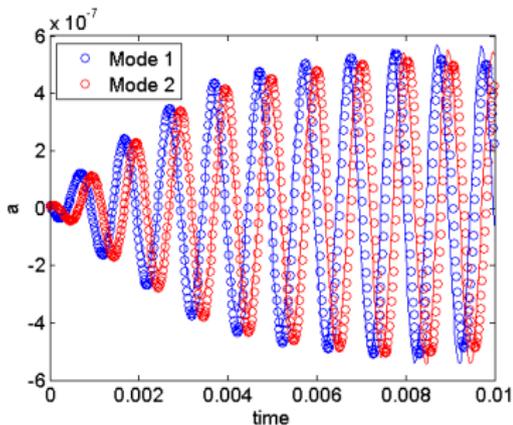
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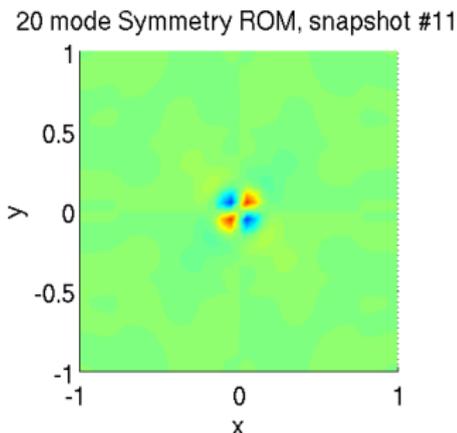
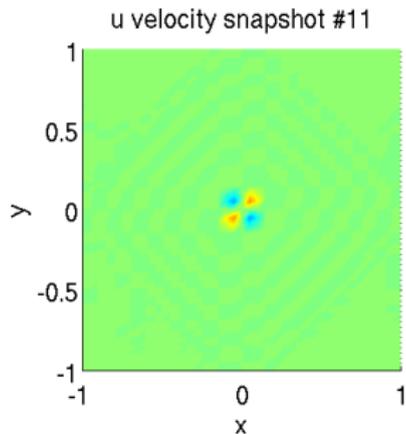
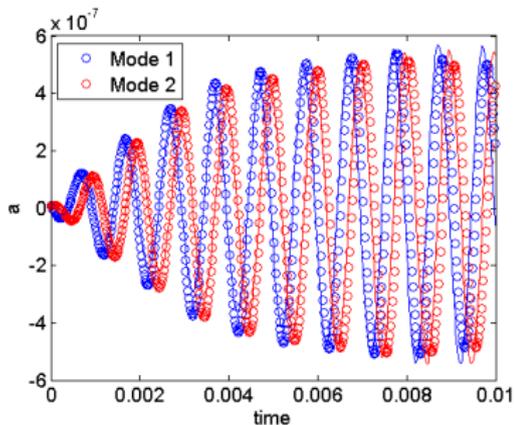
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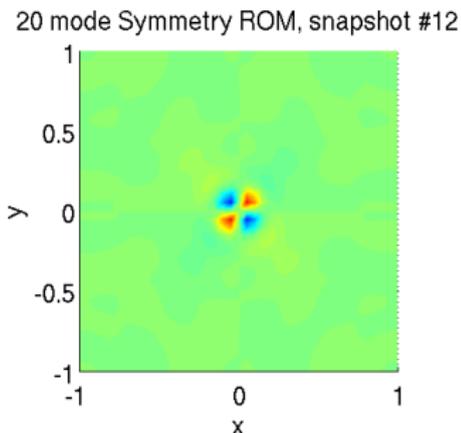
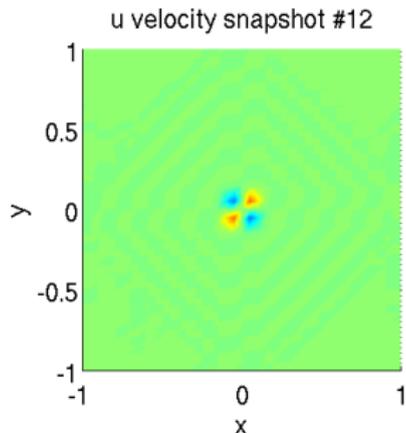
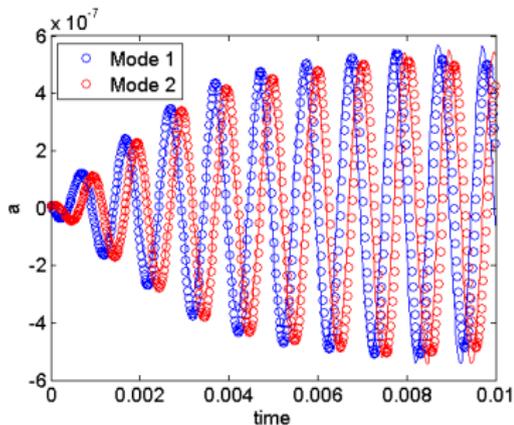
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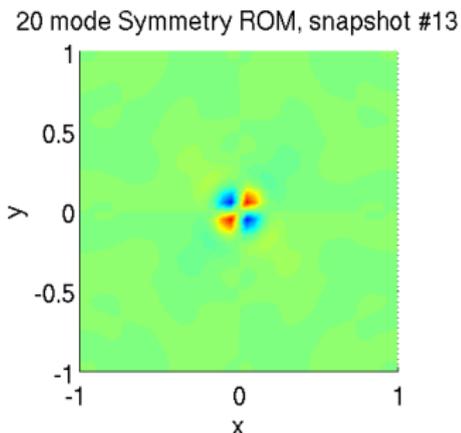
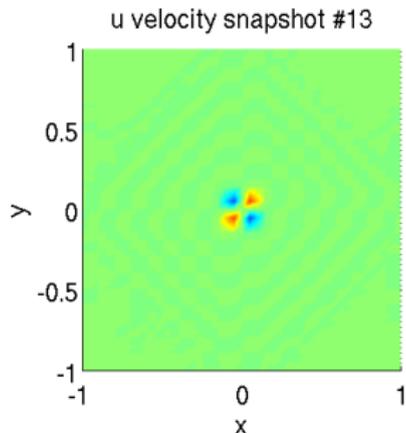
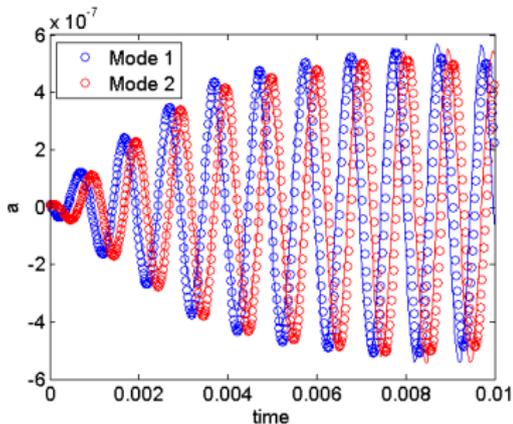
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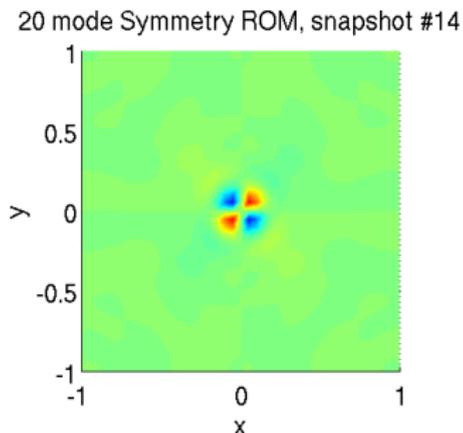
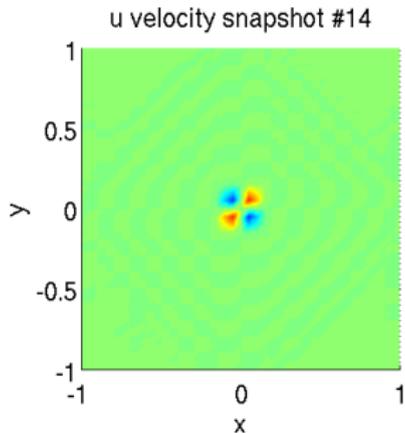
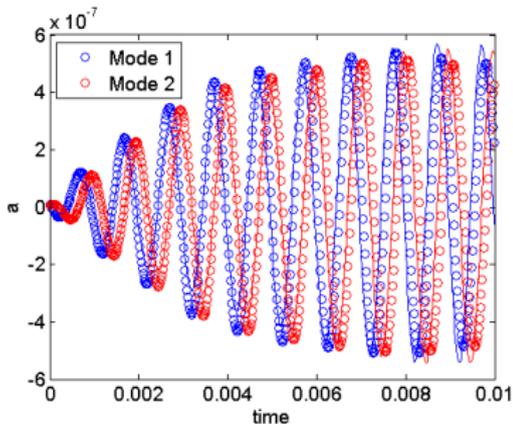
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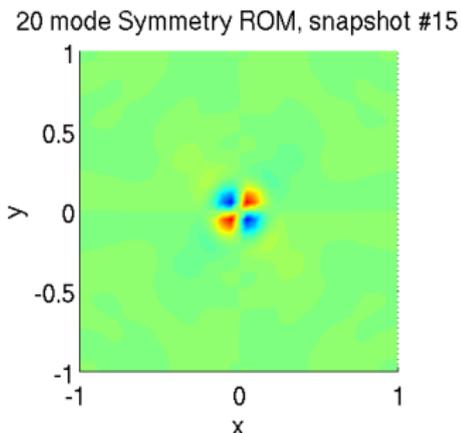
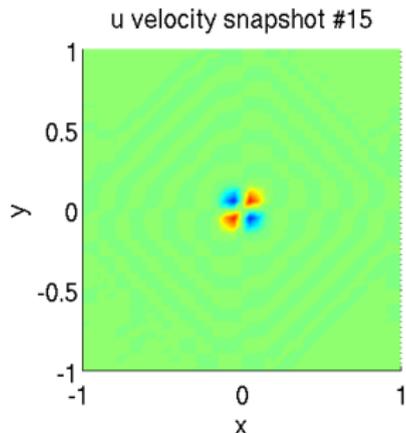
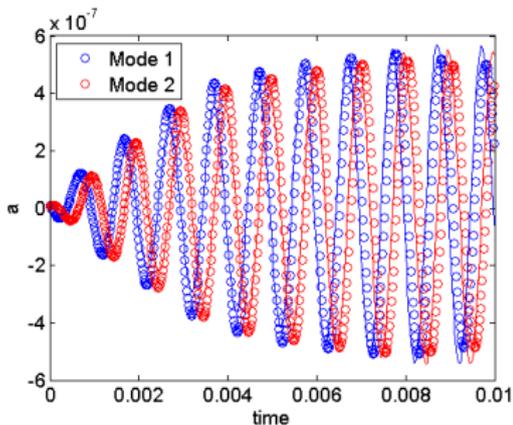
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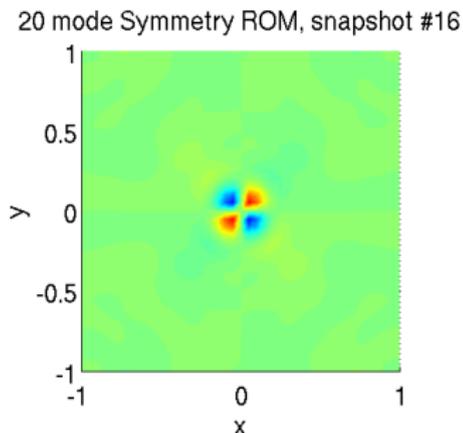
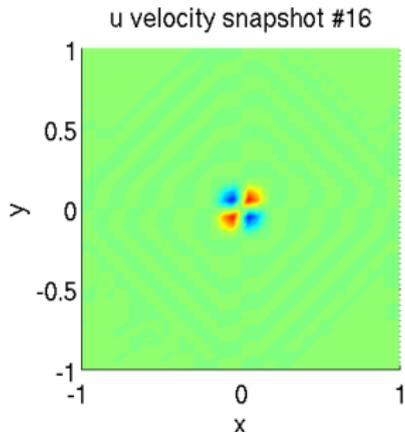
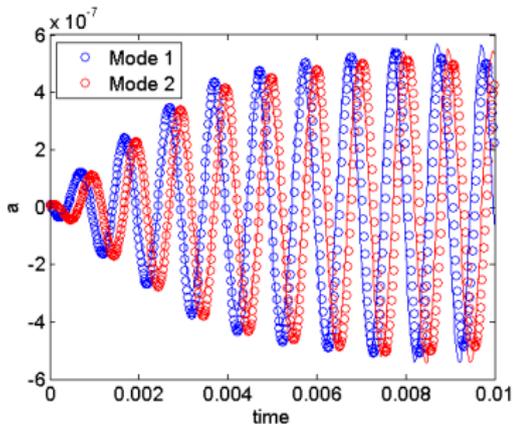
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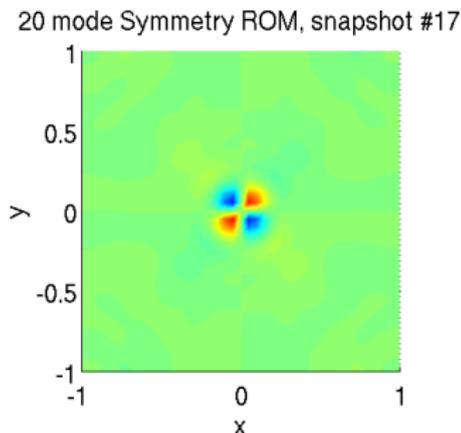
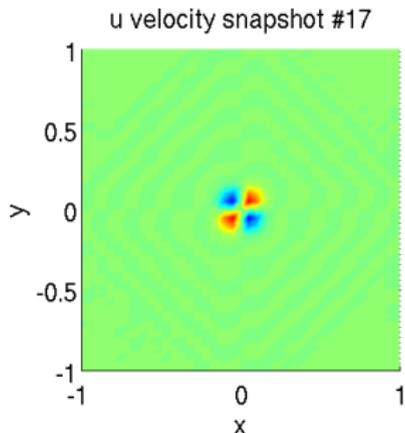
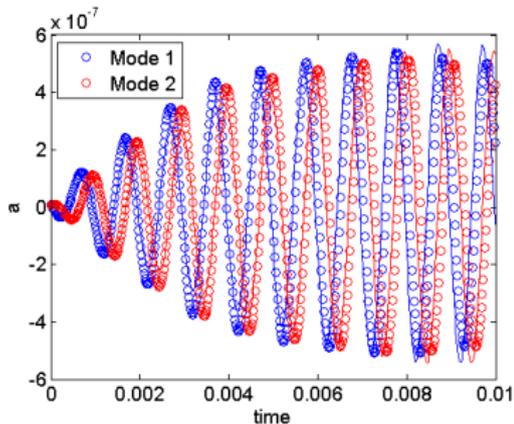
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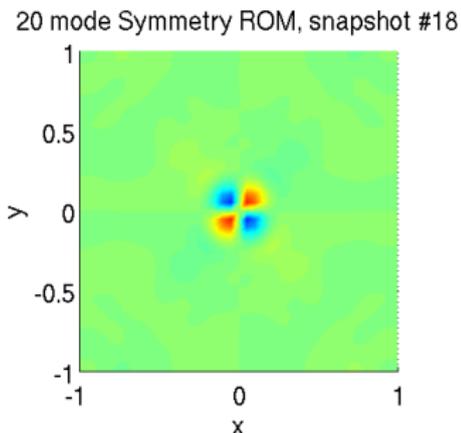
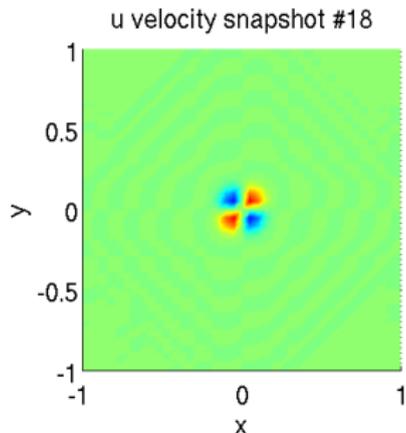
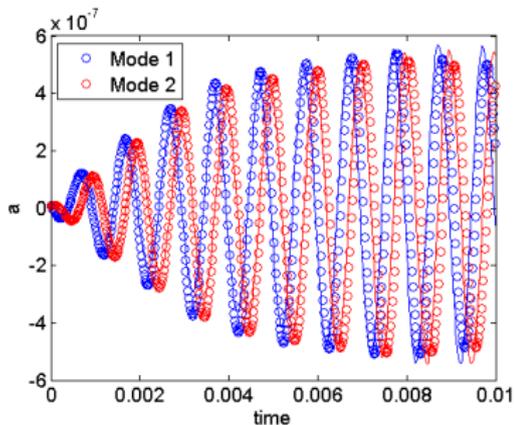
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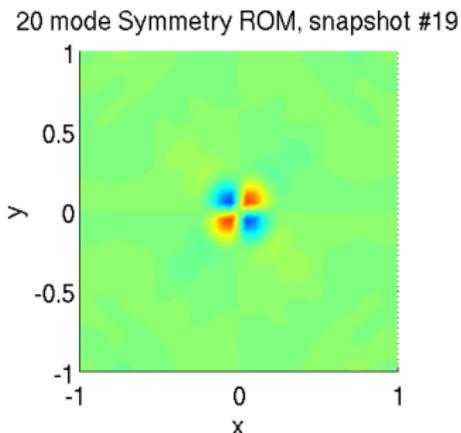
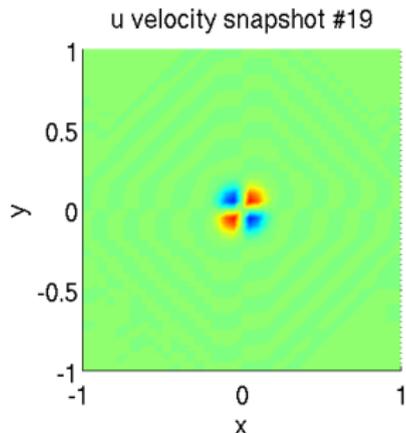
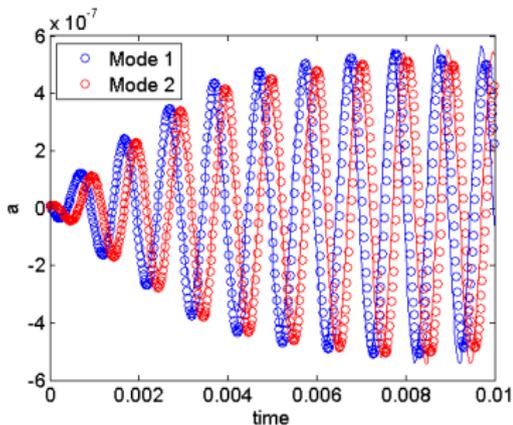
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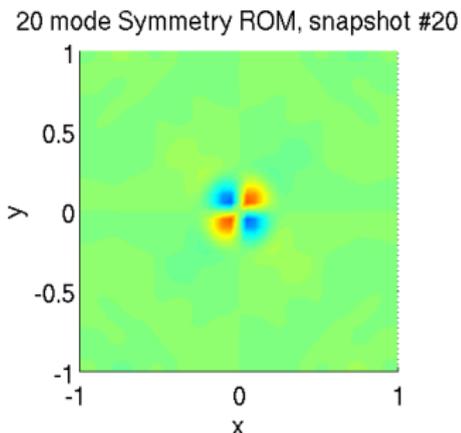
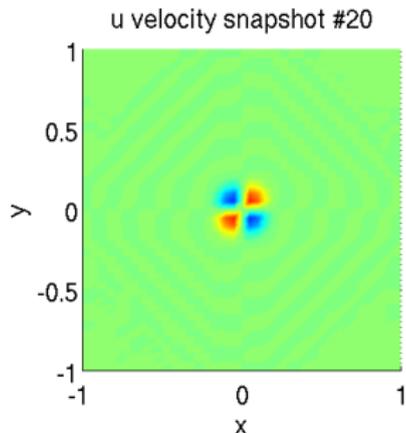
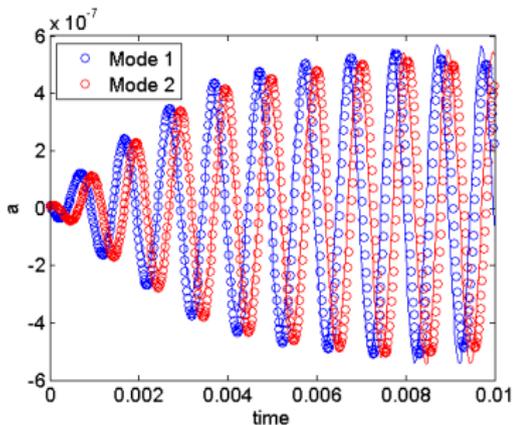
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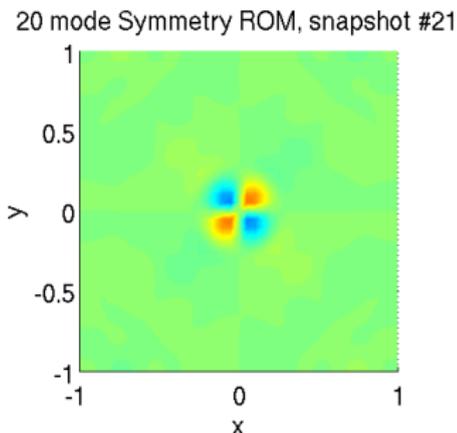
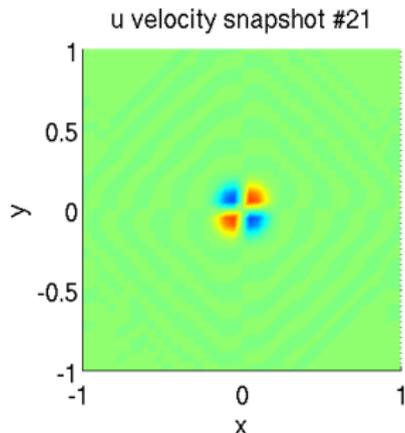
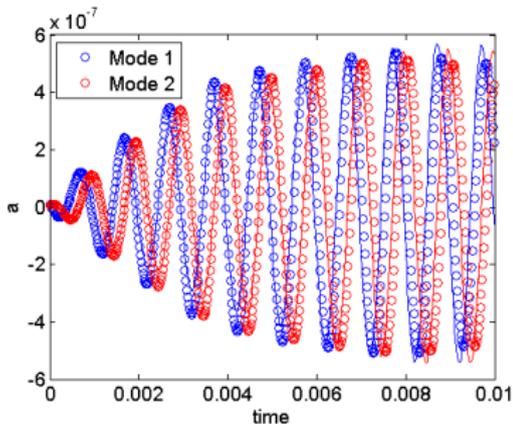
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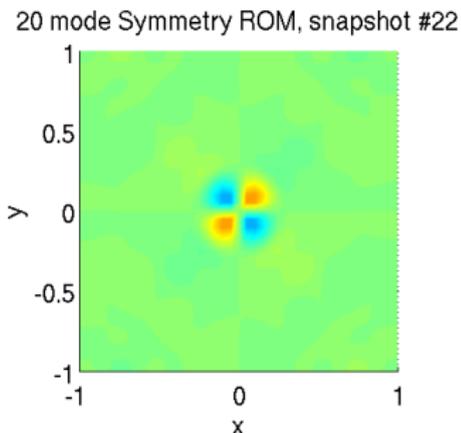
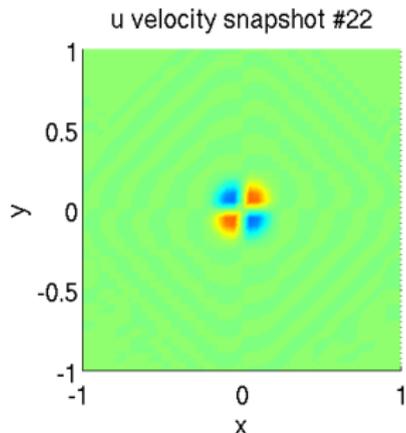
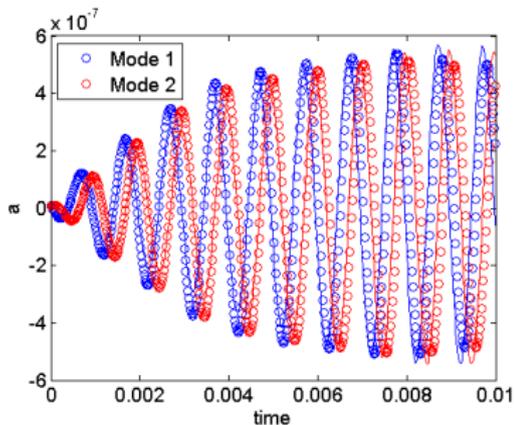
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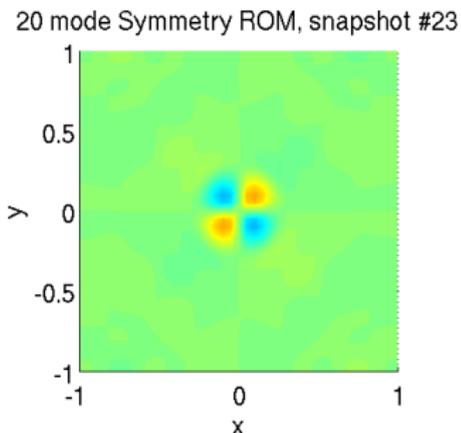
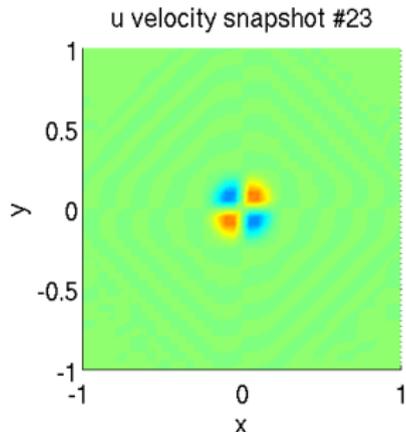
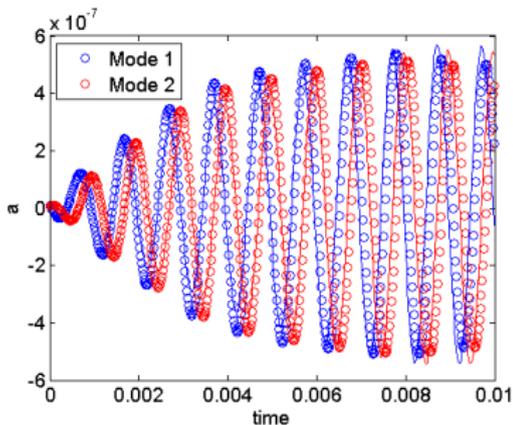
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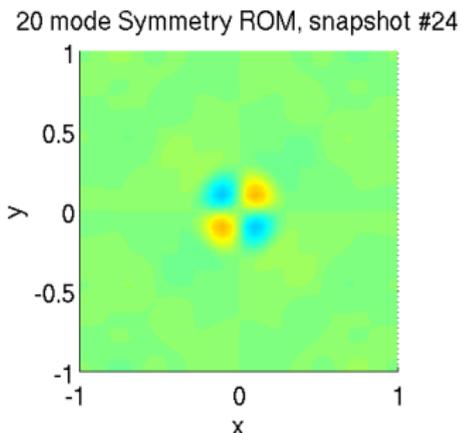
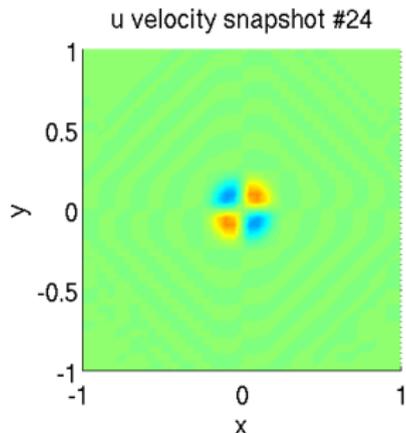
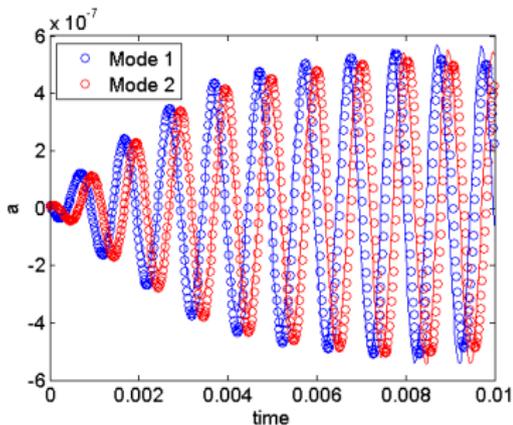
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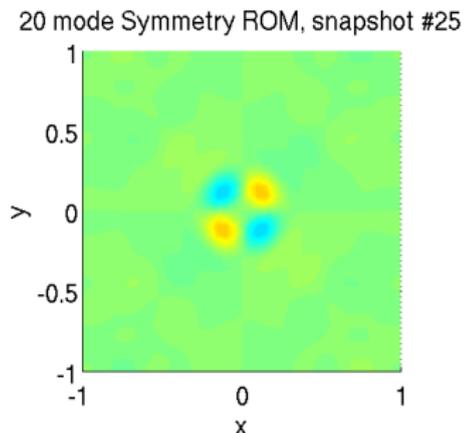
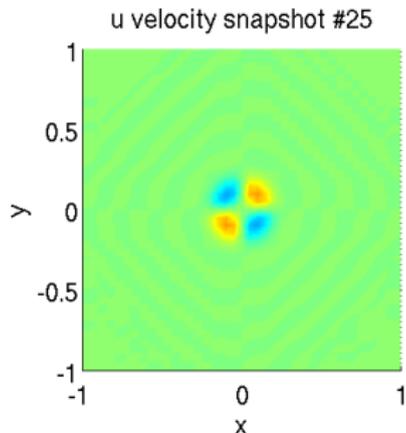
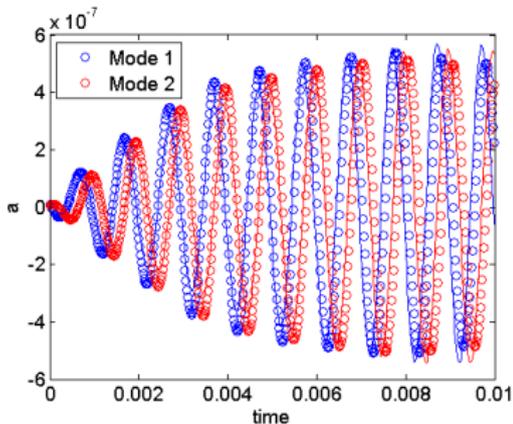
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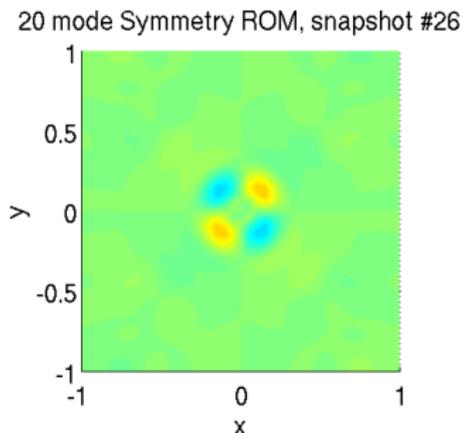
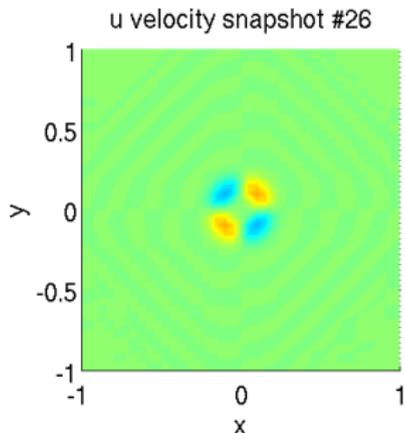
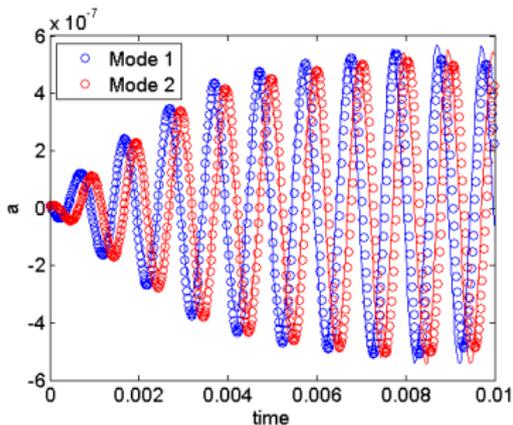
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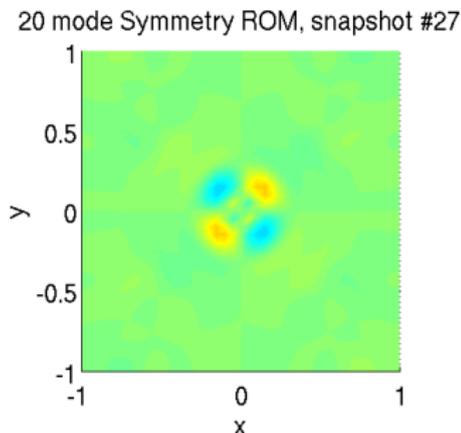
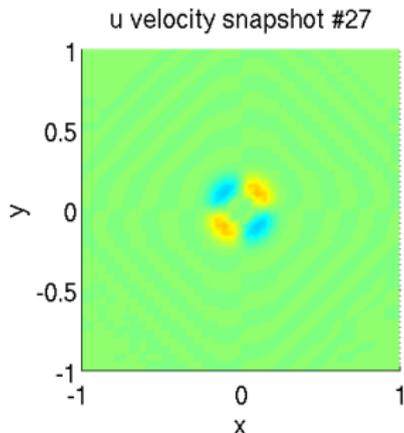
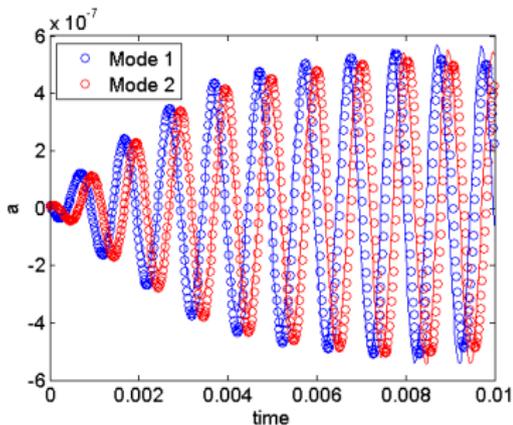
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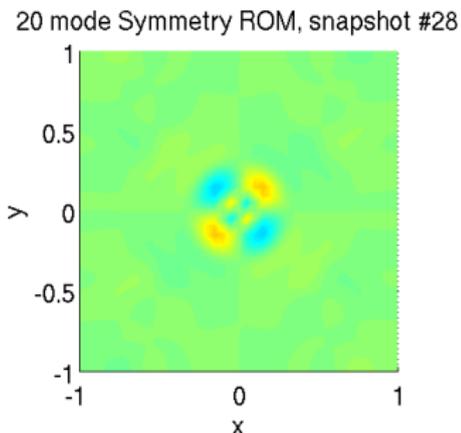
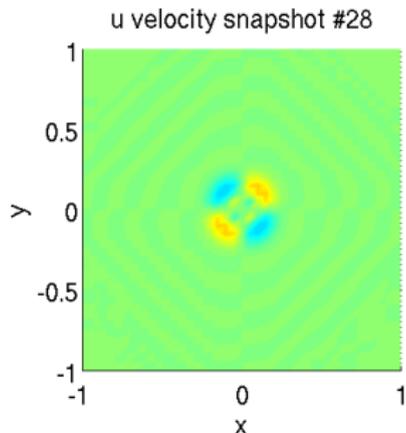
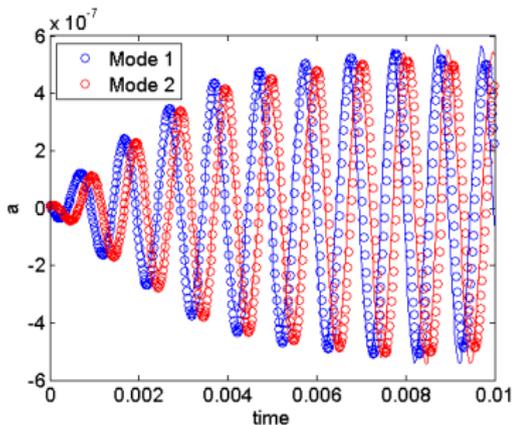
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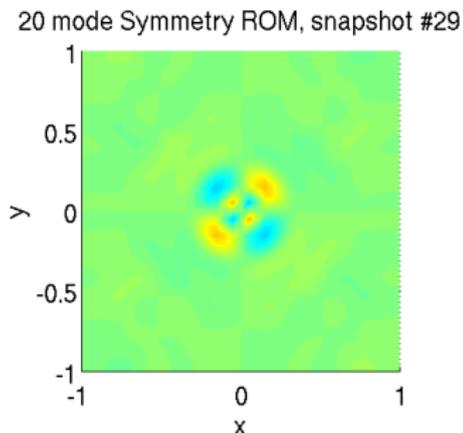
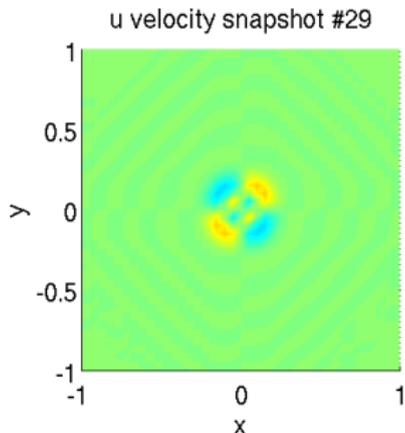
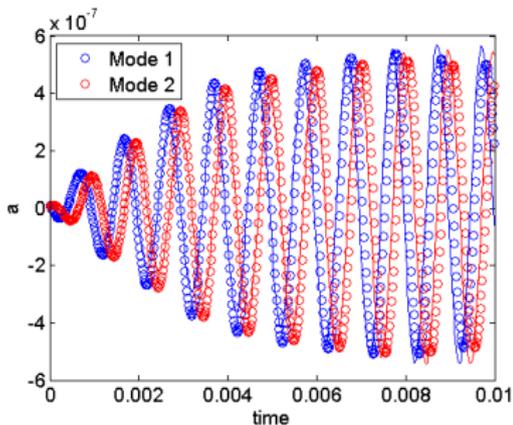
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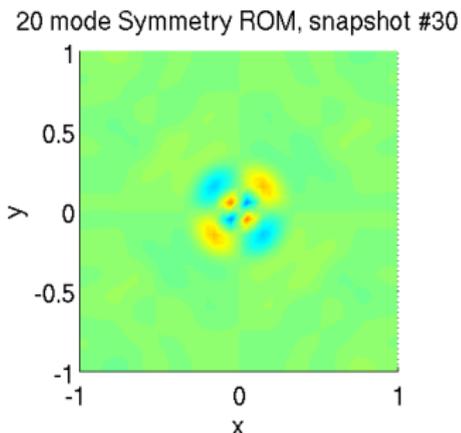
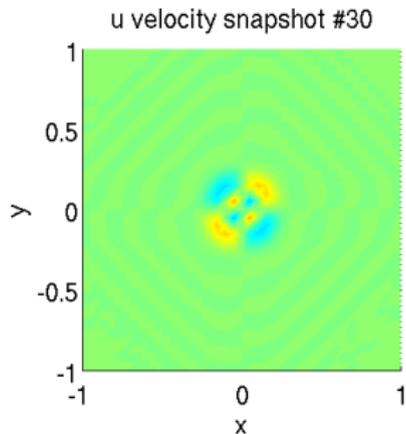
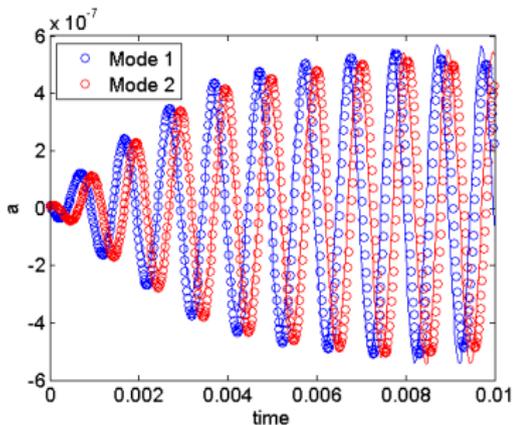
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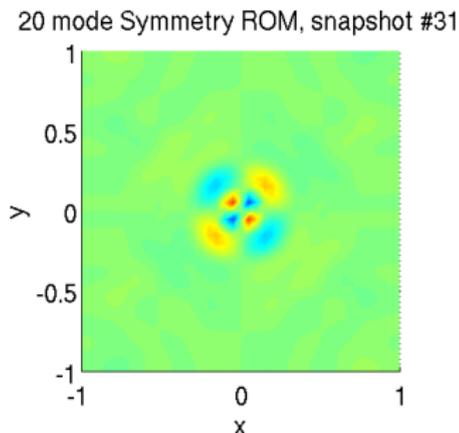
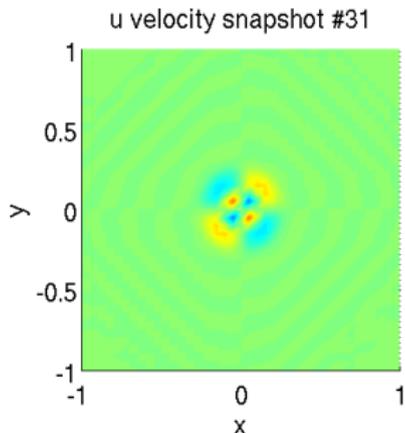
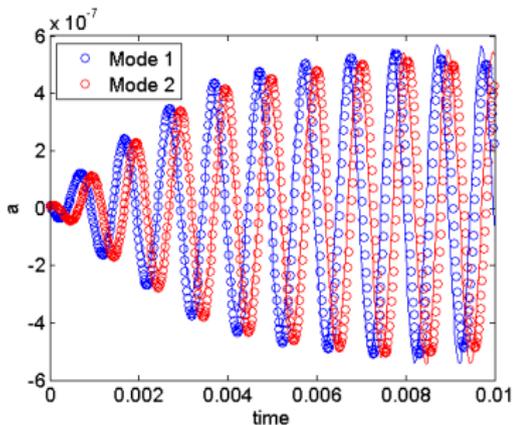
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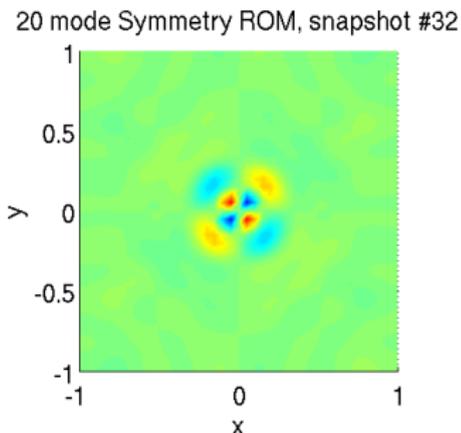
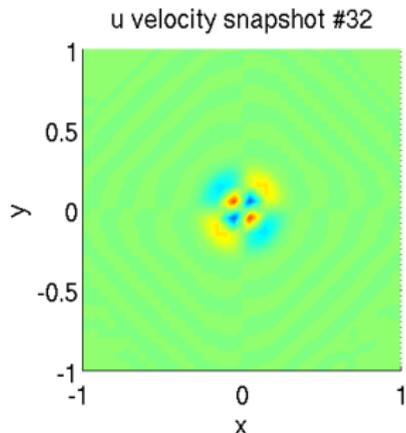
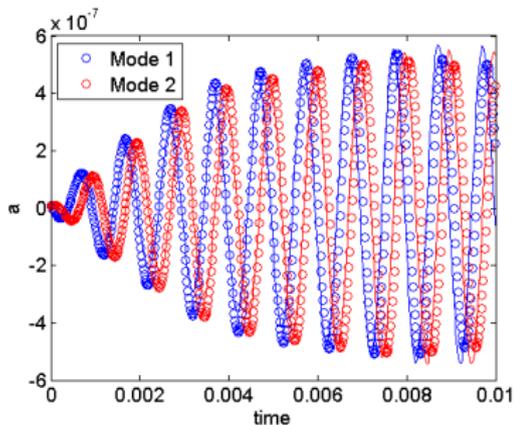
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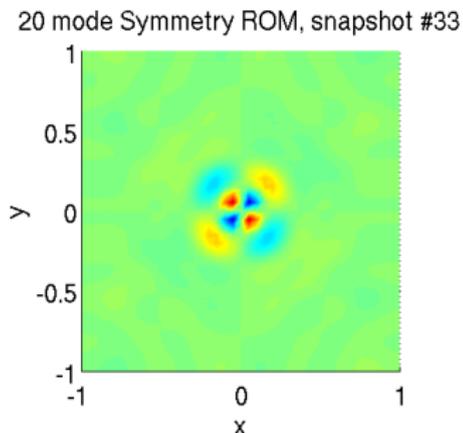
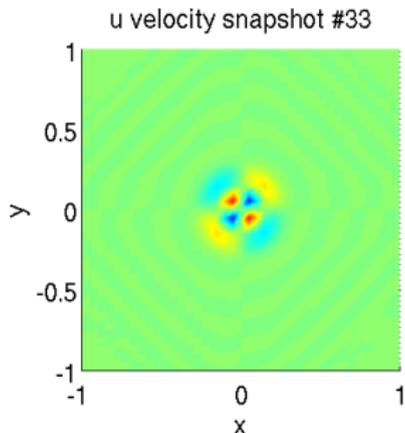
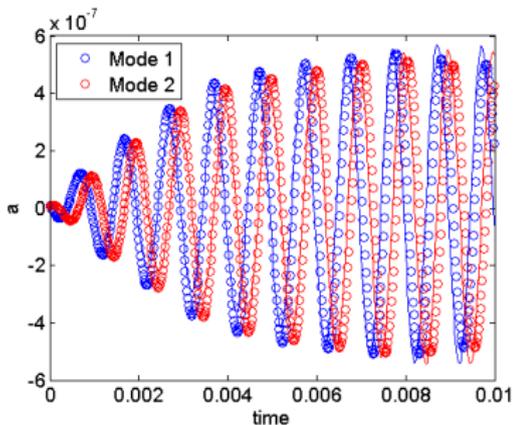
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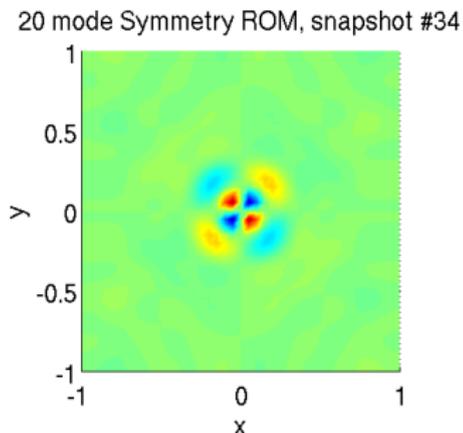
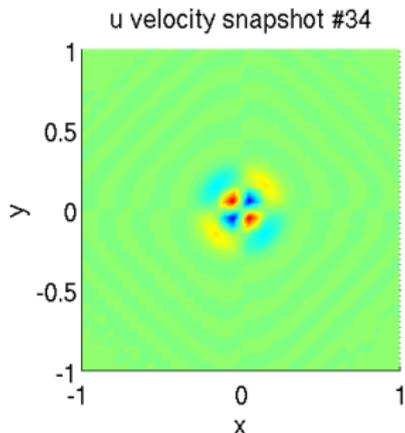
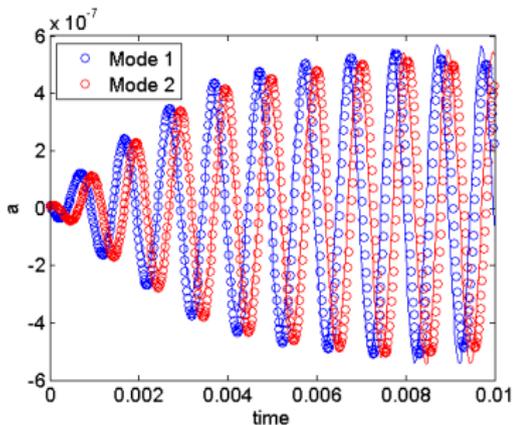
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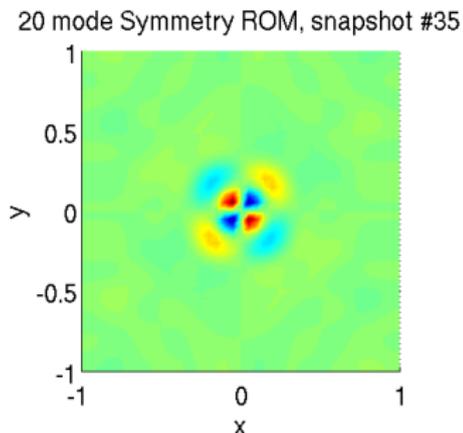
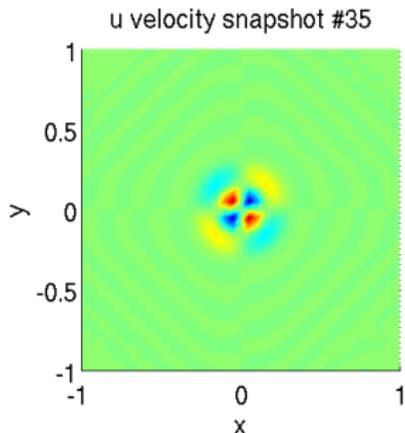
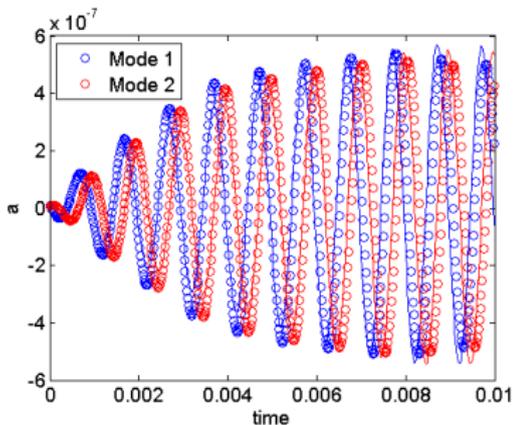
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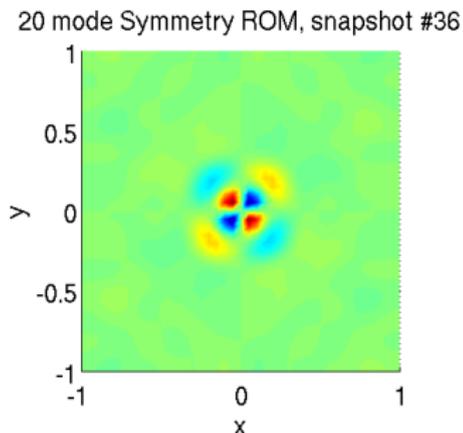
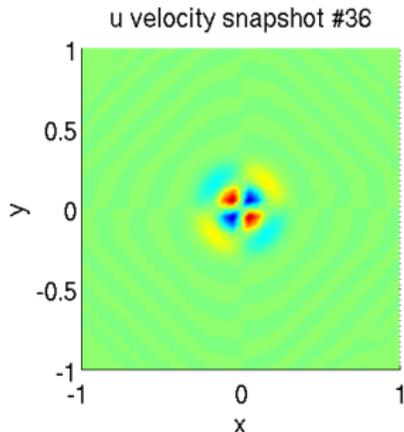
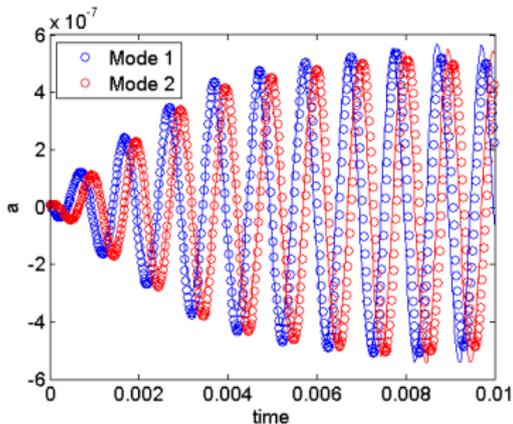
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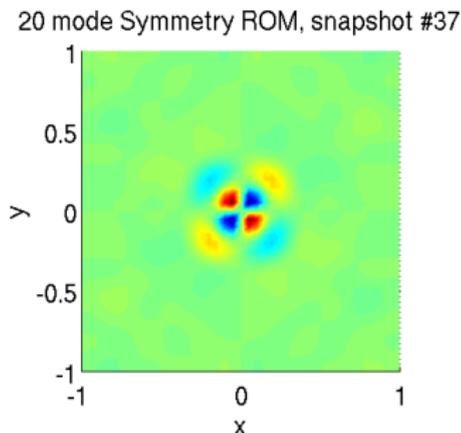
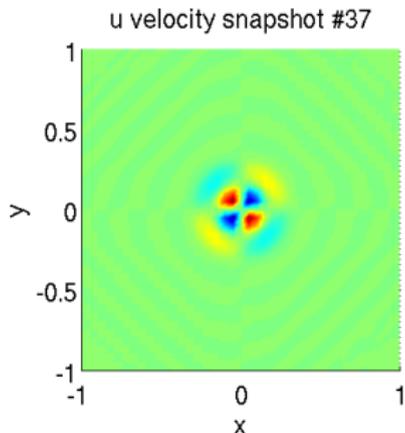
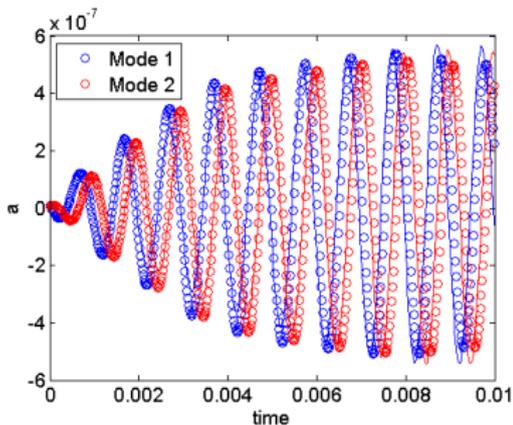
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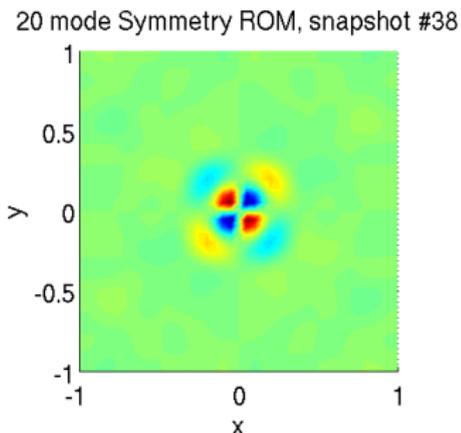
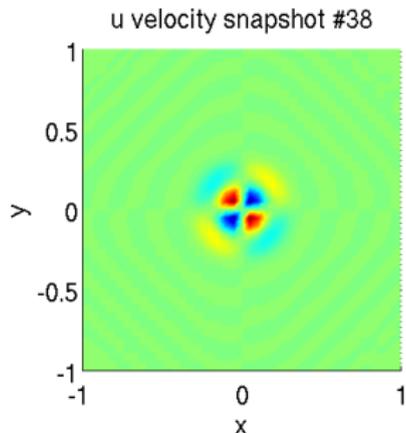
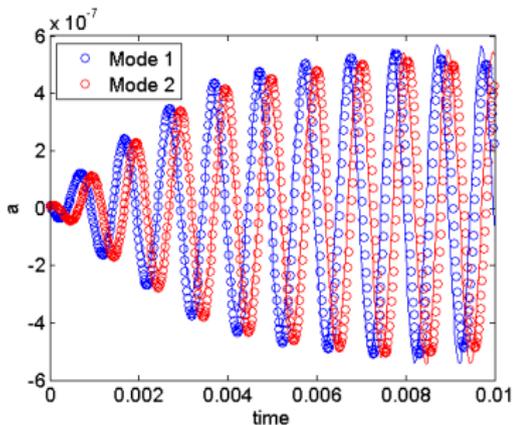
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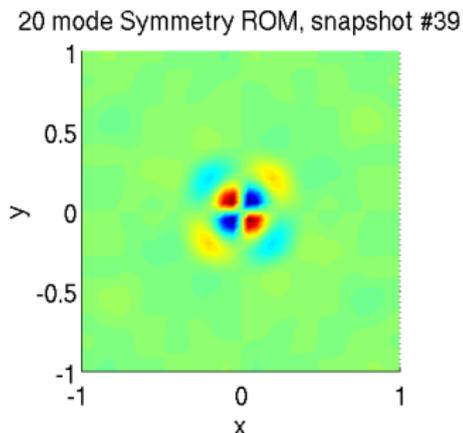
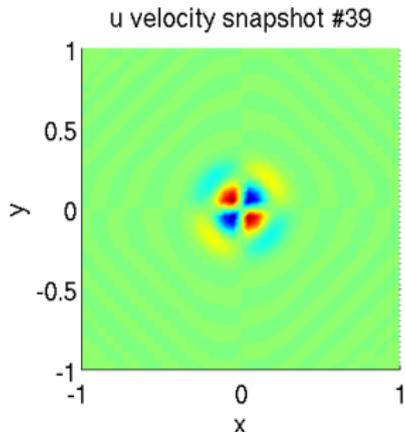
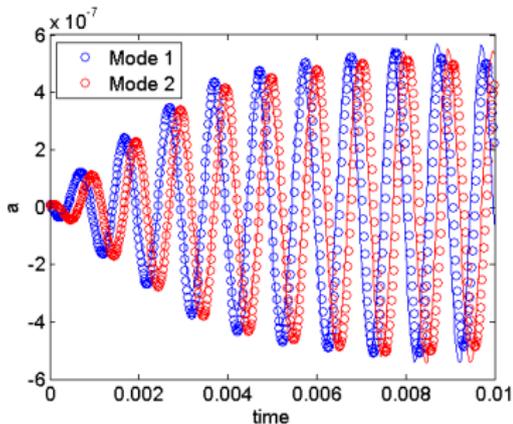
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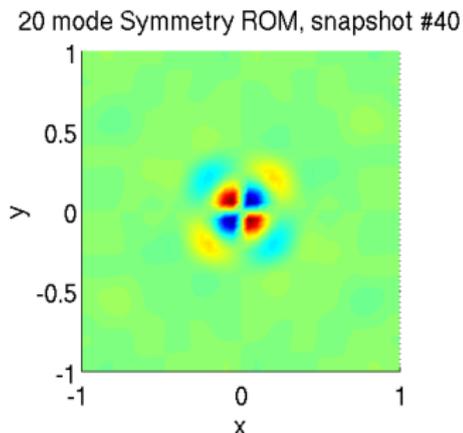
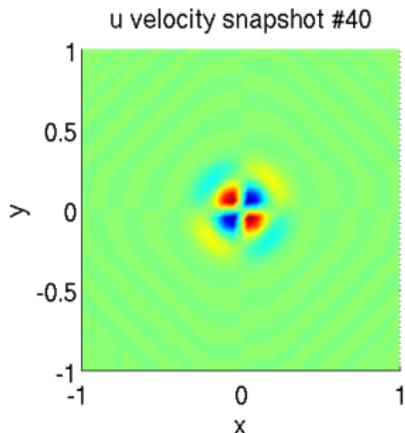
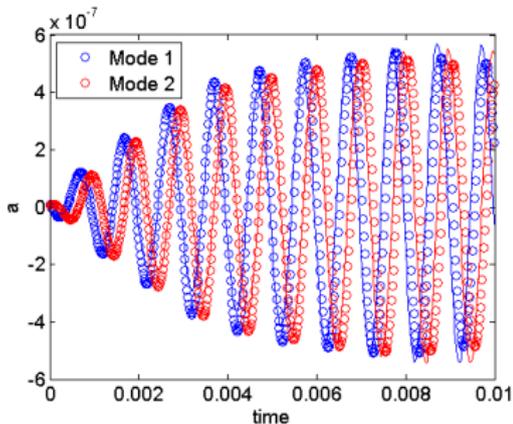
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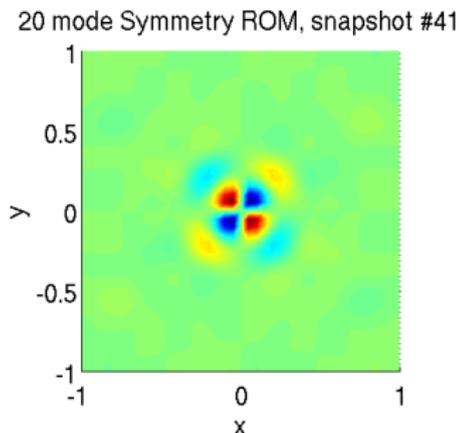
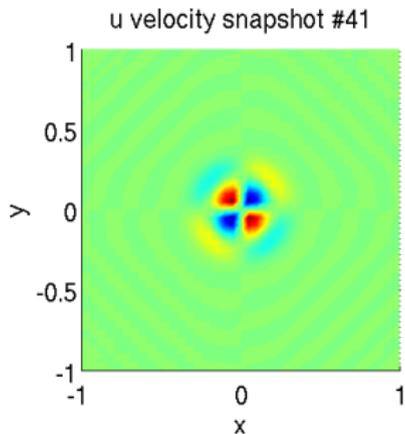
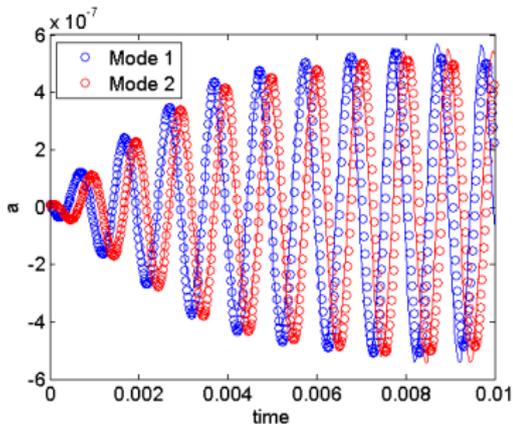
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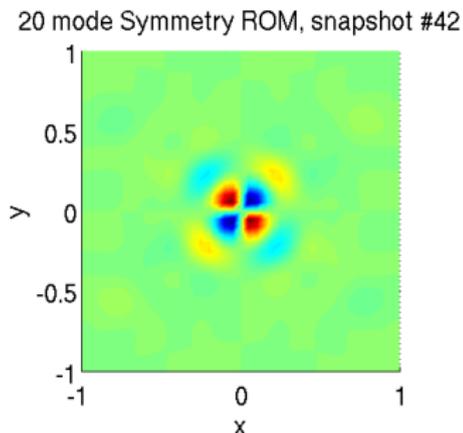
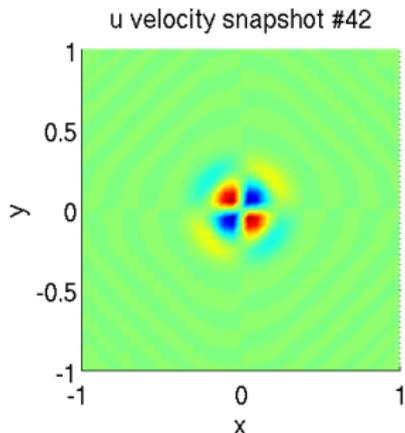
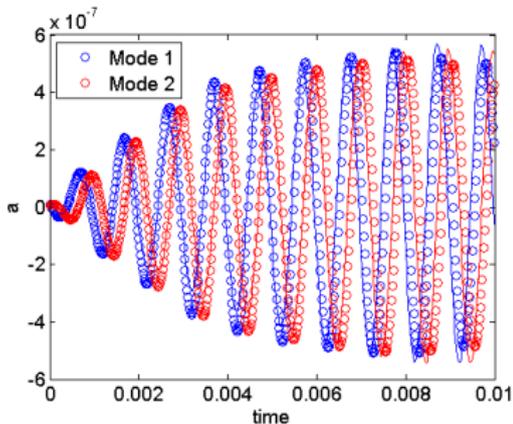
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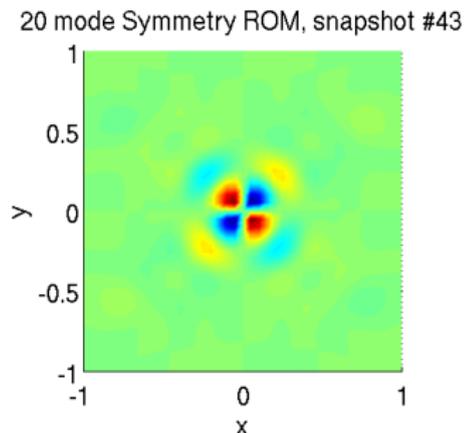
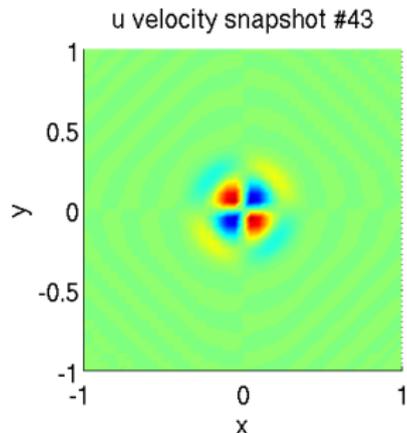
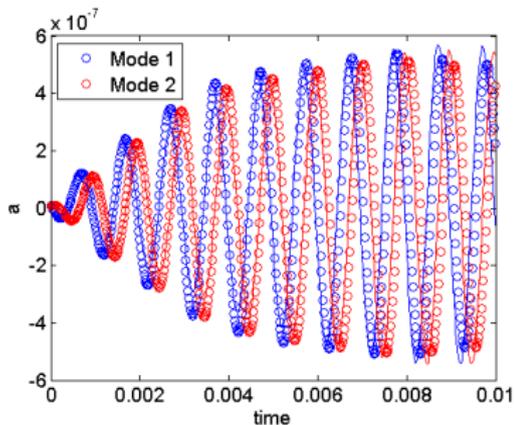
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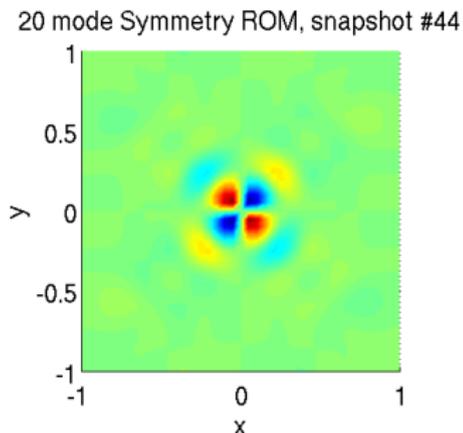
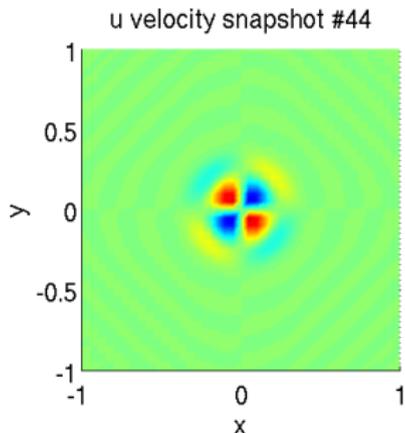
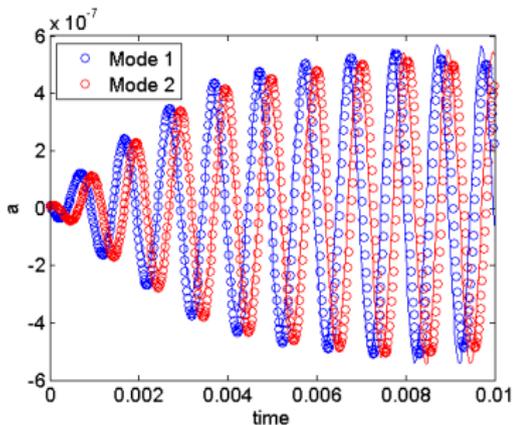
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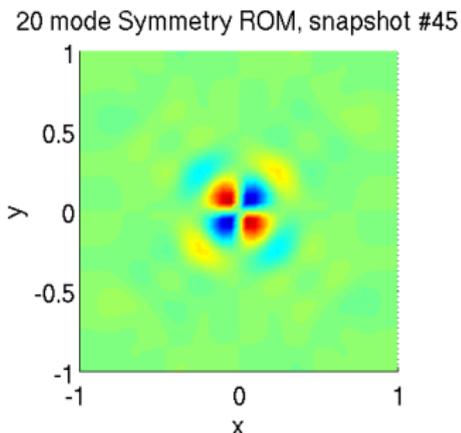
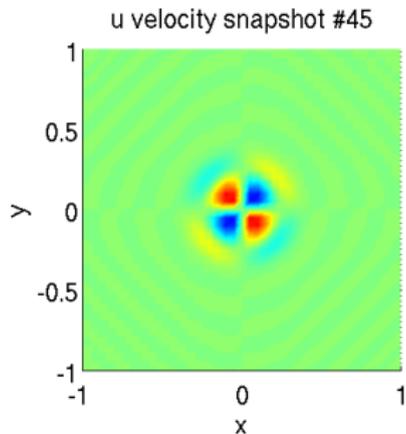
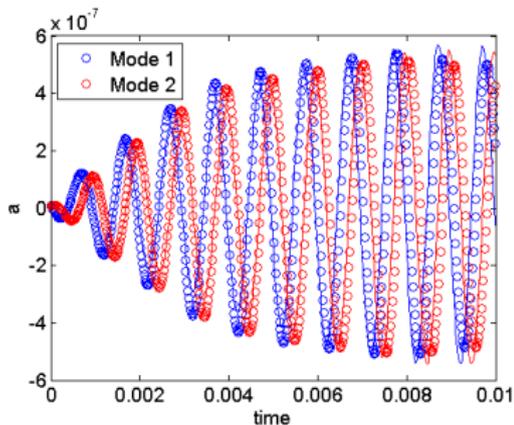
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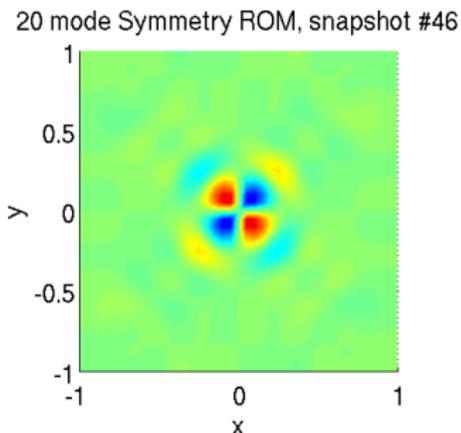
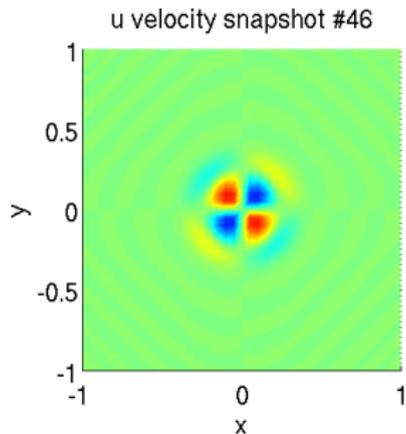
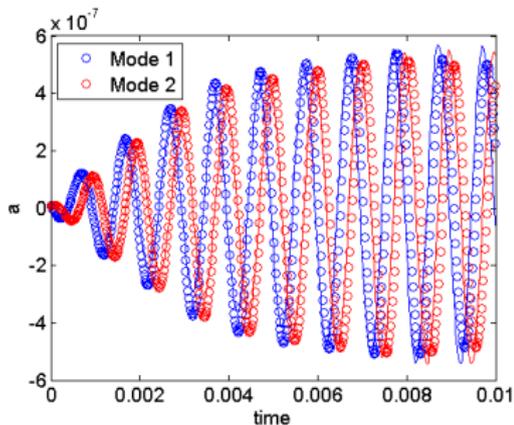
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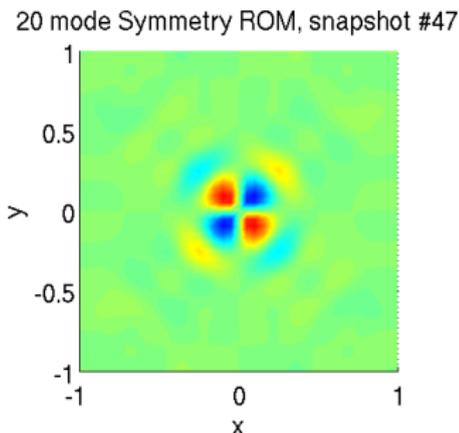
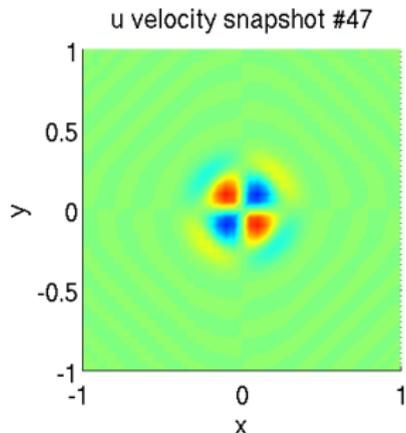
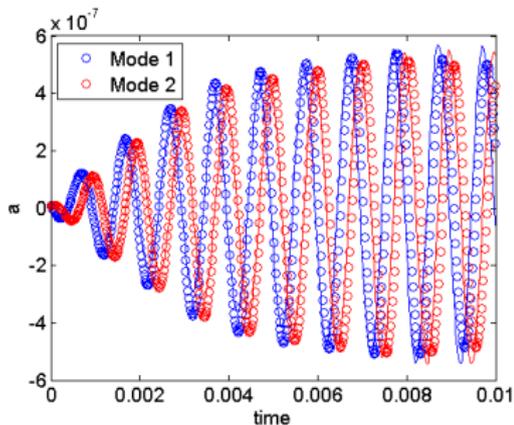
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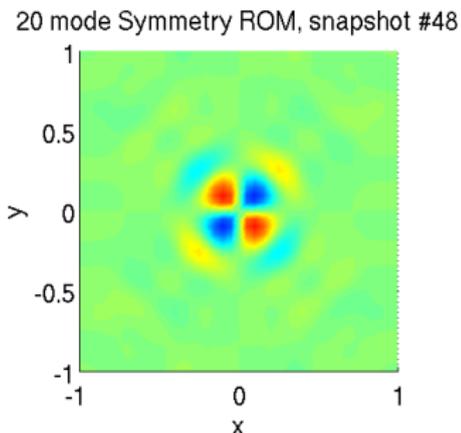
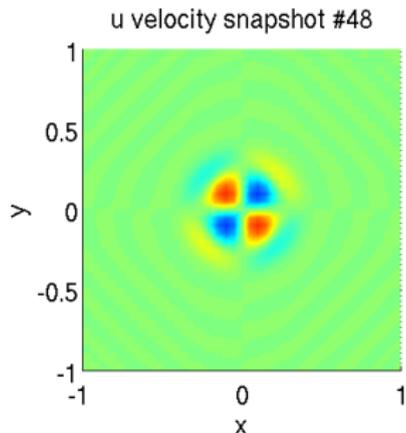
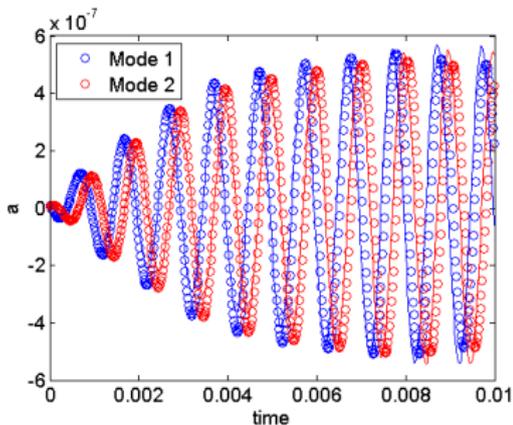
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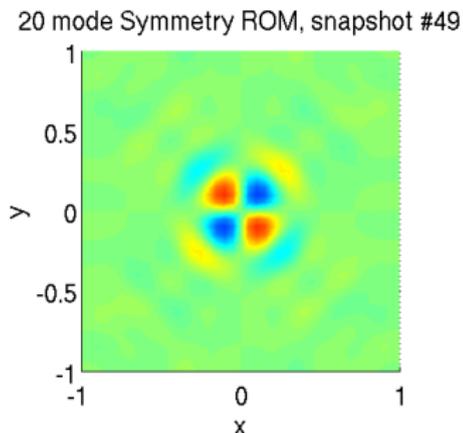
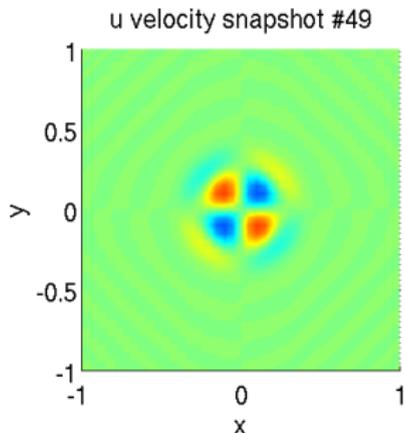
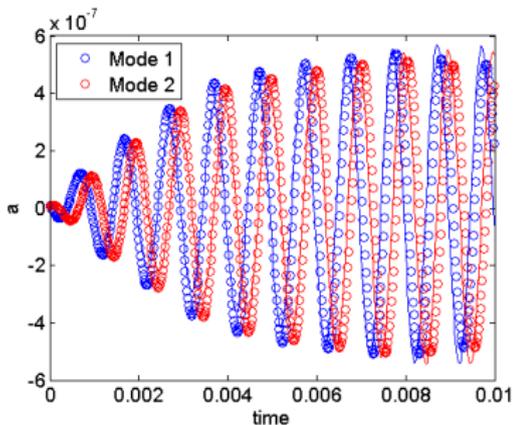
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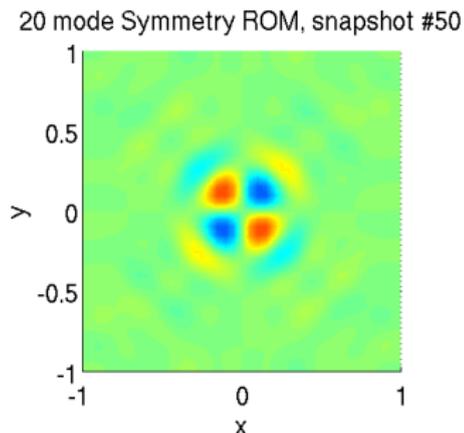
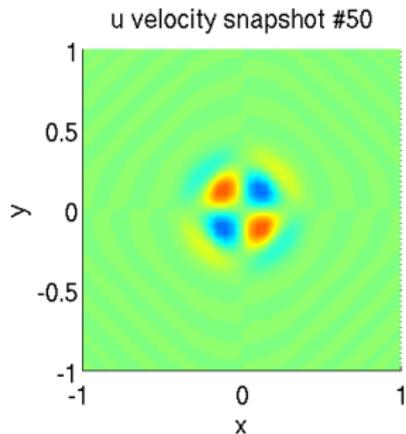
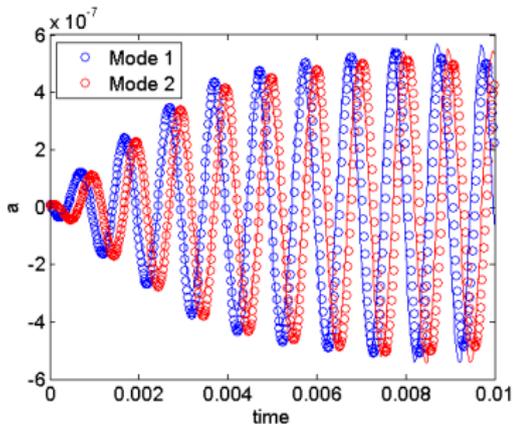
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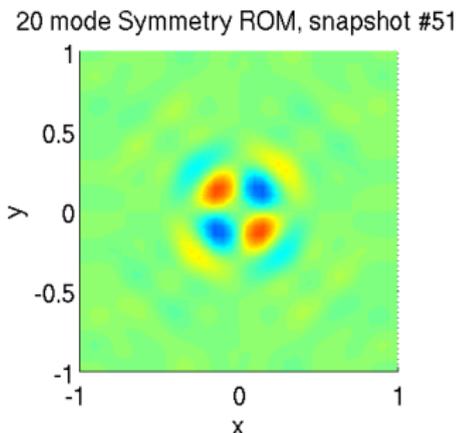
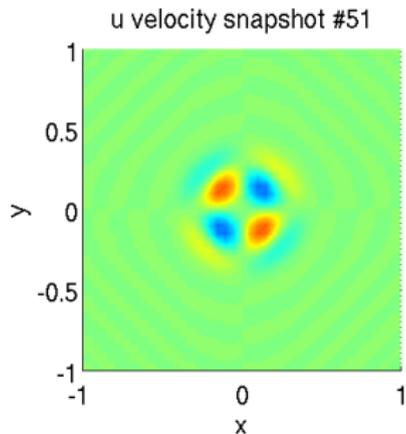
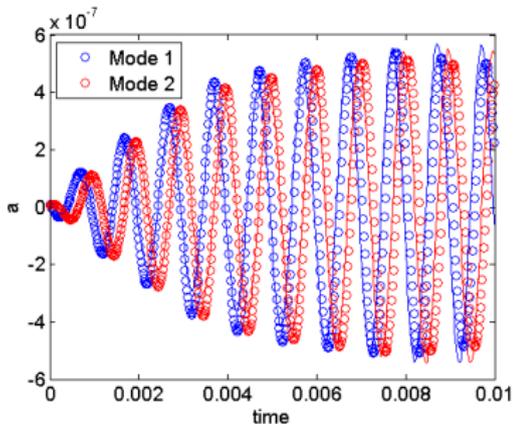
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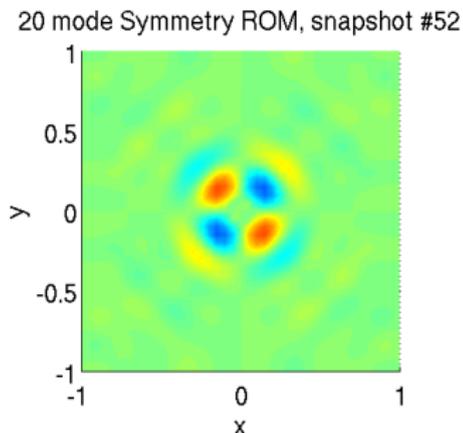
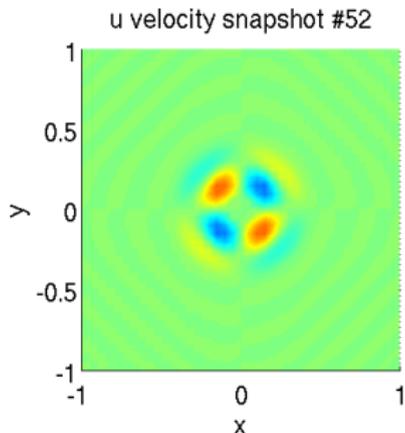
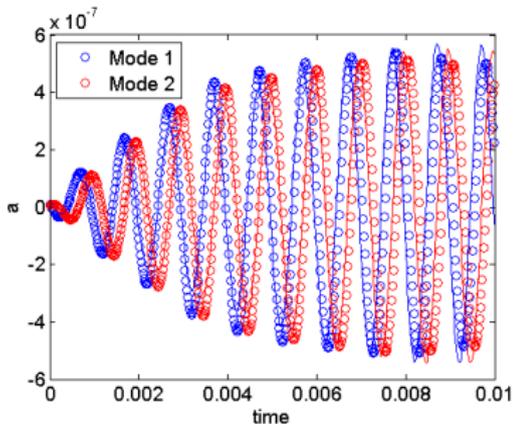
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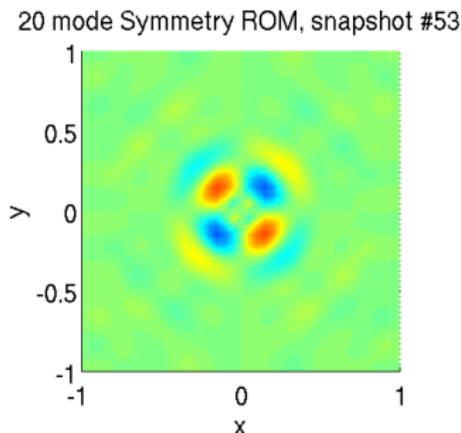
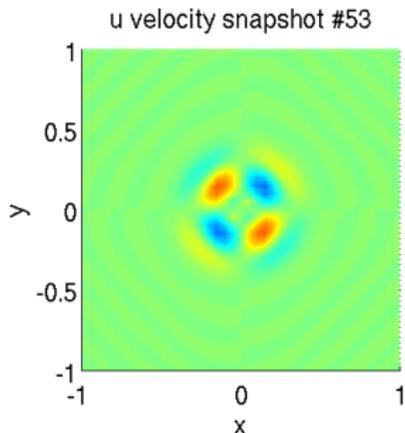
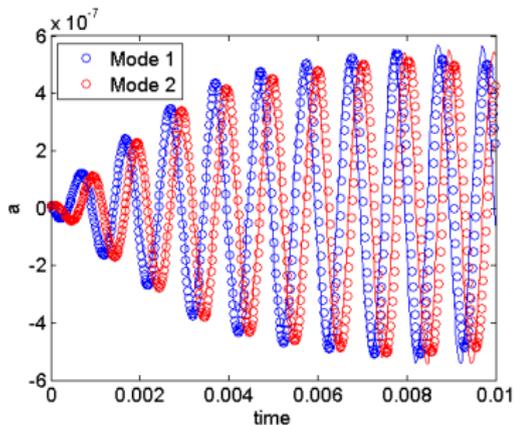
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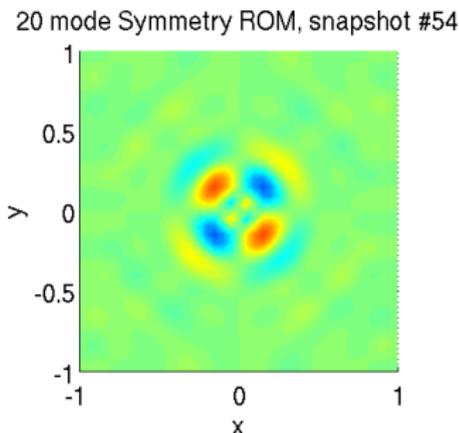
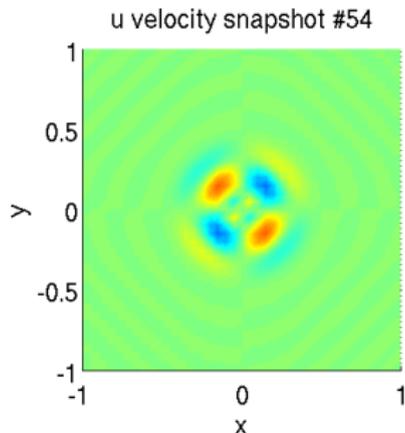
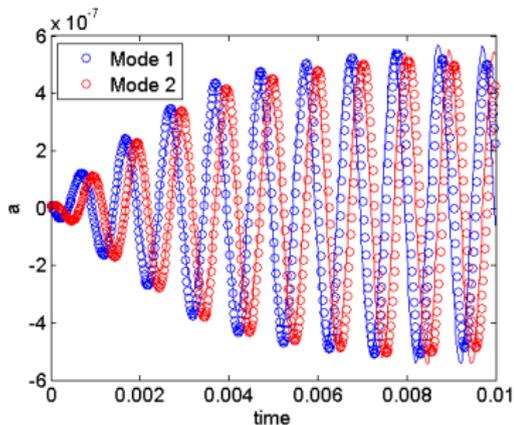
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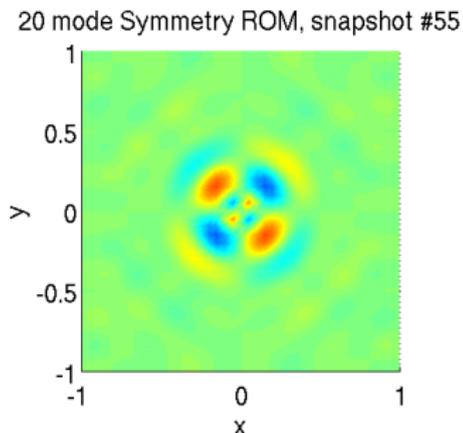
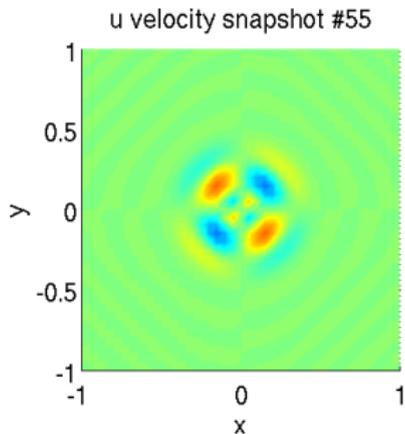
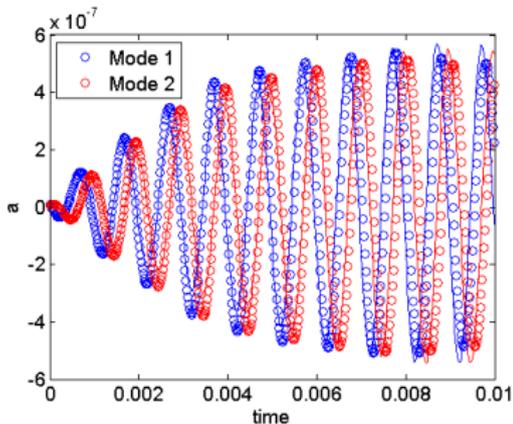
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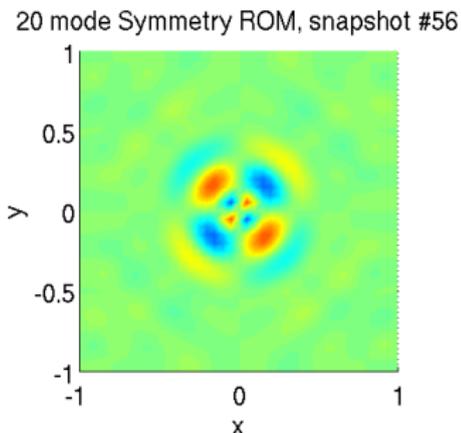
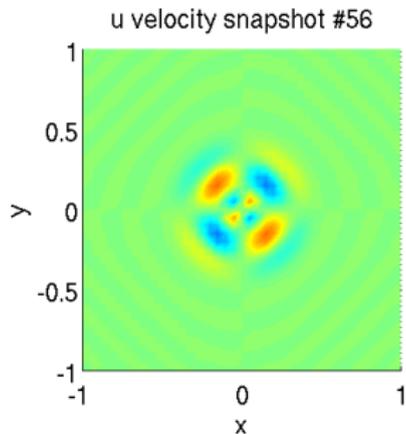
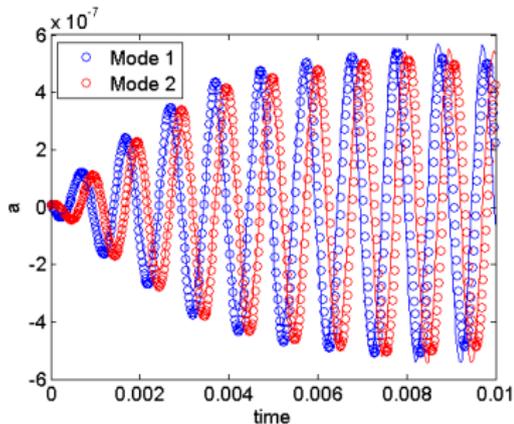
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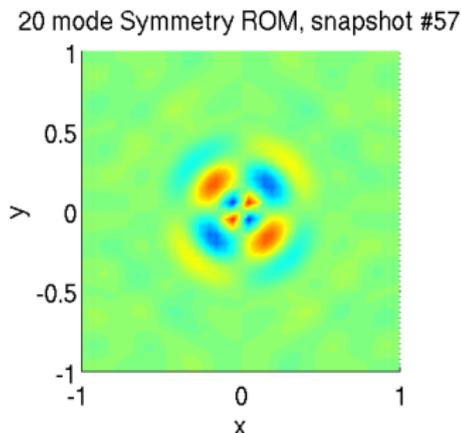
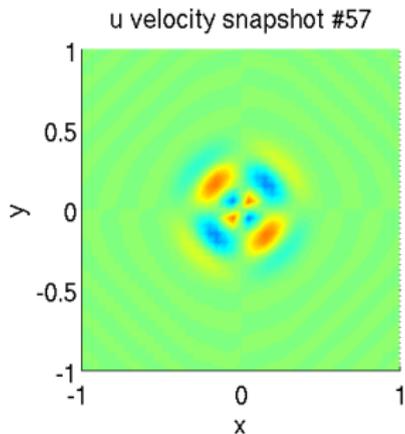
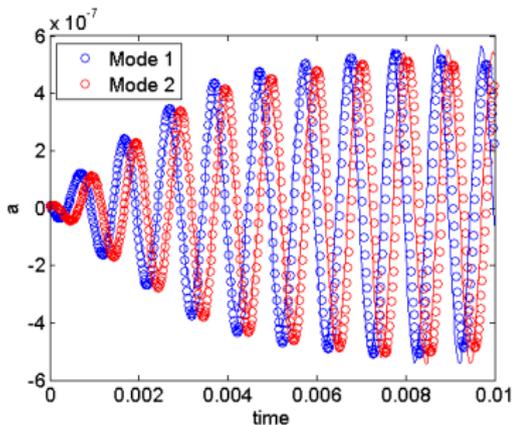
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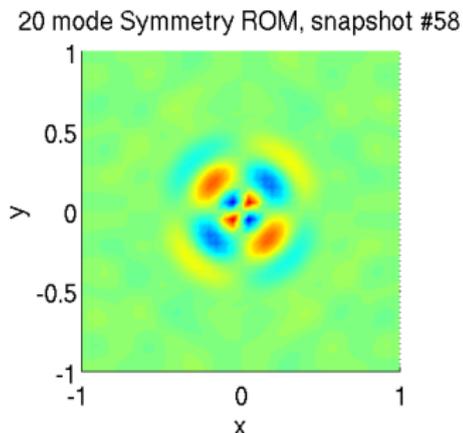
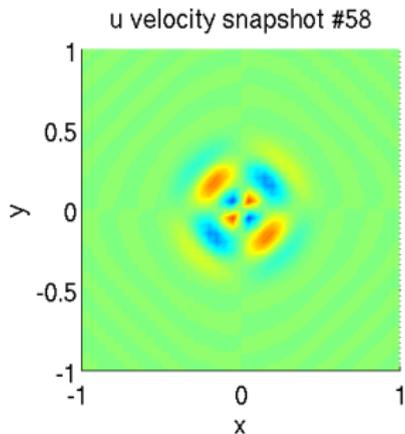
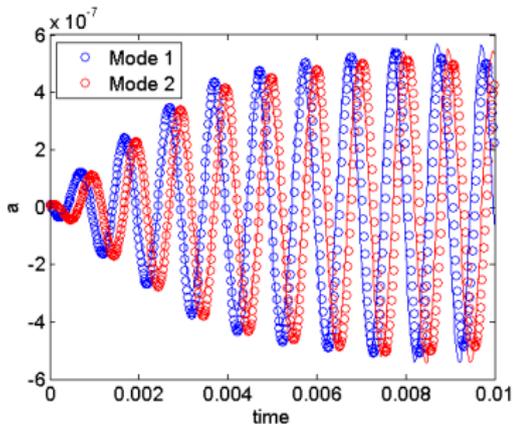
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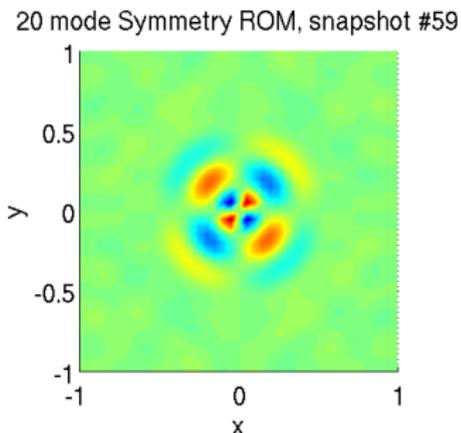
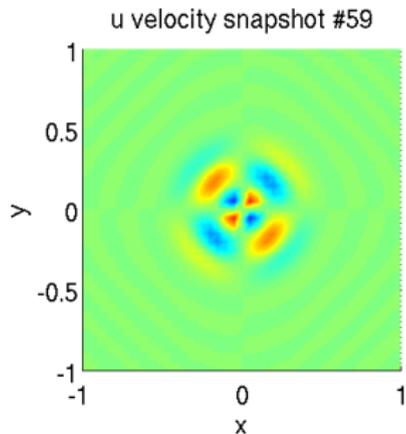
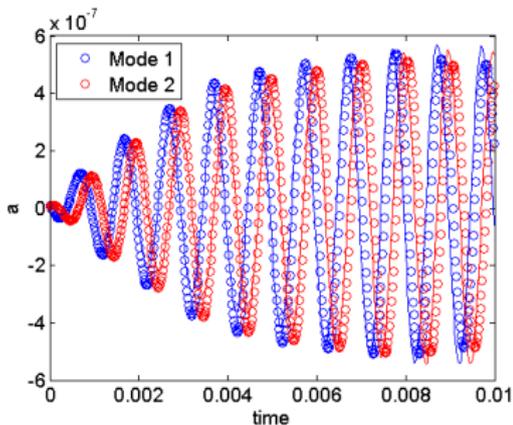
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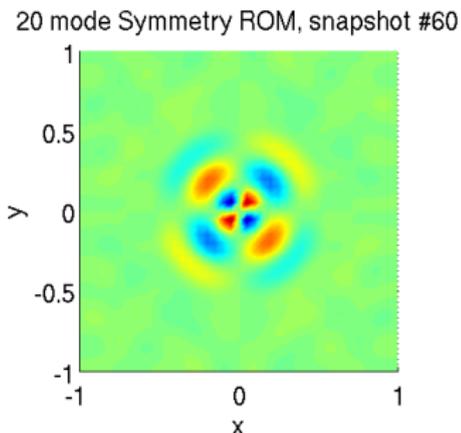
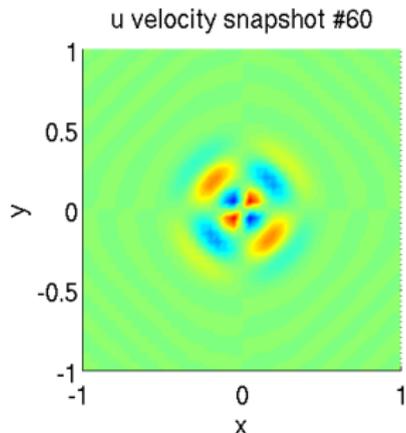
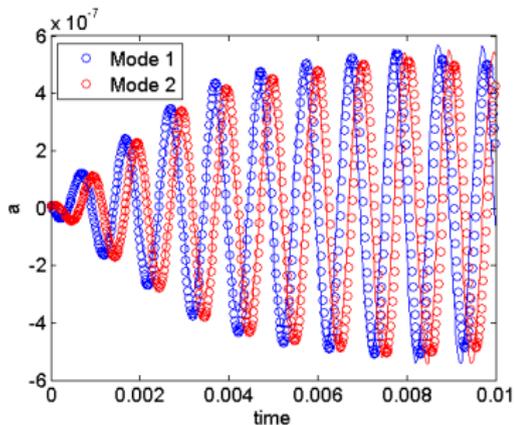
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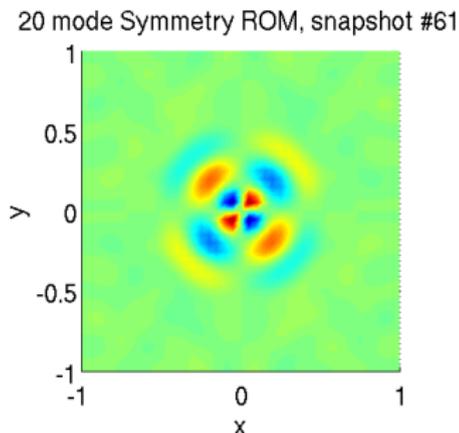
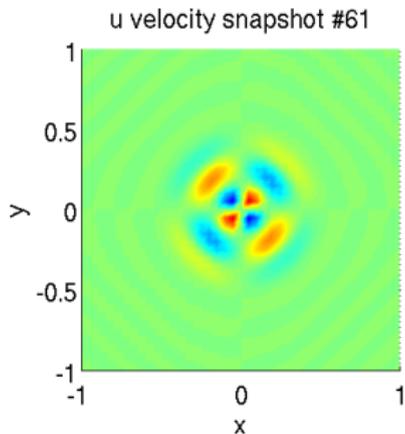
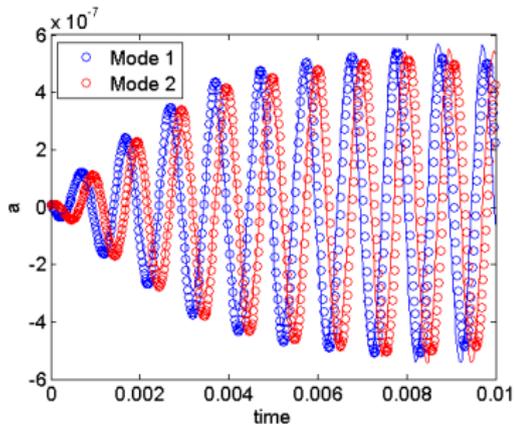
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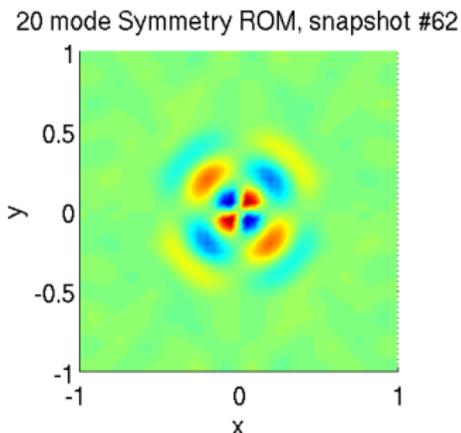
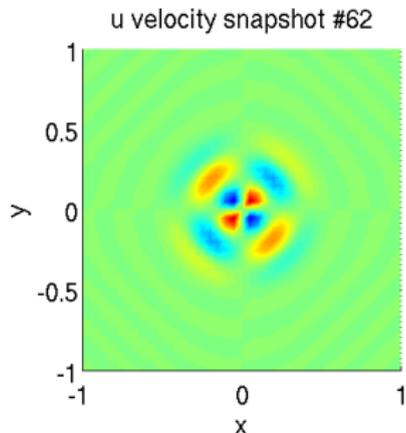
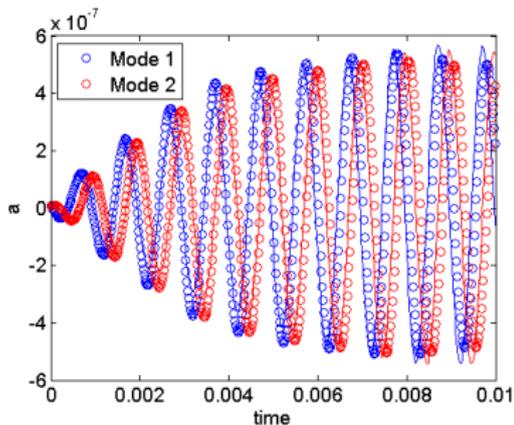
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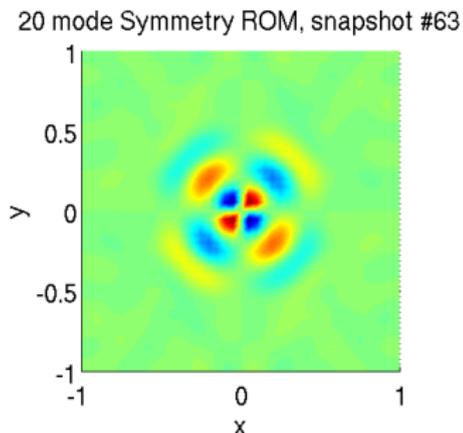
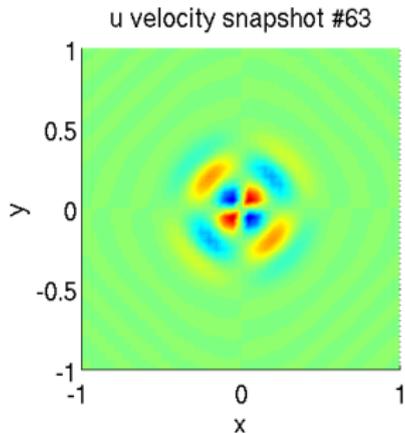
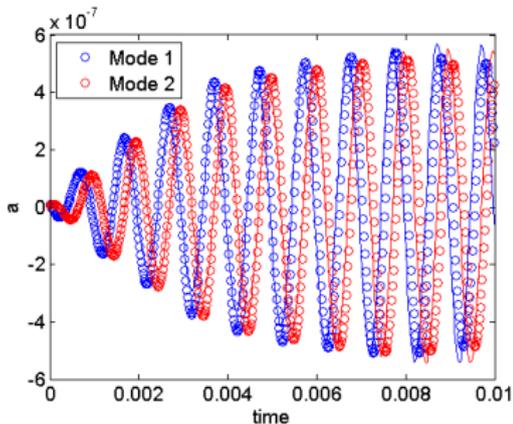
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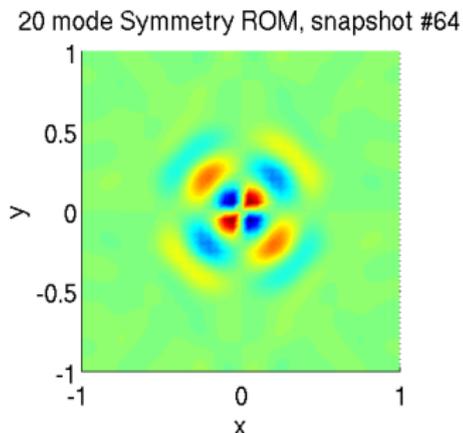
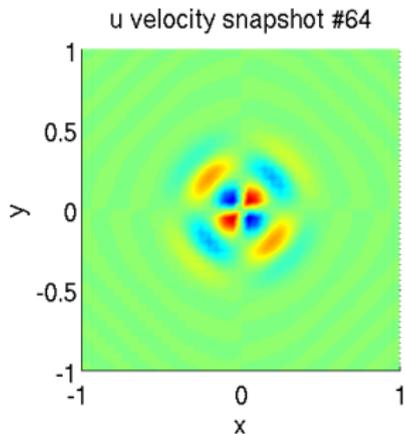
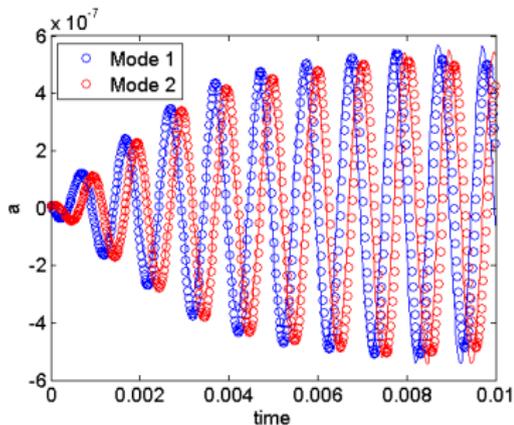
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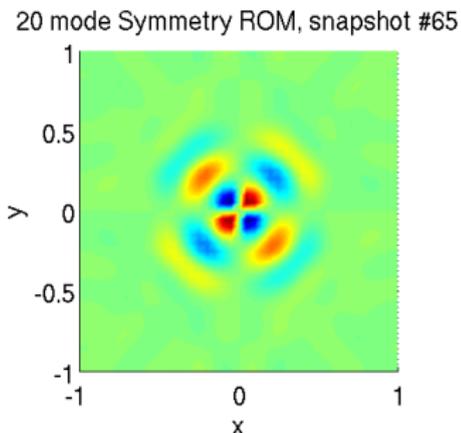
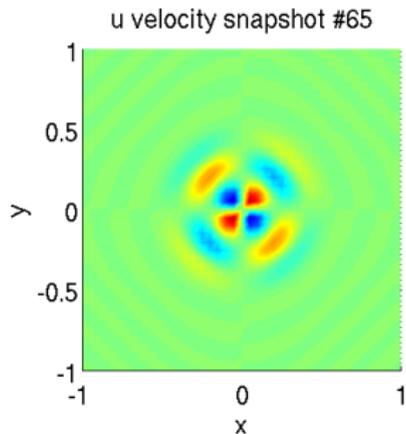
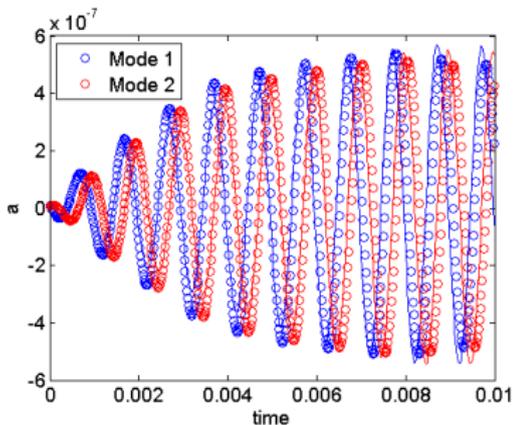
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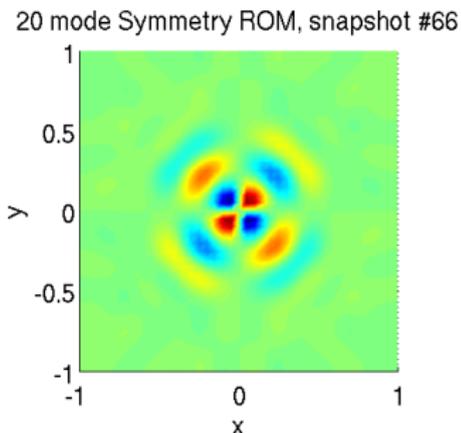
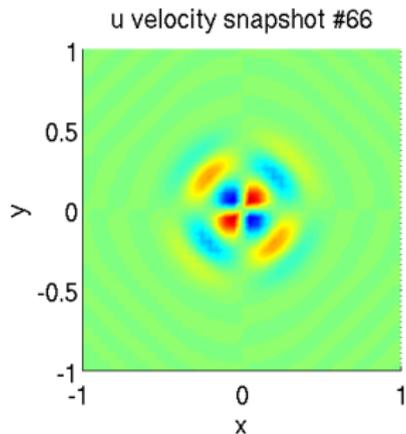
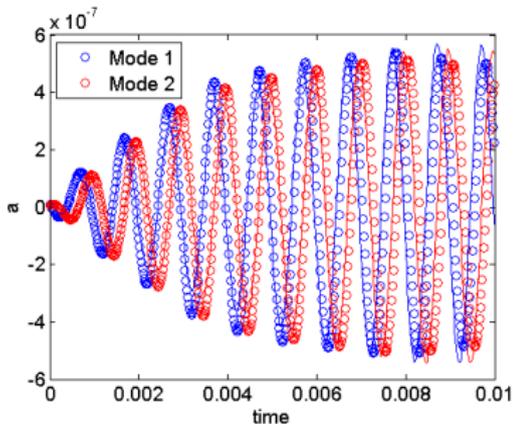
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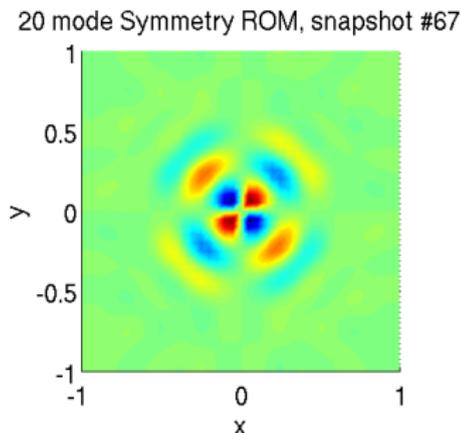
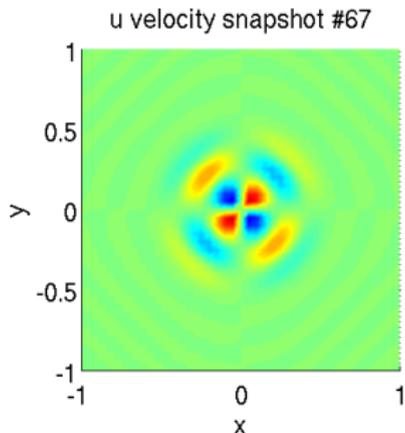
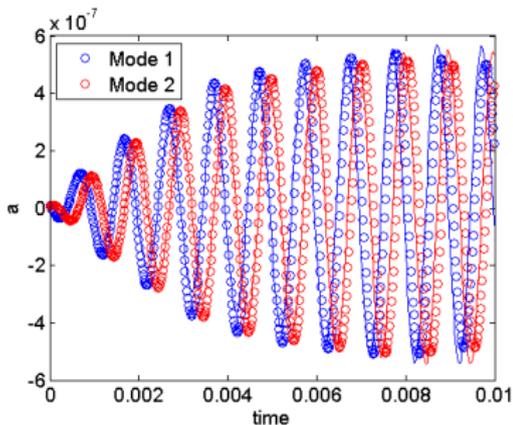
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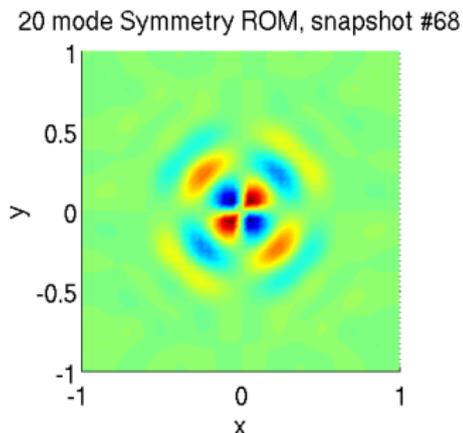
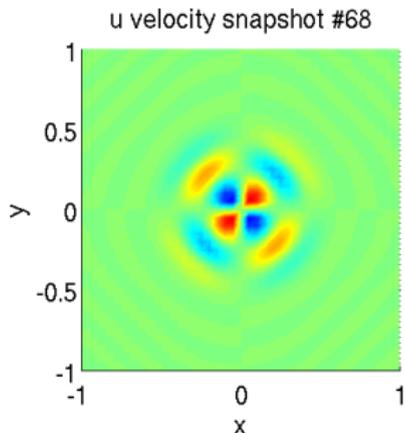
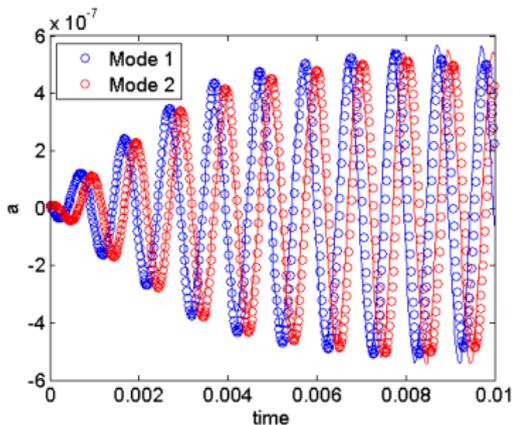
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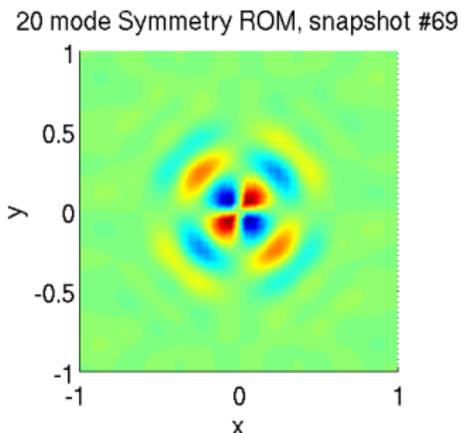
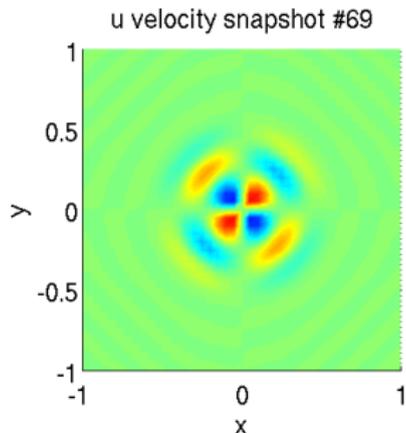
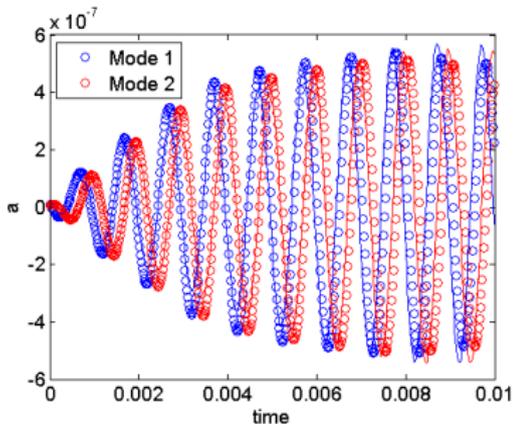
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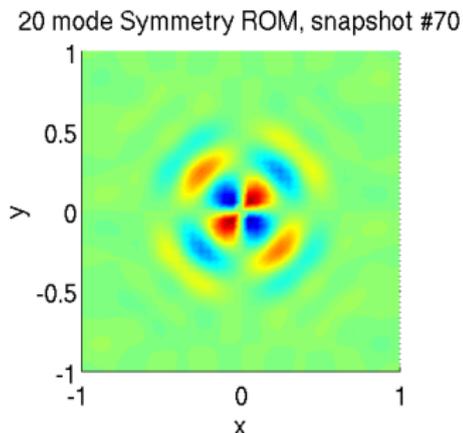
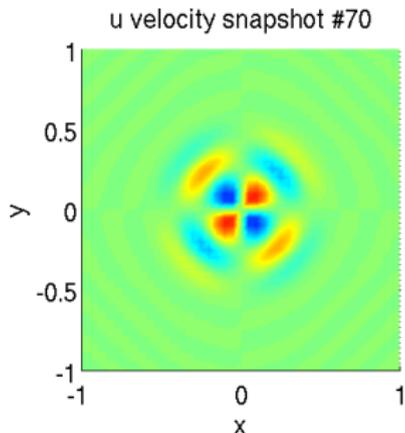
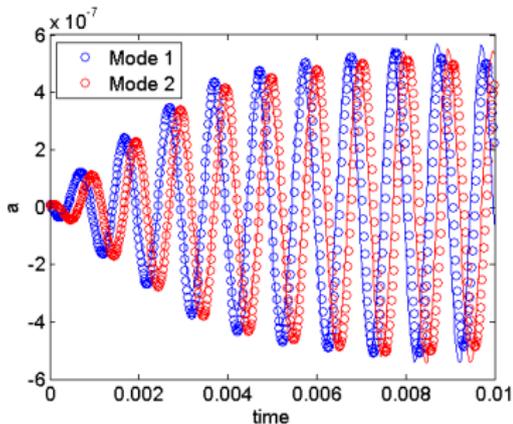
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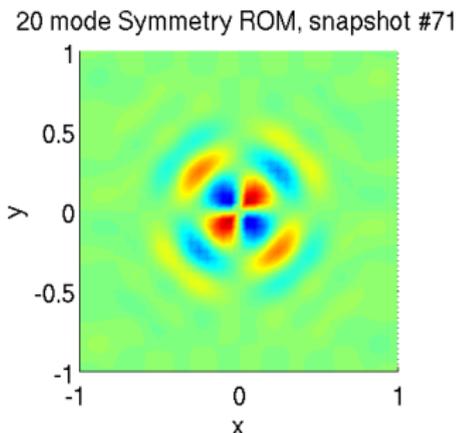
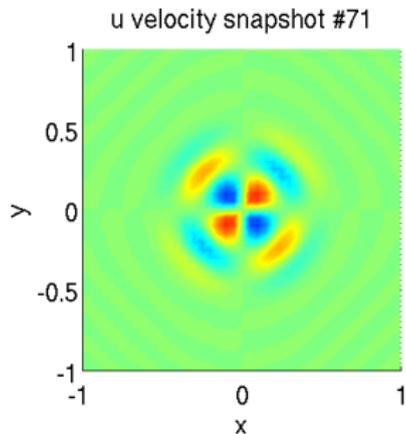
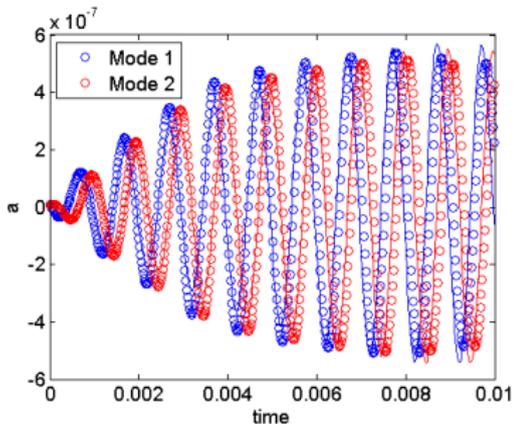
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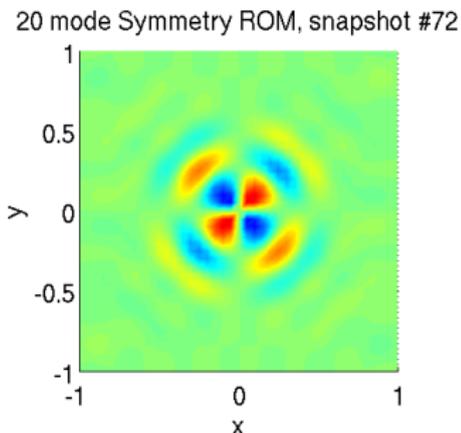
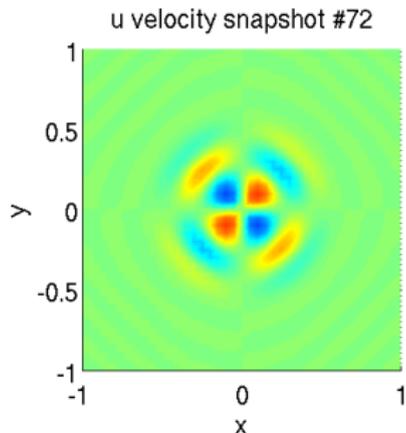
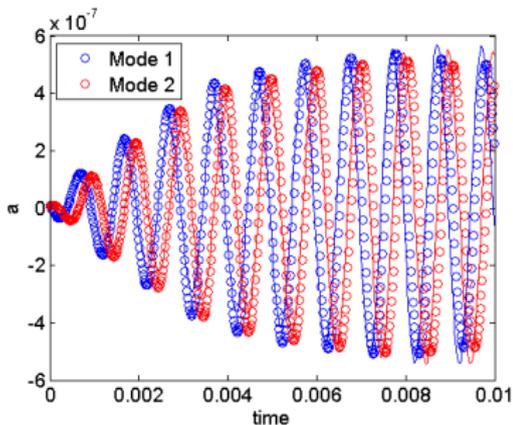
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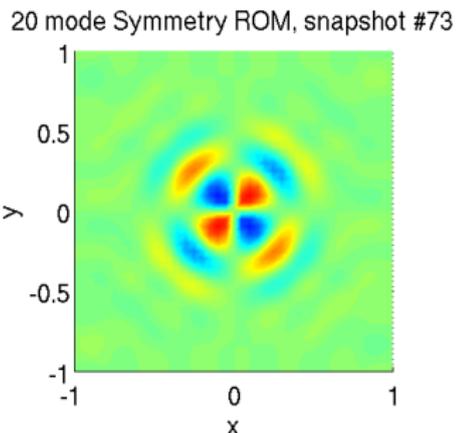
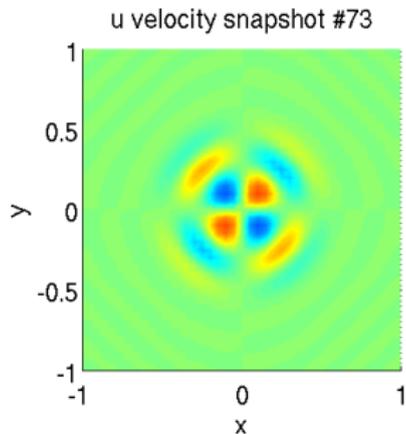
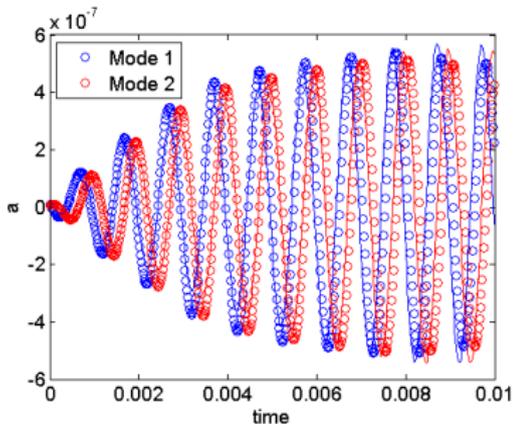
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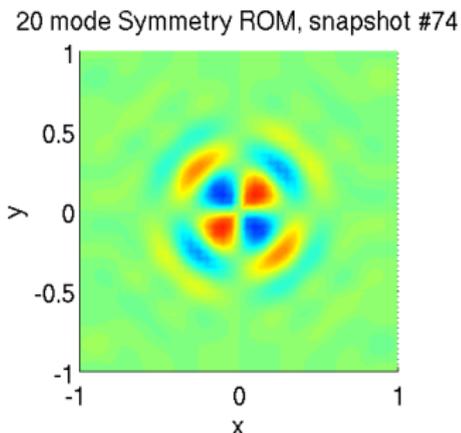
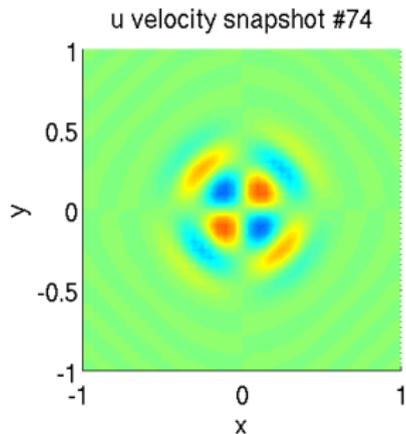
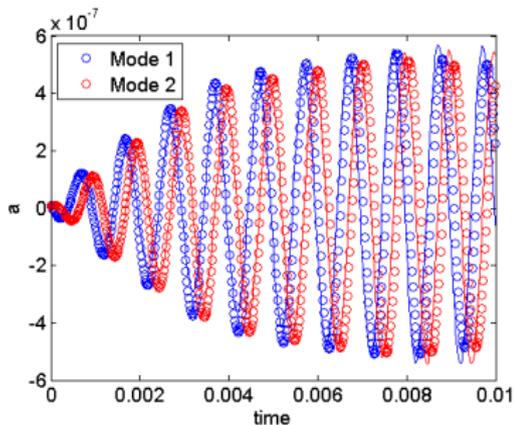
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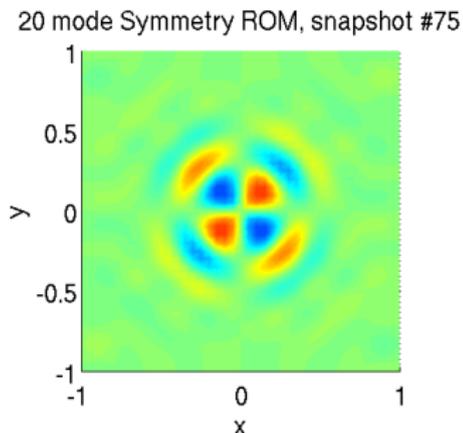
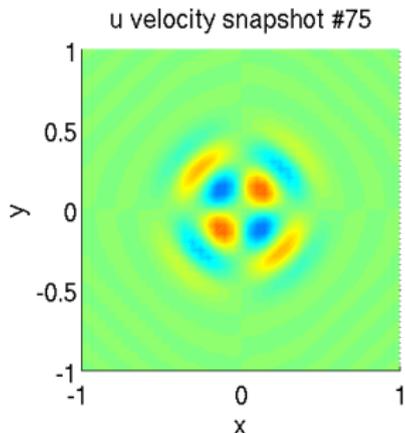
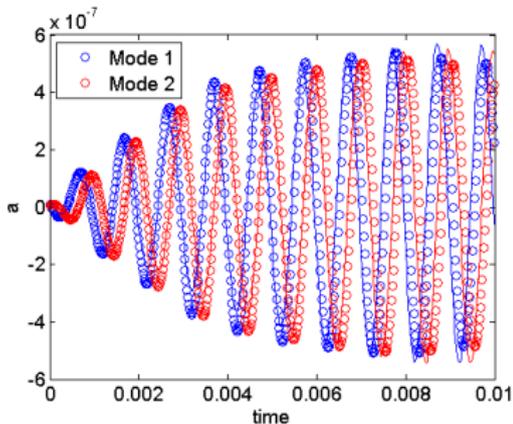
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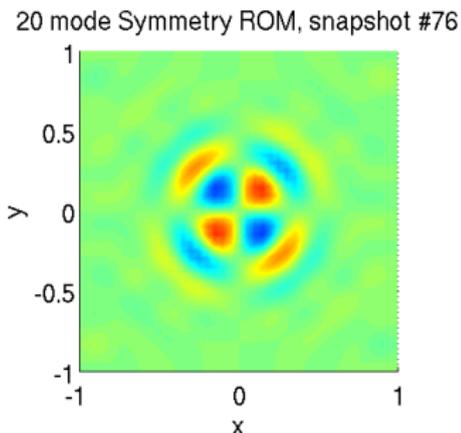
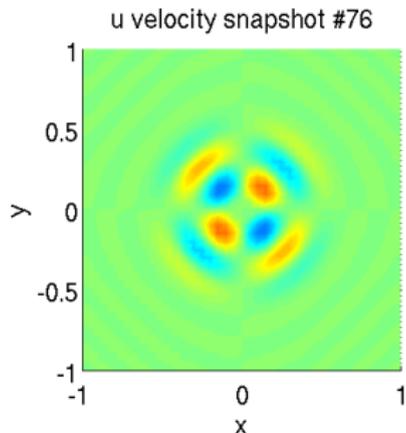
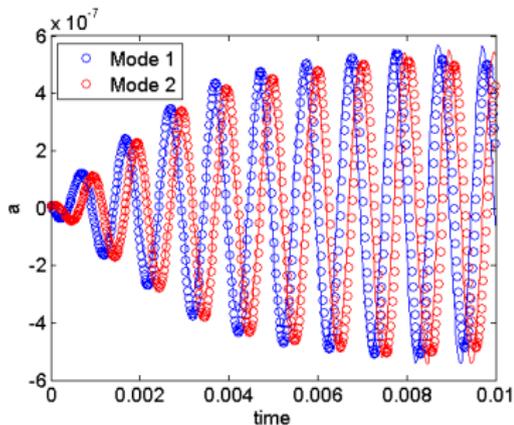
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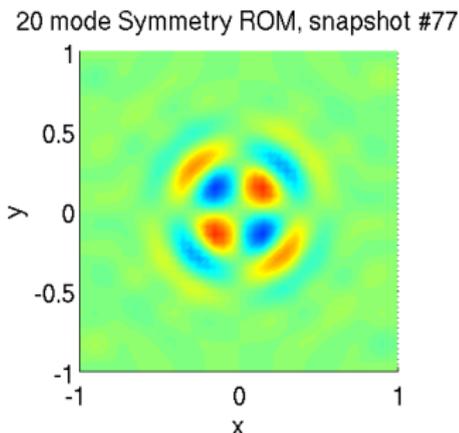
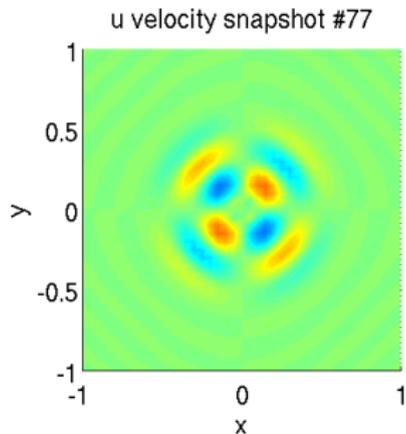
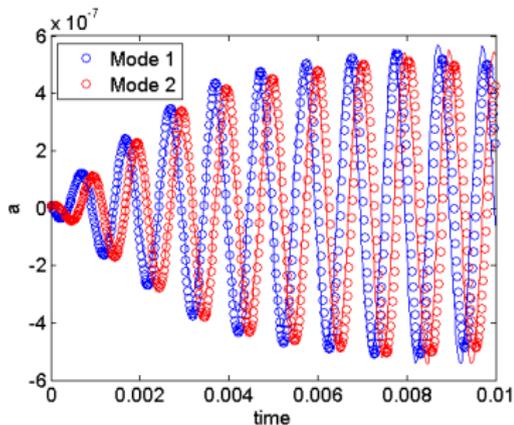
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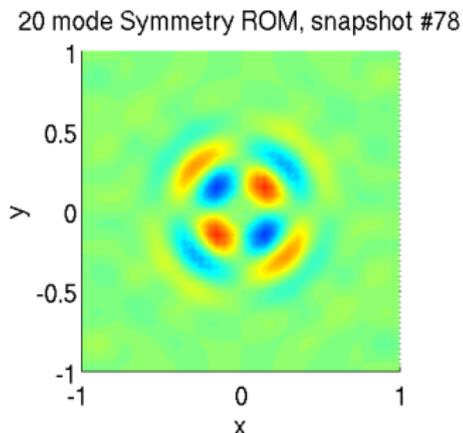
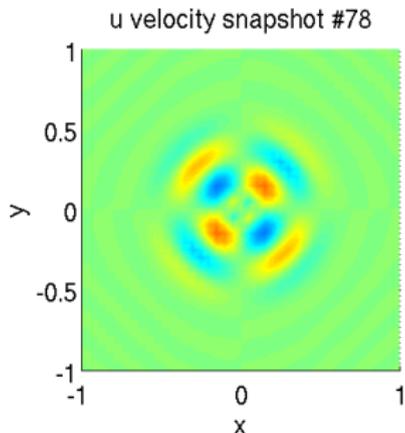
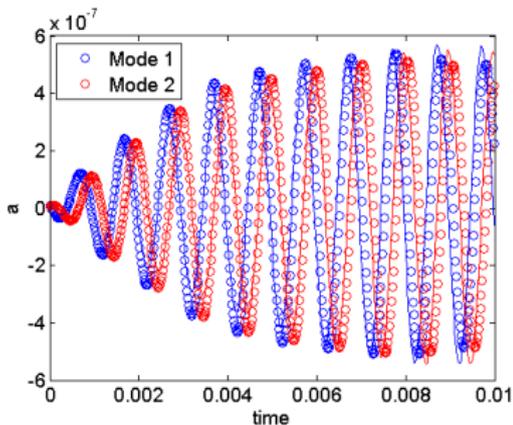
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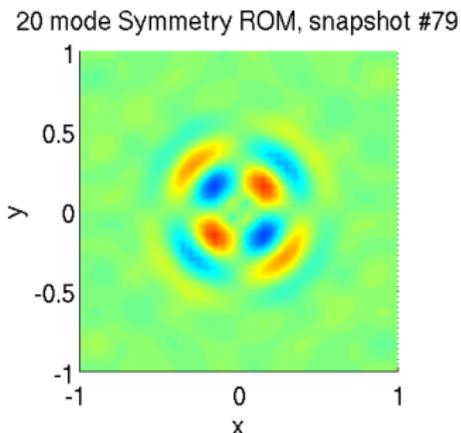
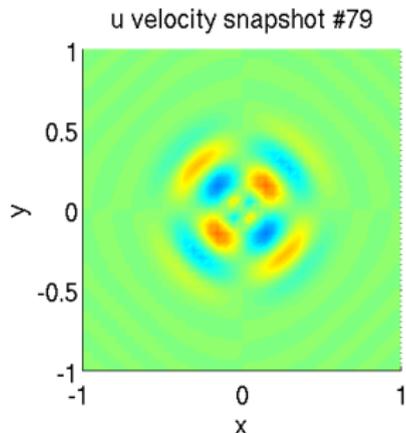
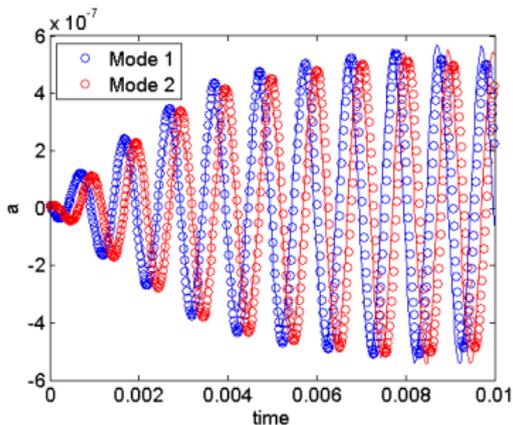
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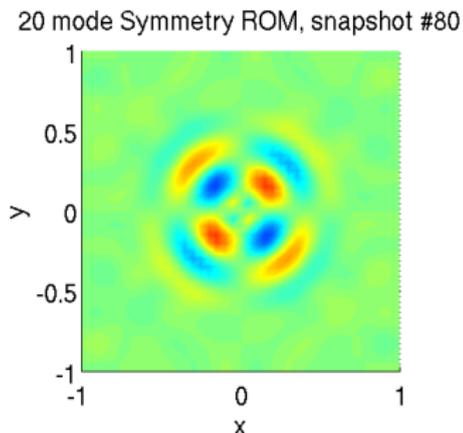
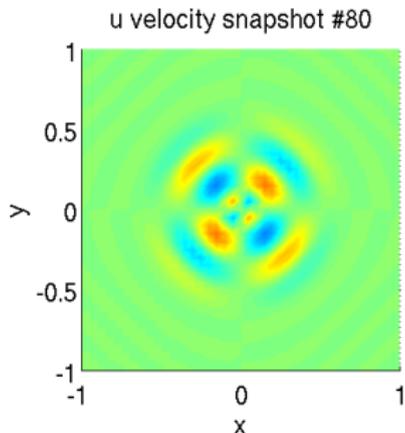
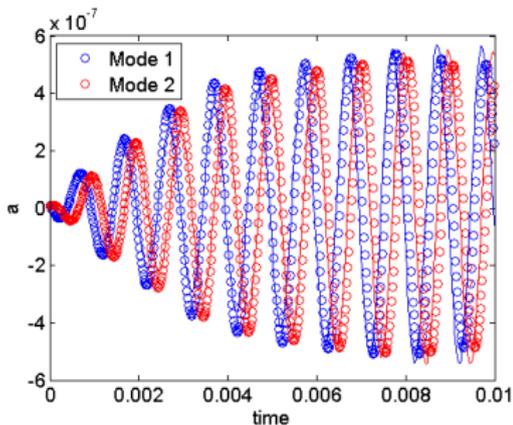
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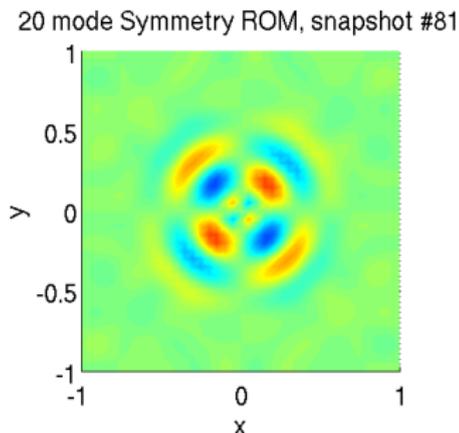
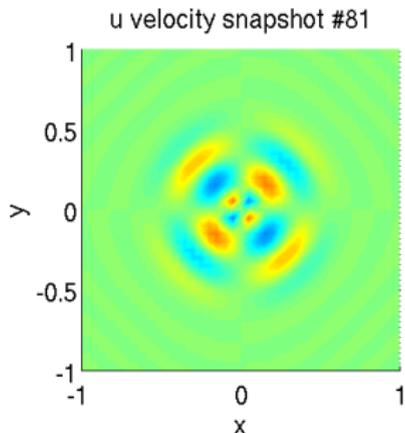
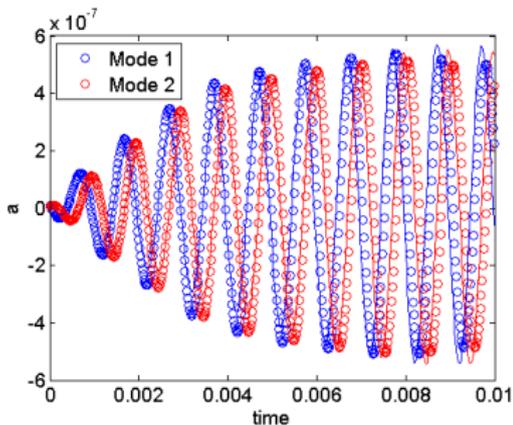
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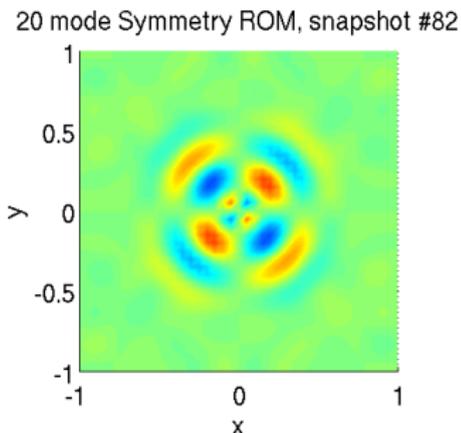
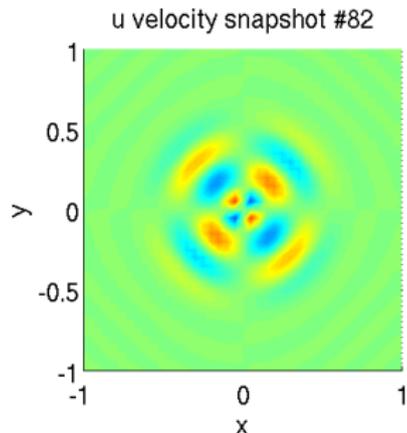
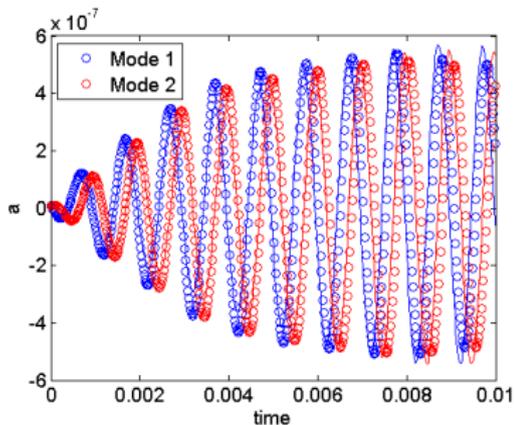
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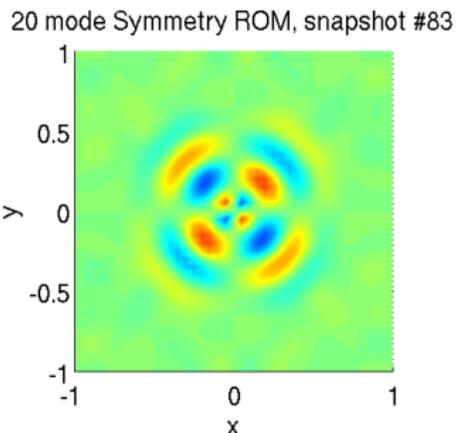
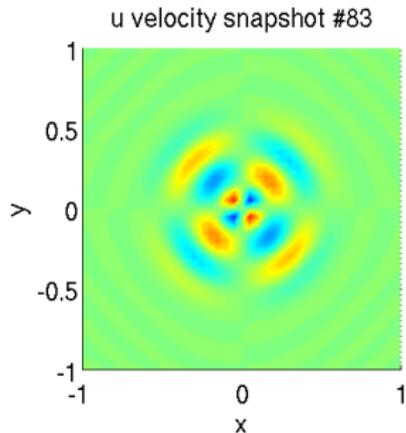
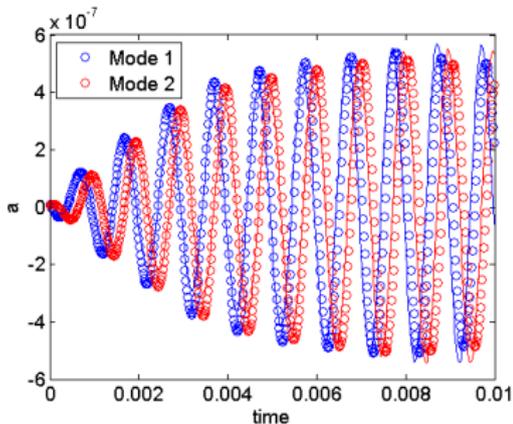
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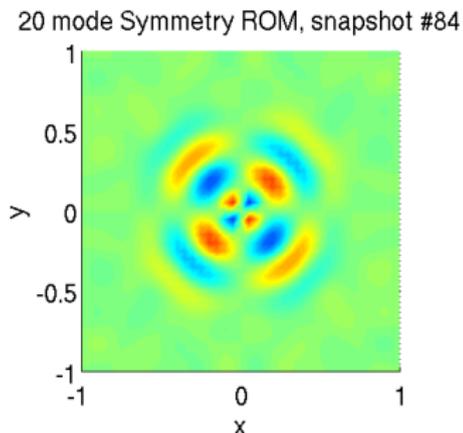
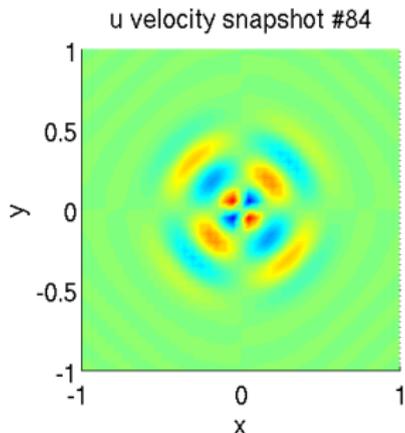
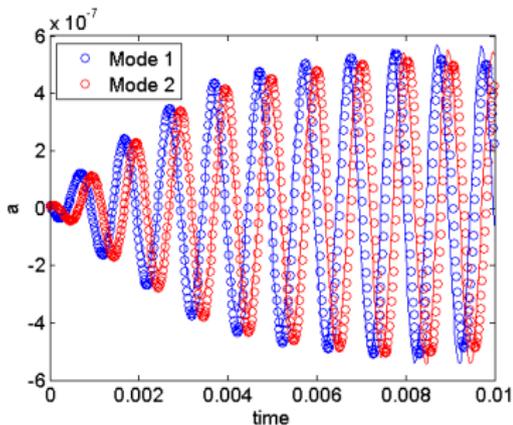
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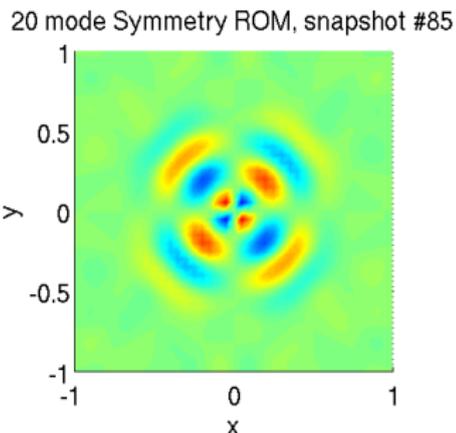
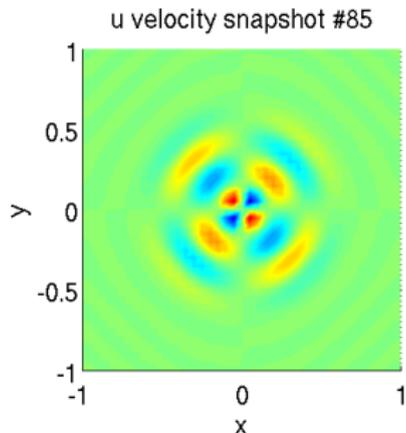
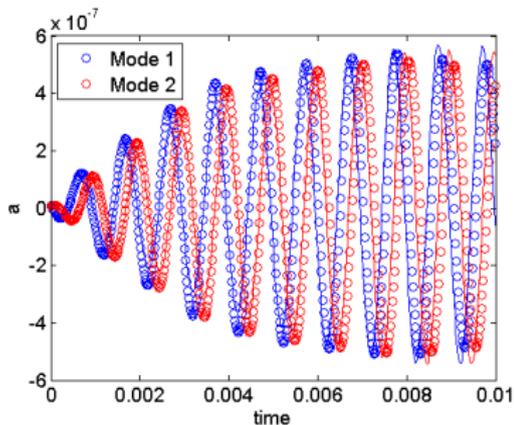
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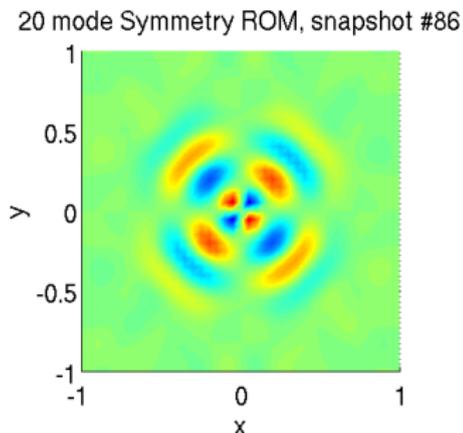
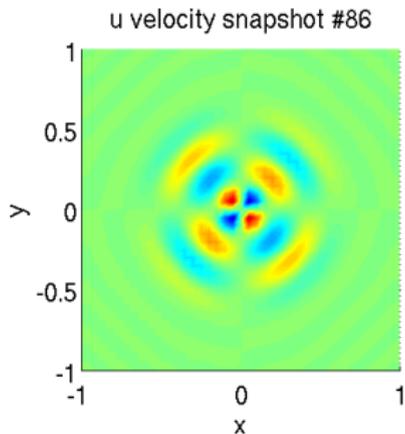
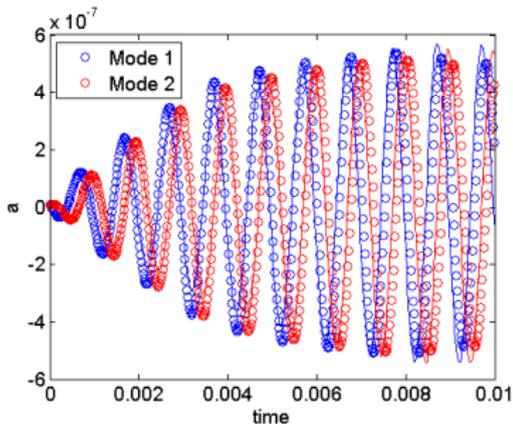
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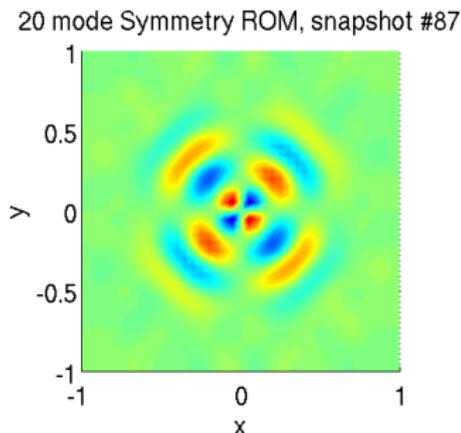
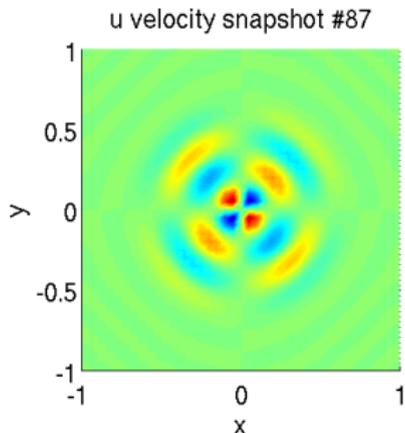
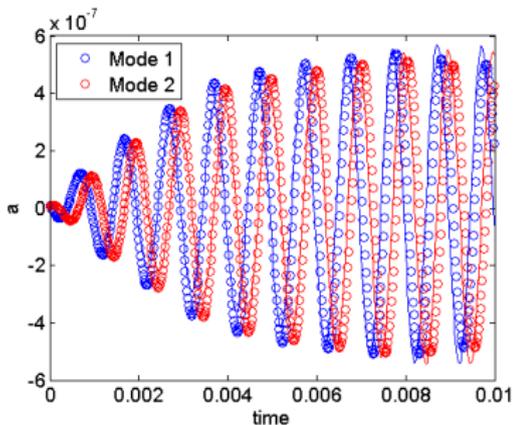
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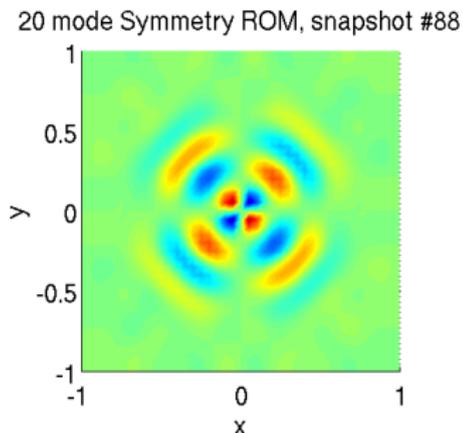
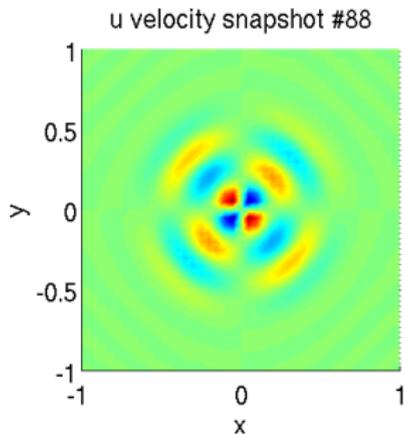
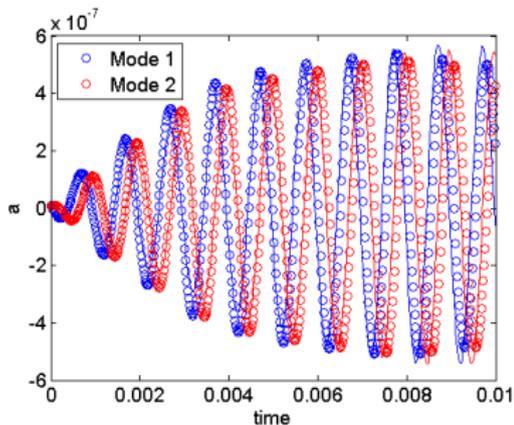
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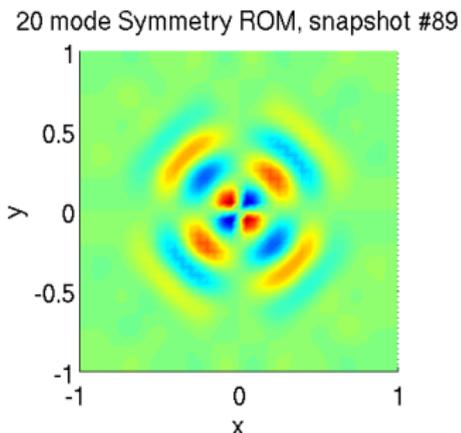
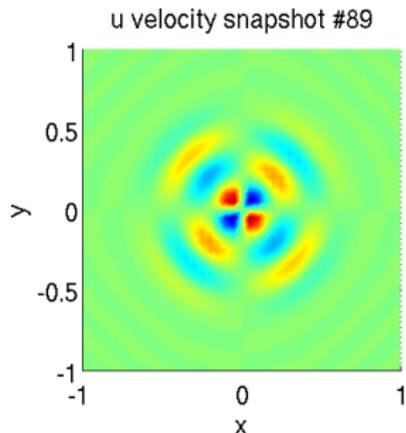
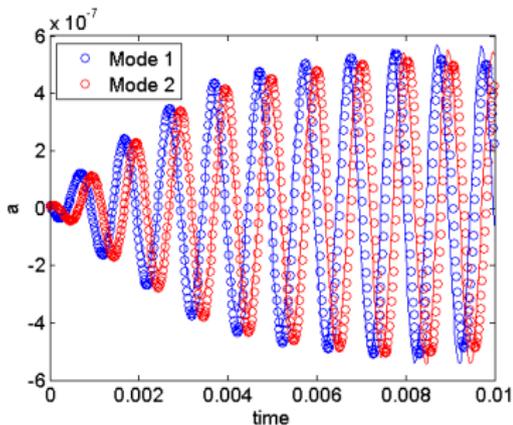
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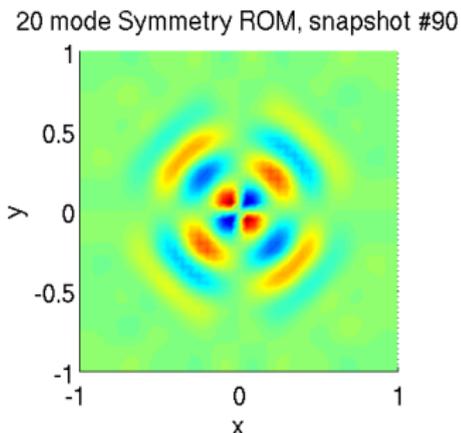
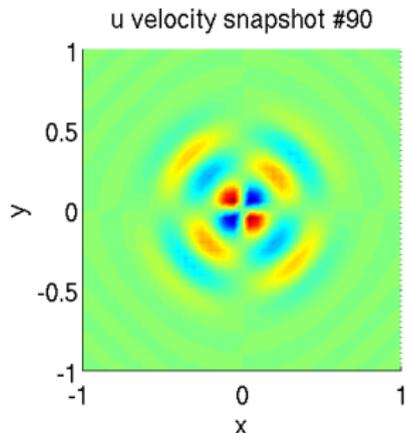
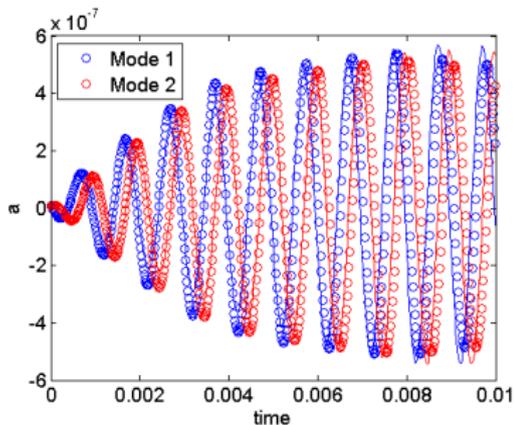
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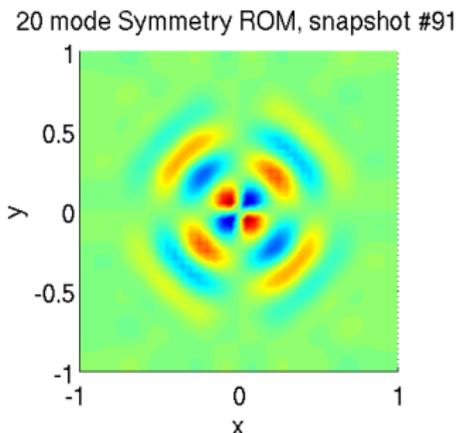
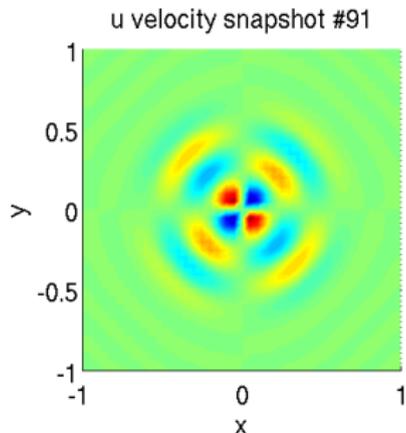
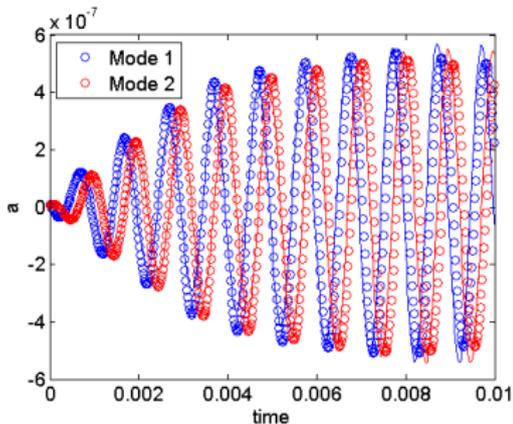
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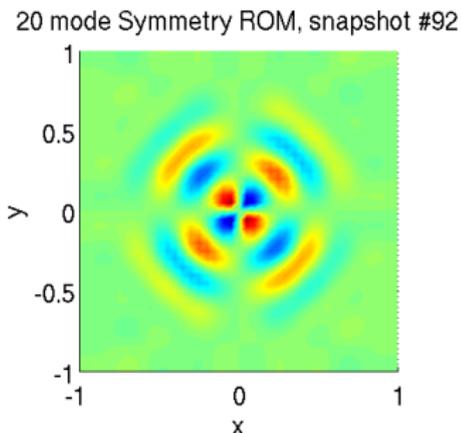
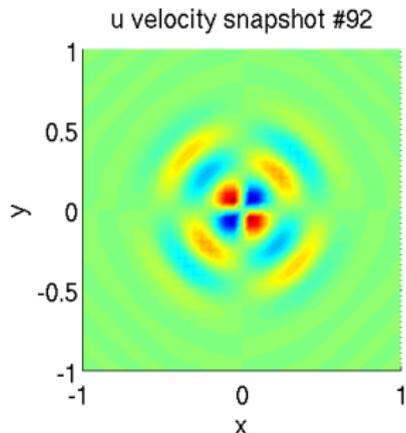
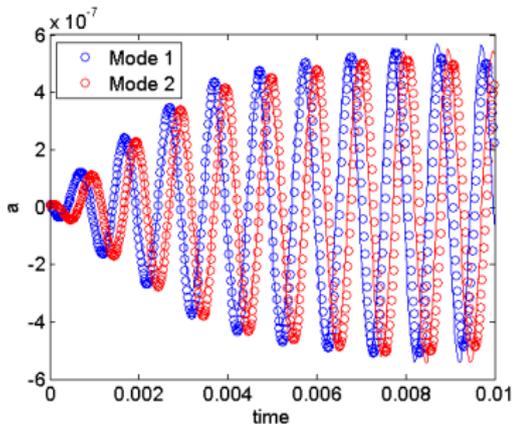
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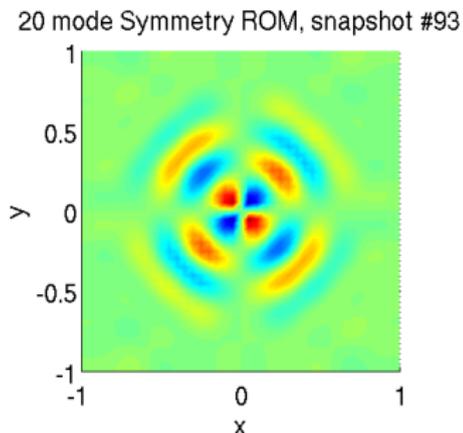
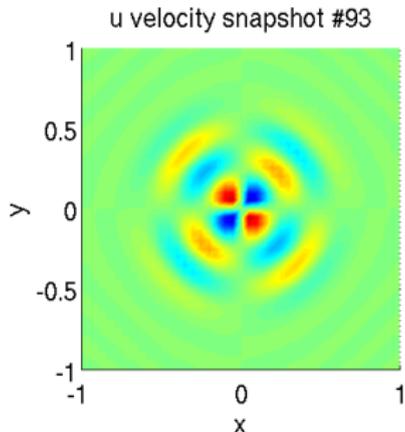
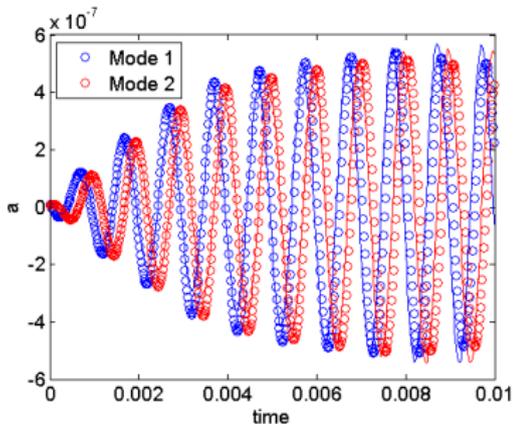
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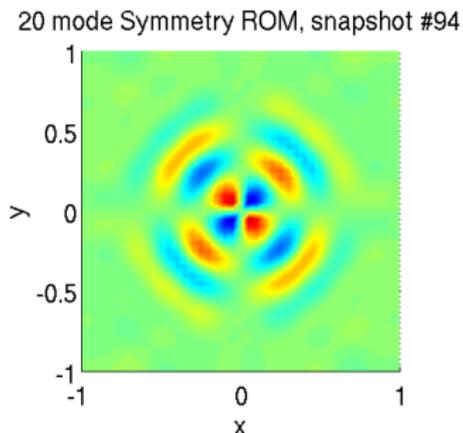
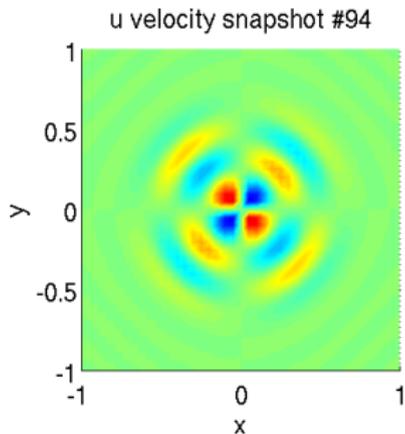
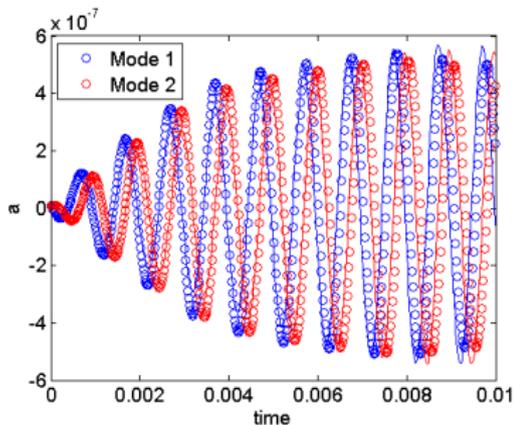
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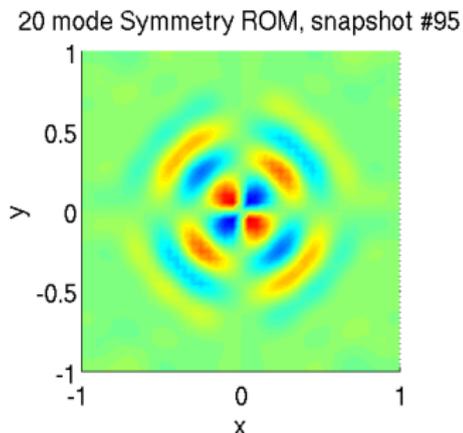
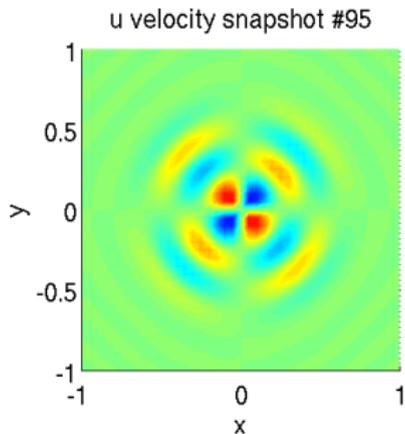
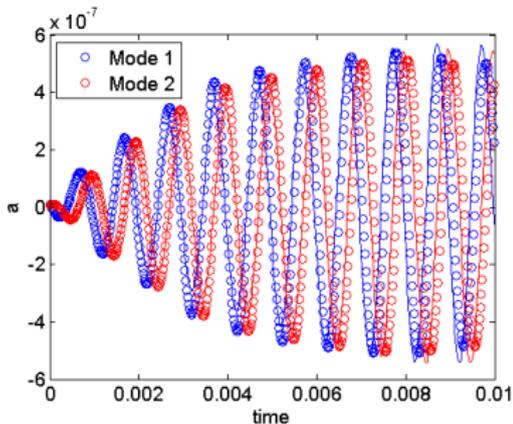
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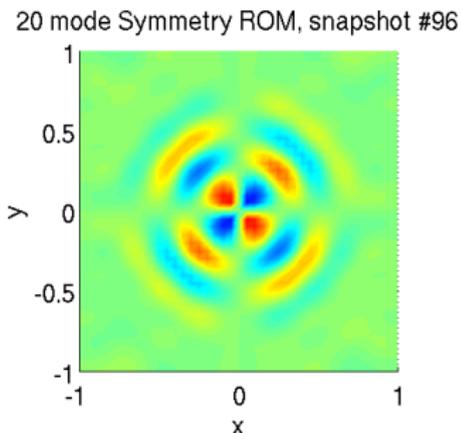
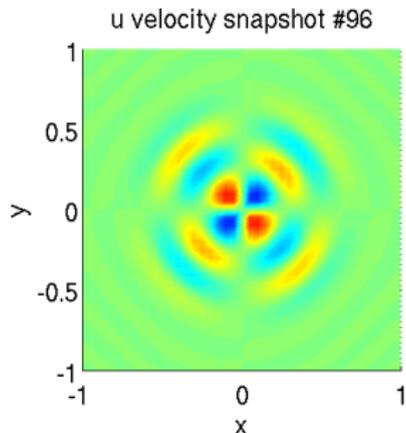
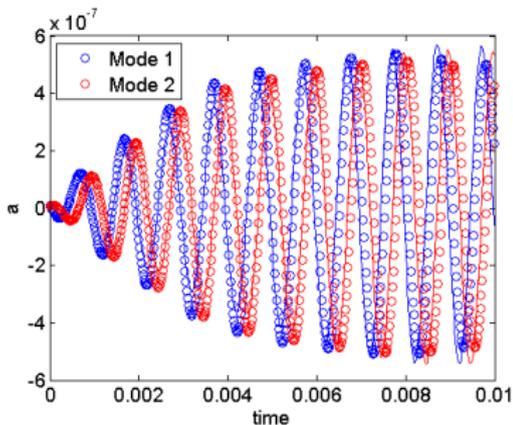
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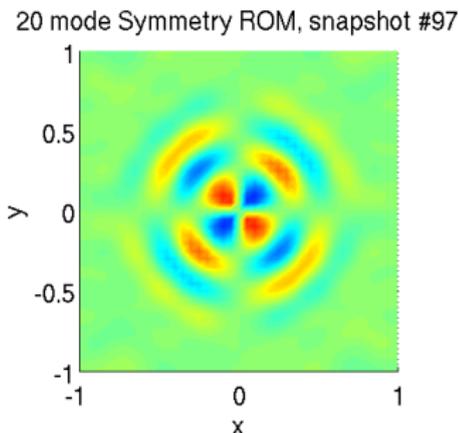
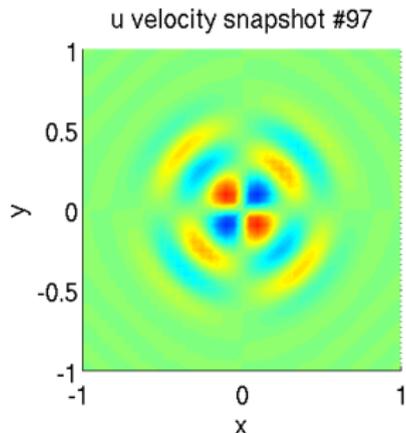
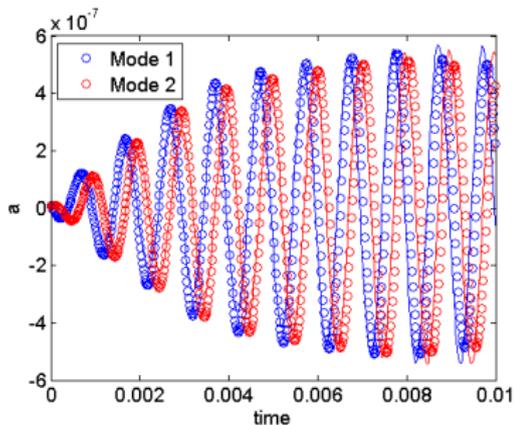
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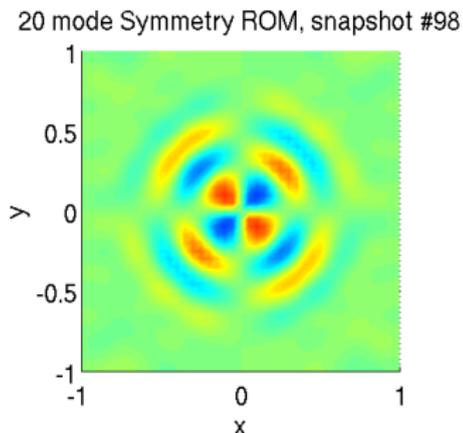
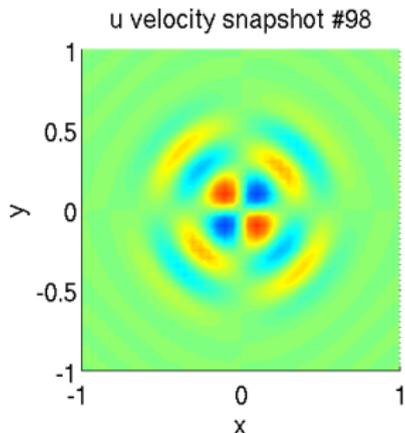
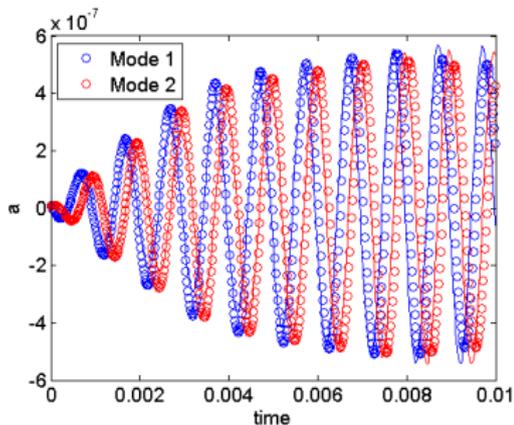
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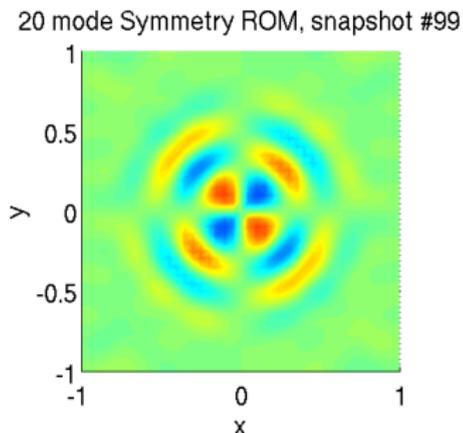
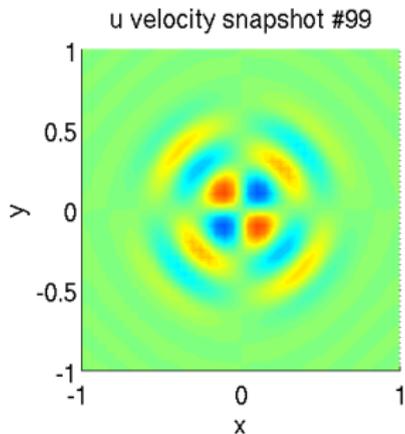
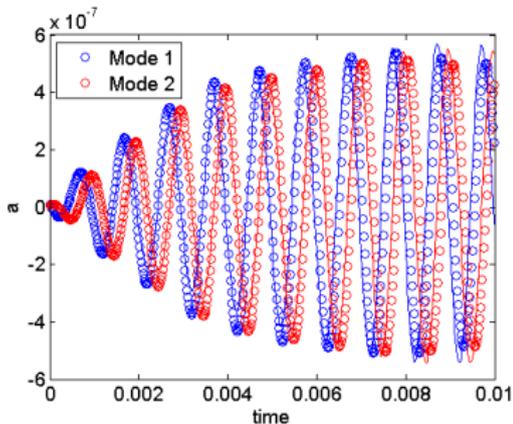
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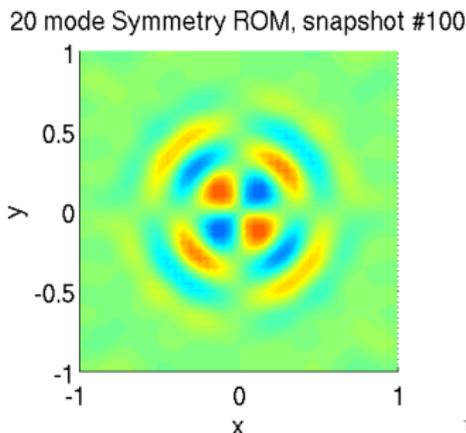
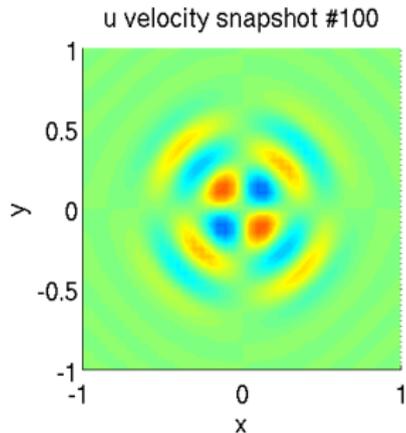
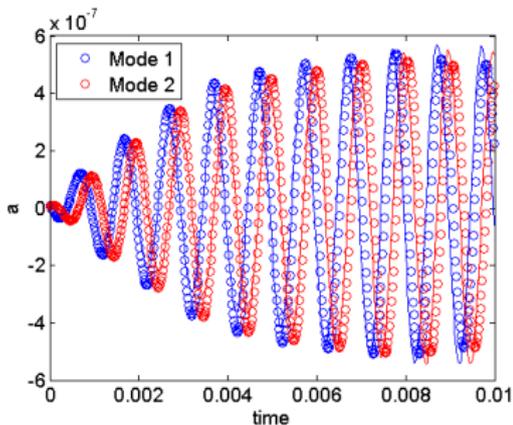
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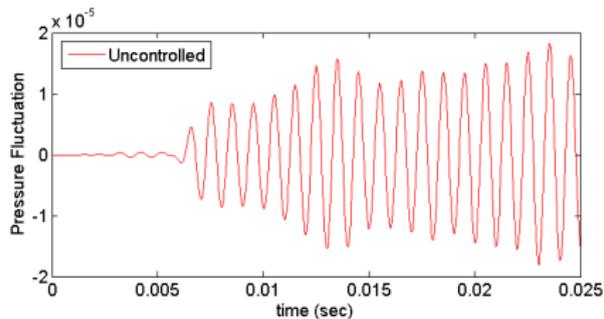
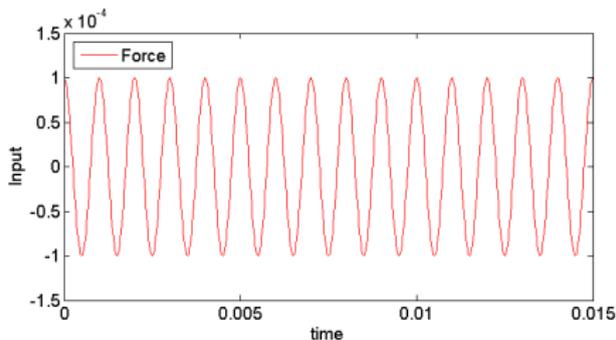
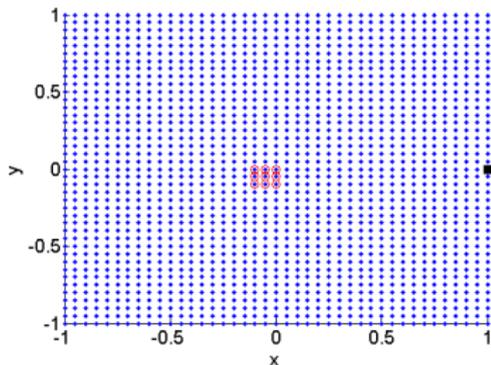


# LQR Control of Driven Pulse

- **Control problem:** compute actuation that will minimize  $p'$  at  $(x, y) = (1, 0)$ .

- ▶ Compute **LQR controller** feedback law  $u_M = -\mathbf{K}\mathbf{x}_M$  to minimize quadratic cost functional using ROM\*:

$$J \equiv \frac{1}{T} \int_0^T [p'^2(1, 0; t) + \tau u^2] dt$$



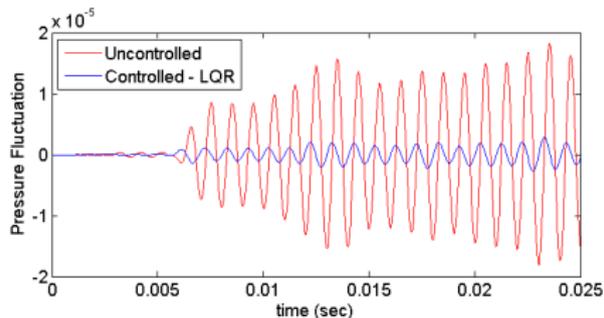
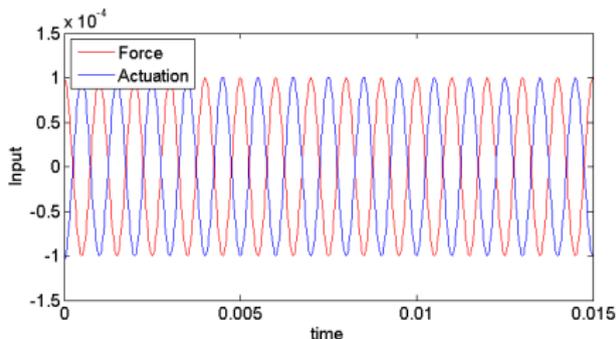
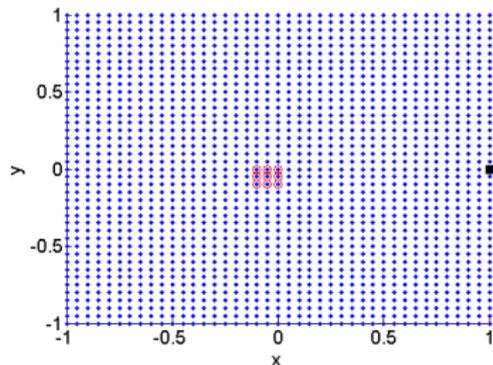
- \* The computation of  $\mathbf{K} = \mathbf{R}^{-1}\mathbf{B}^T\mathbf{X}$  requires solution of algebraic Riccati equation  $\mathbf{A}^T\mathbf{X} + \mathbf{X}\mathbf{A} - \frac{1}{\tau}\mathbf{X}\mathbf{B}\mathbf{B}^T\mathbf{X} + \mathbf{C}^T\mathbf{C} = \mathbf{0}$  [8].

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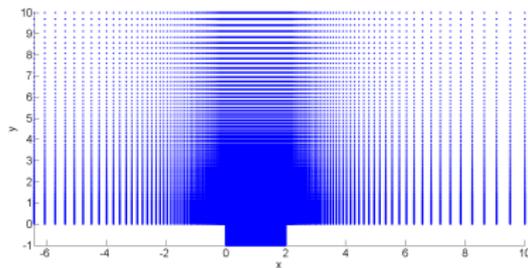
$$J \equiv \frac{1}{T} \int_0^T [p'^2(1, 0; t) + \tau u^2] dt$$



\* The computation of  $\mathbf{K} = \mathbf{R}^{-1}\mathbf{B}^T\mathbf{X}$  requires solution of algebraic Riccati equation  $\mathbf{A}^T\mathbf{X} + \mathbf{X}\mathbf{A} - \frac{1}{\tau}\mathbf{X}\mathbf{B}\mathbf{B}^T\mathbf{X} + \mathbf{C}^T\mathbf{C} = \mathbf{0}$  [8].

# Laminar Viscous Driven Cavity Problem

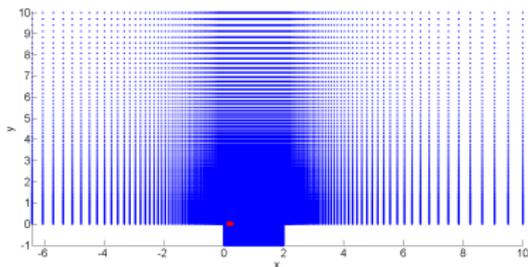
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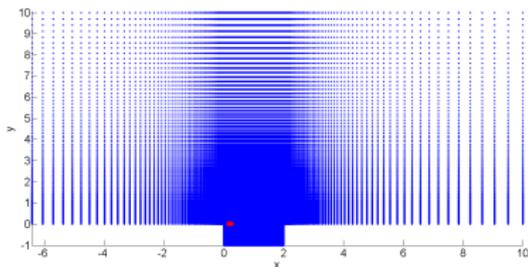
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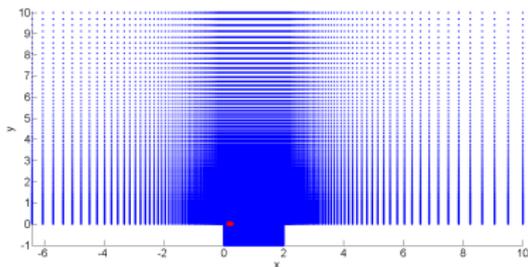


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Inherently non-linear problem!  
High-fidelity solution obtained by solving full *non-linear* Navier-Stokes equations.



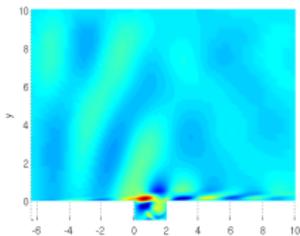
# Expected ROM Performance

ROM based on Navier-Stokes equations  
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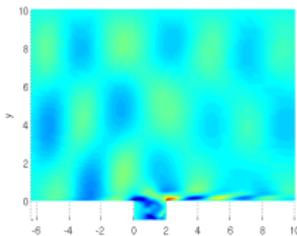
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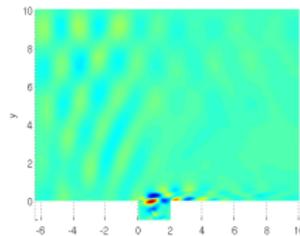
Non-linear dynamics of flow  
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POD reduced basis modes.



$u$  mode 1  
(24.9% energy)



$u$  mode 2  
(23.7% energy)



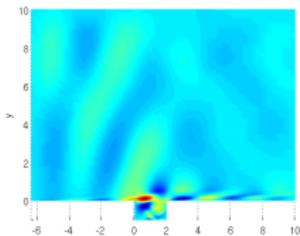
$u$  mode 3  
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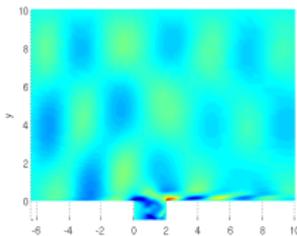
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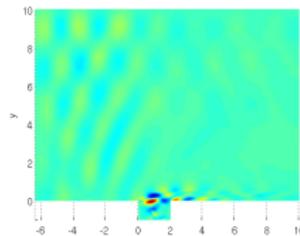
Non-linear dynamics of the flow  
*are not* fully captured in equations  
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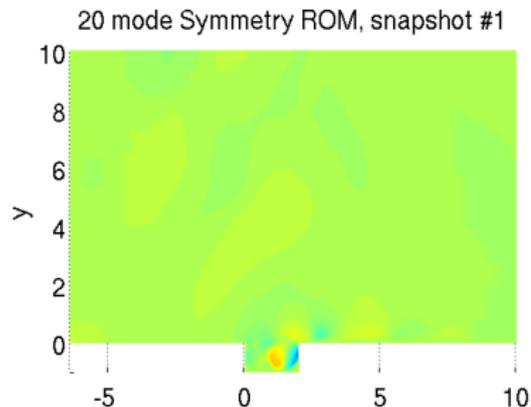
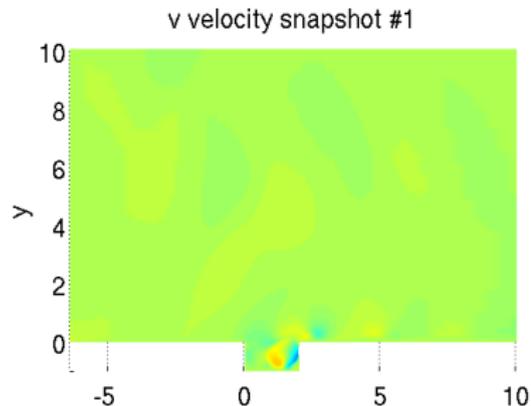
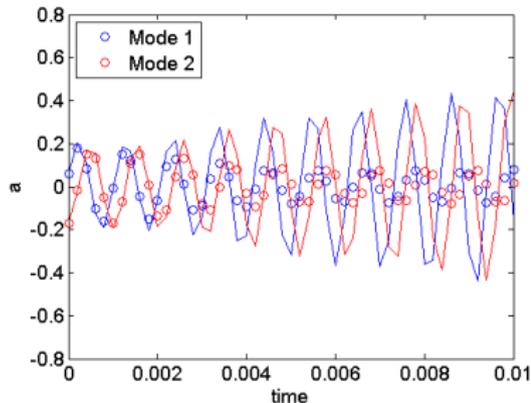


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$$\mathbf{q}'_{,t} + \mathbf{A}_i(\bar{\mathbf{q}})\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} = \mathbf{F}$$

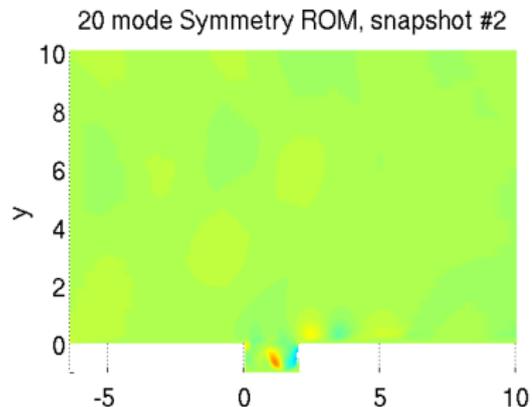
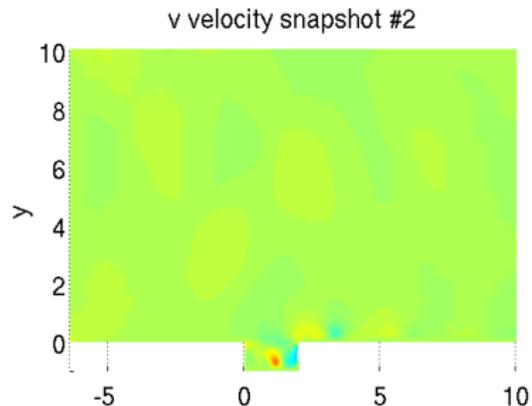
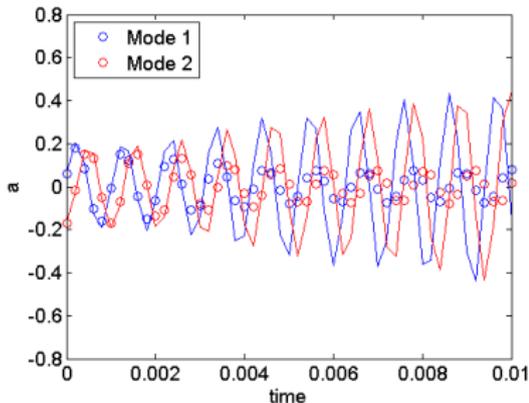
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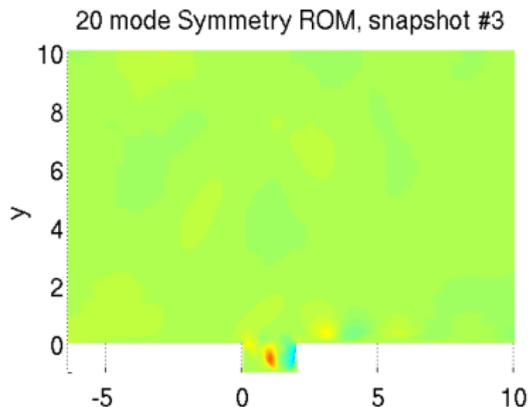
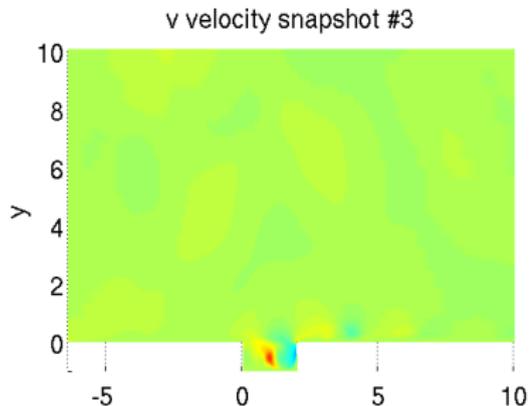
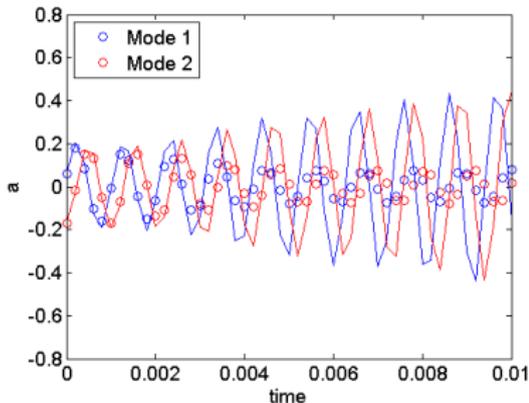
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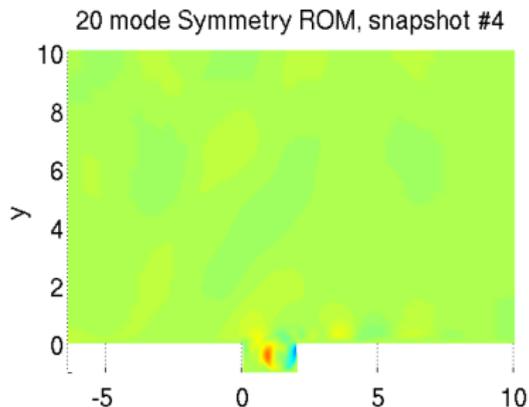
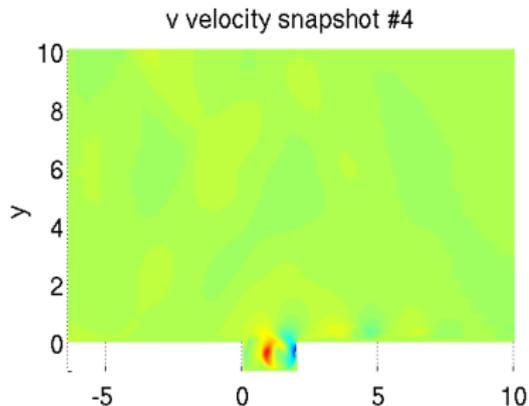
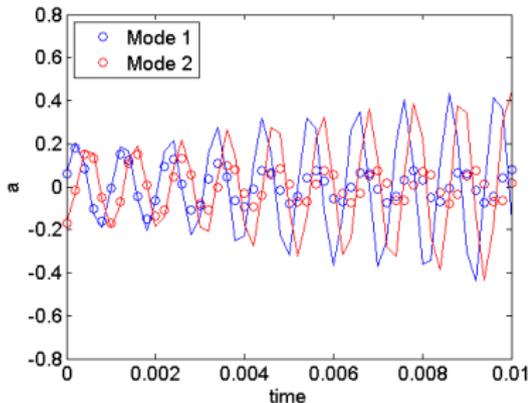
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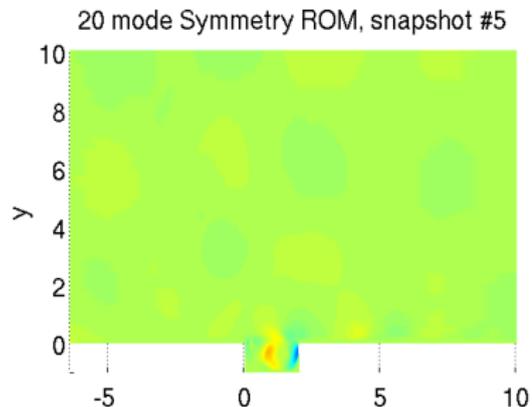
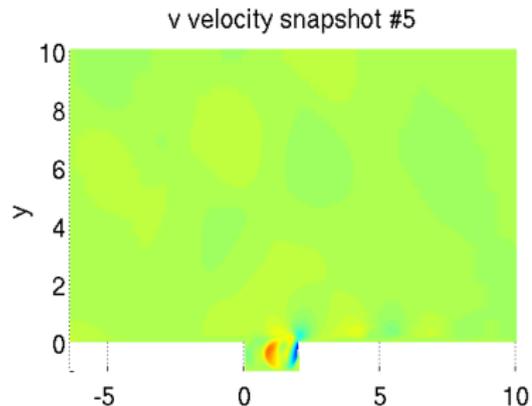
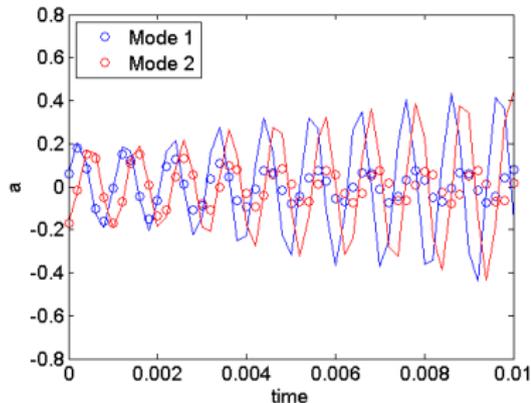
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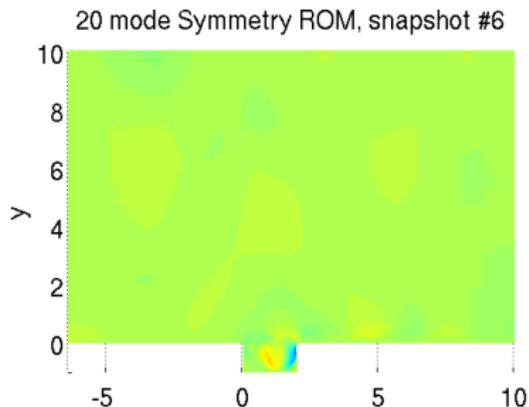
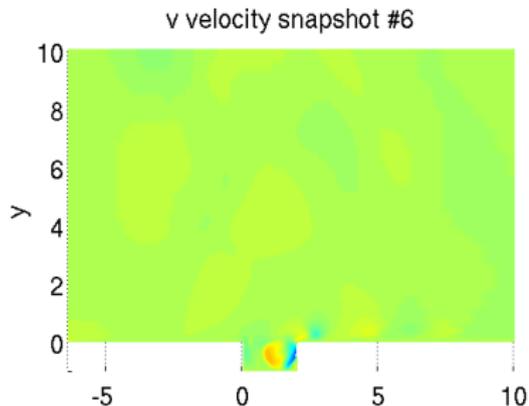
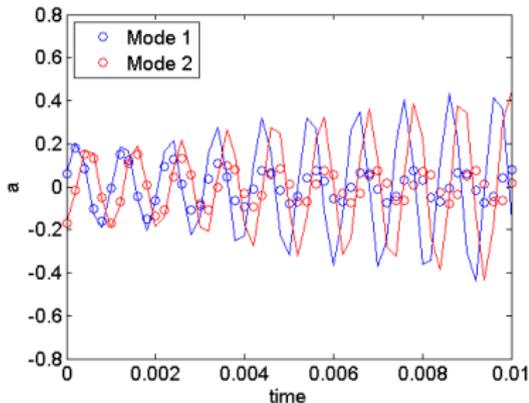
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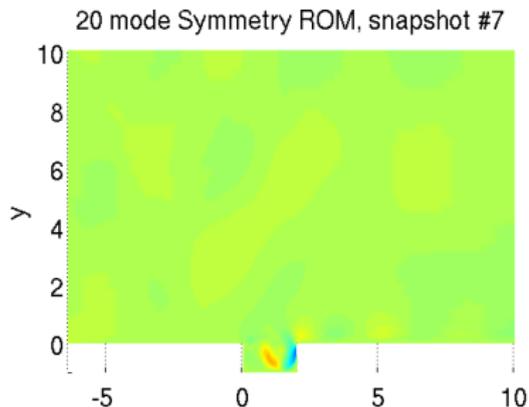
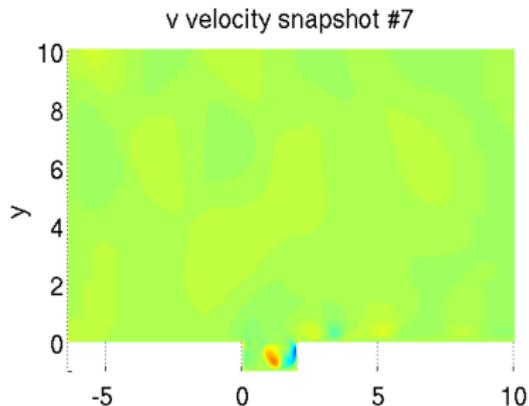
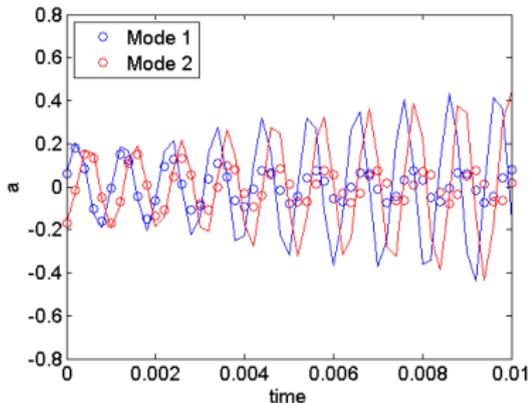
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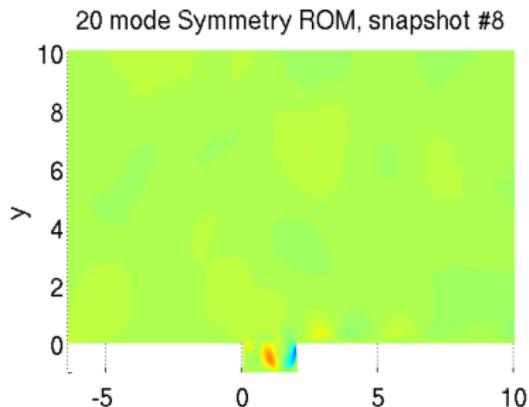
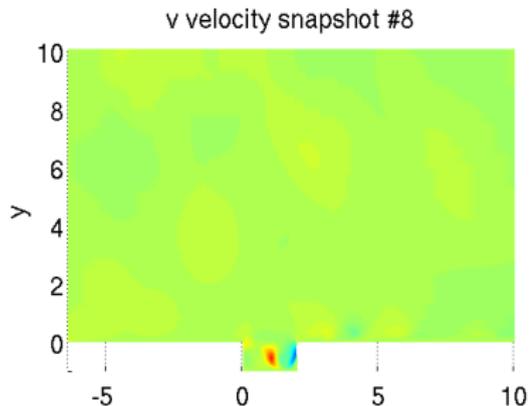
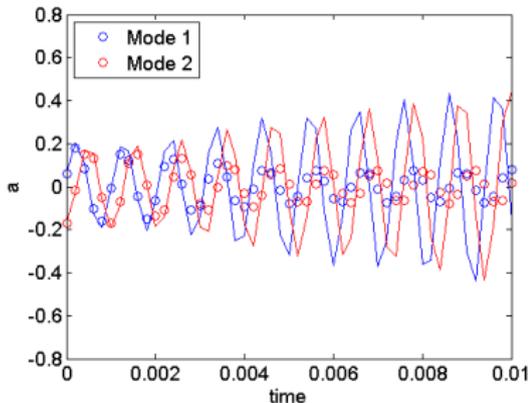
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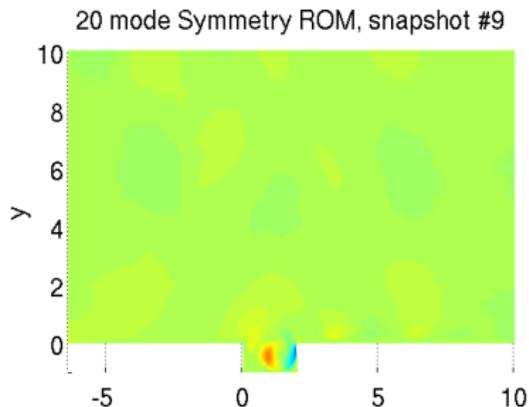
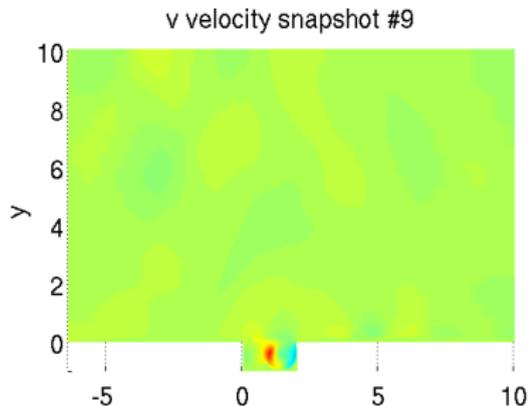
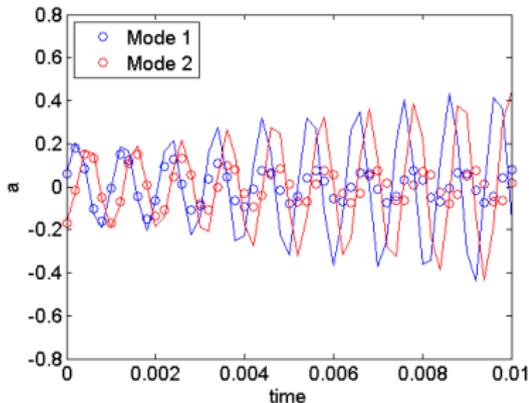
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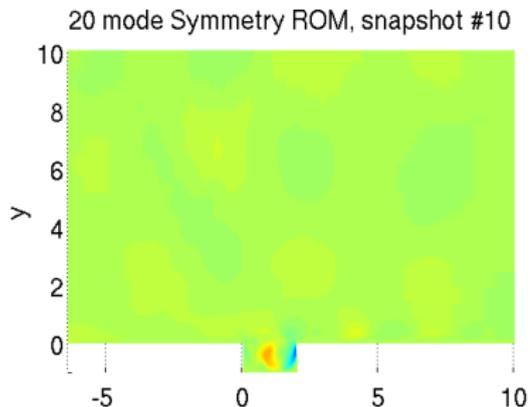
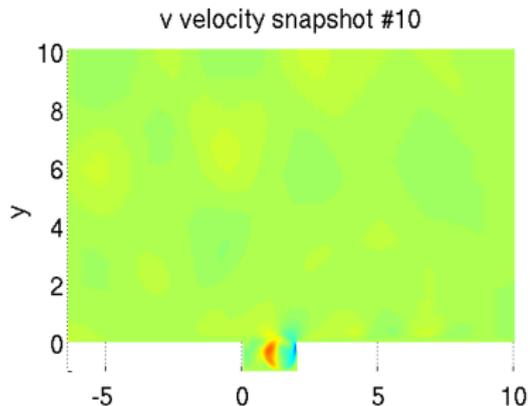
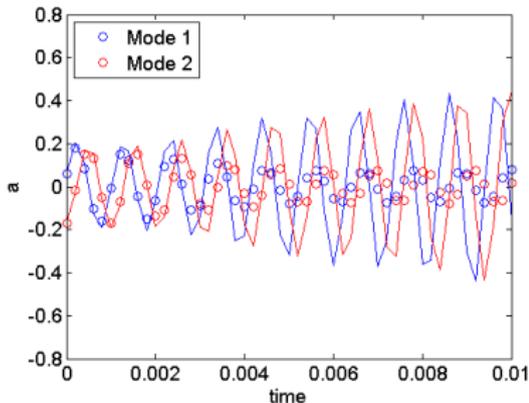
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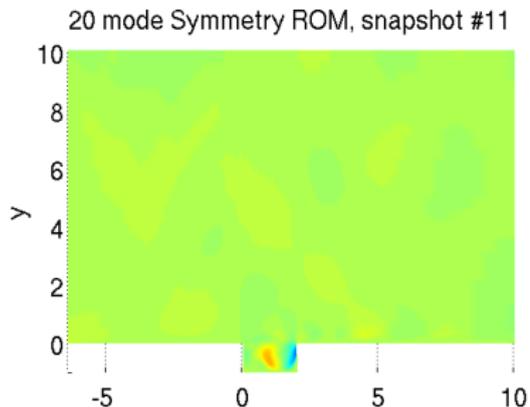
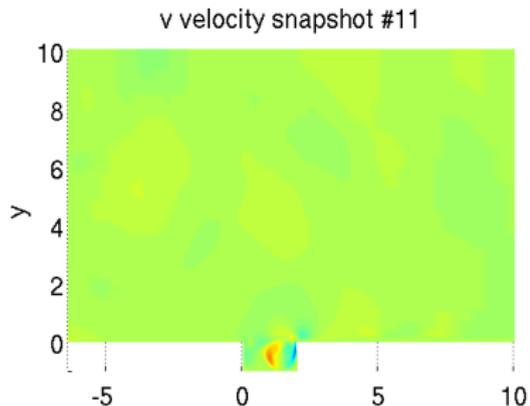
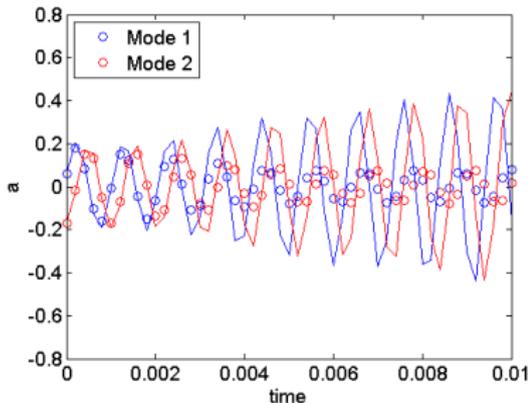
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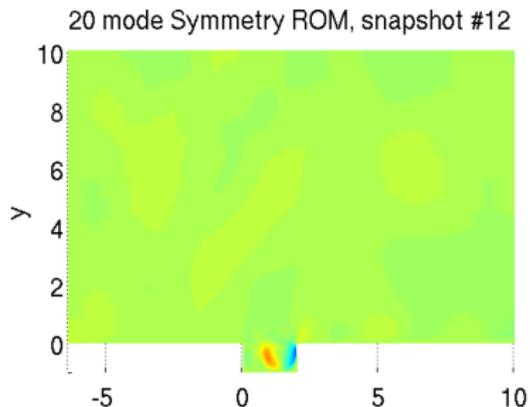
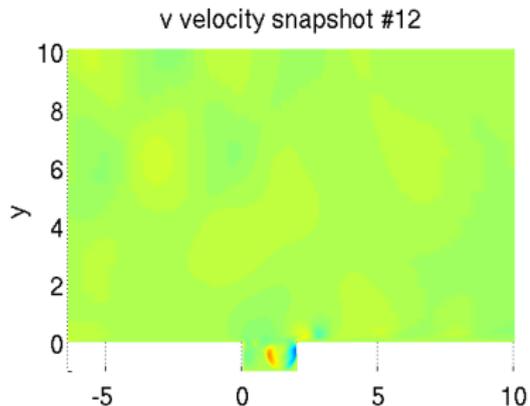
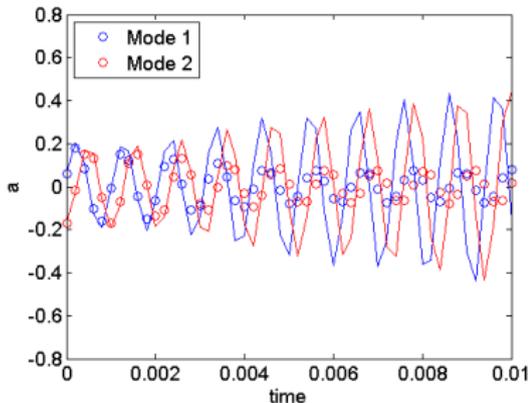
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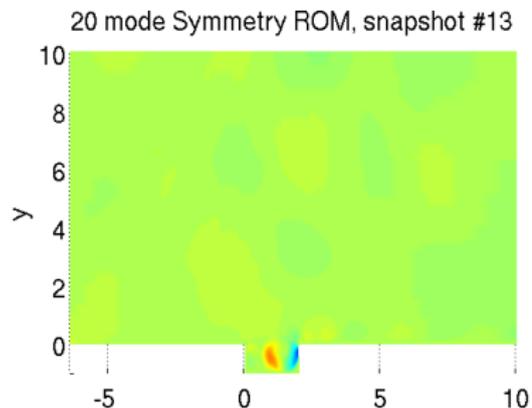
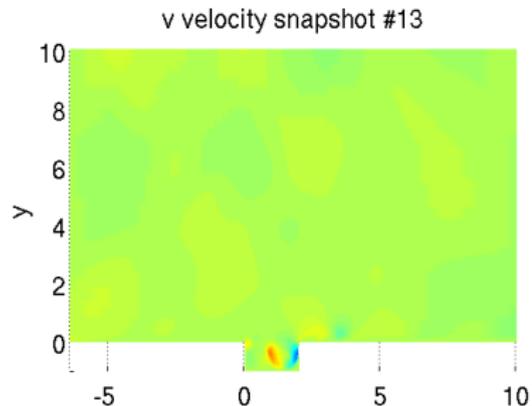
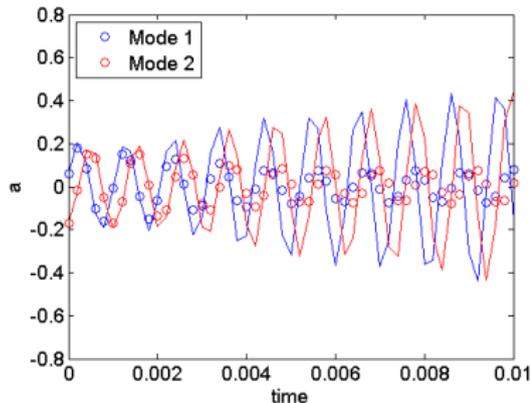
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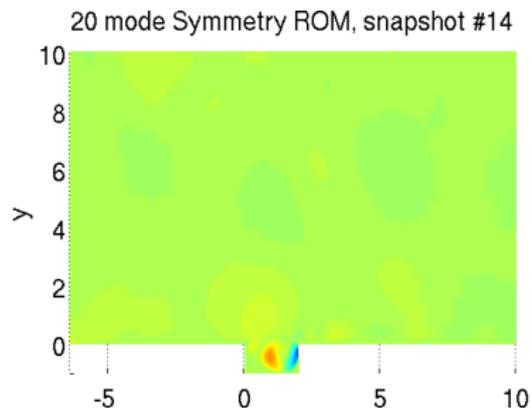
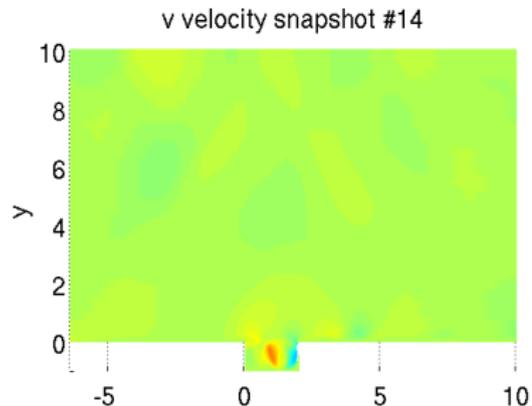
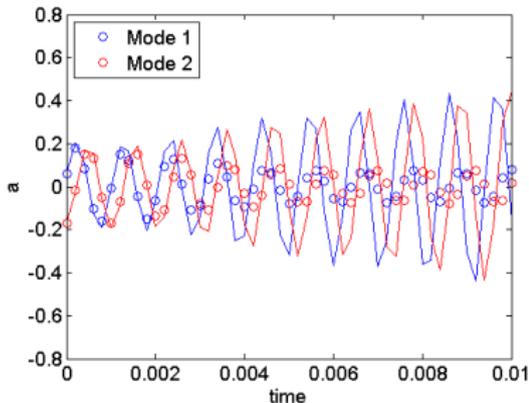
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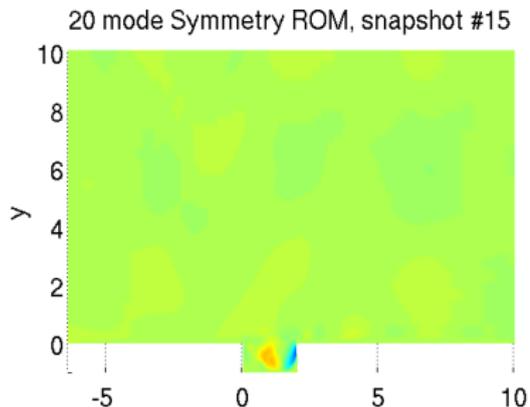
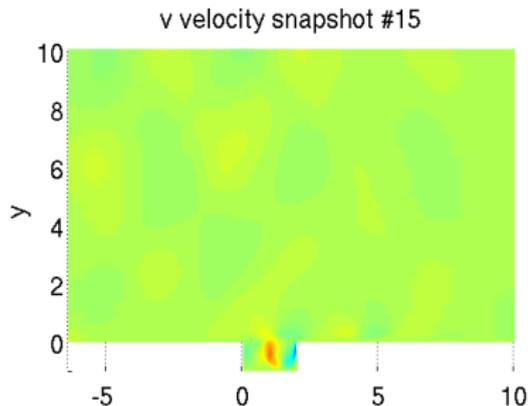
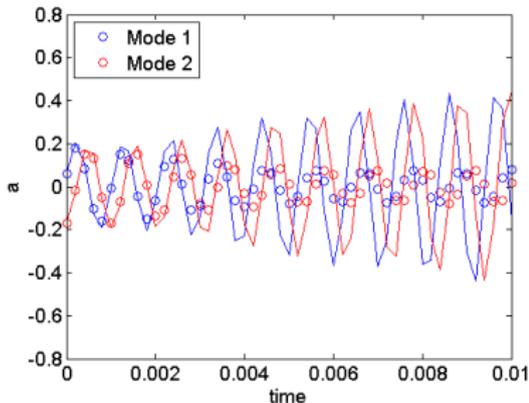
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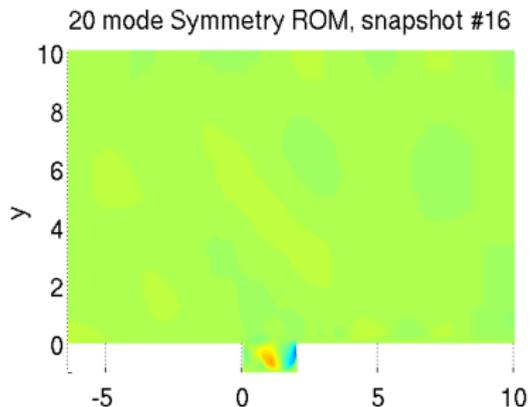
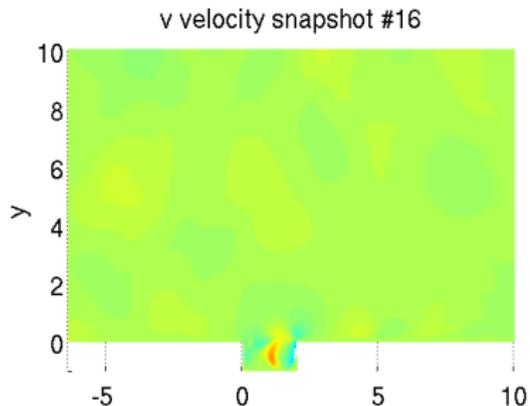
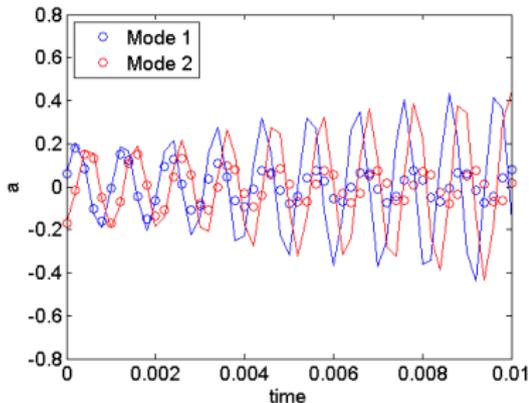
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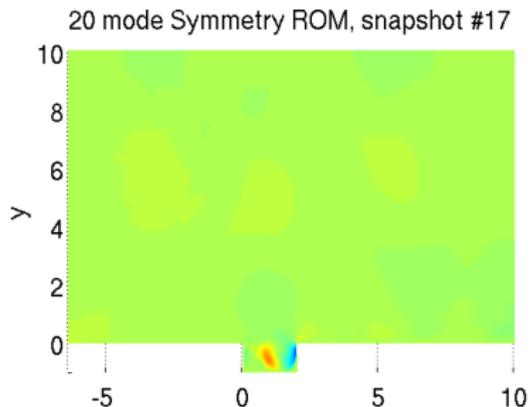
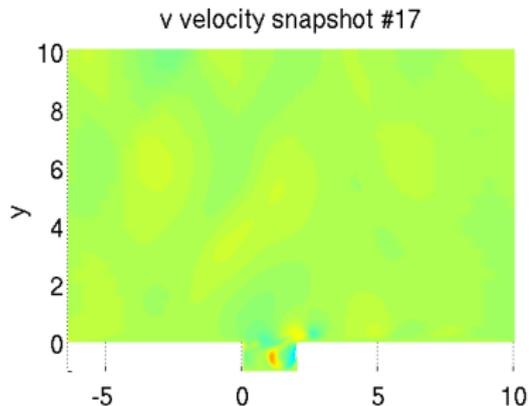
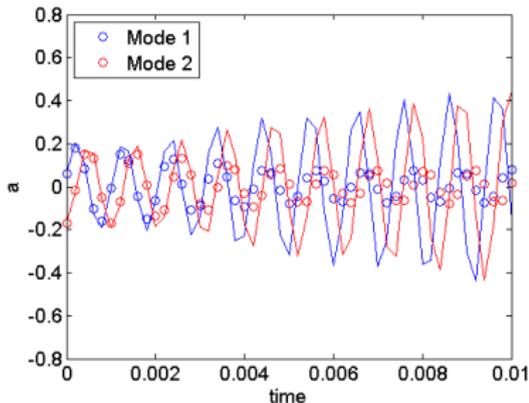
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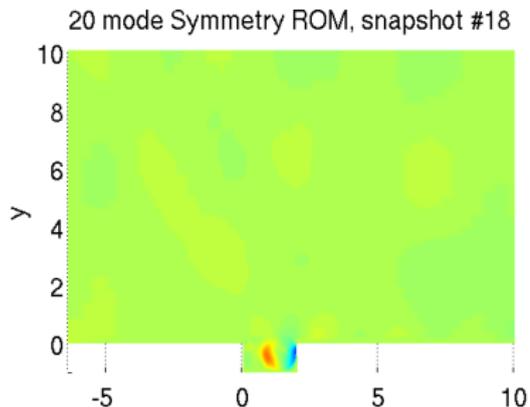
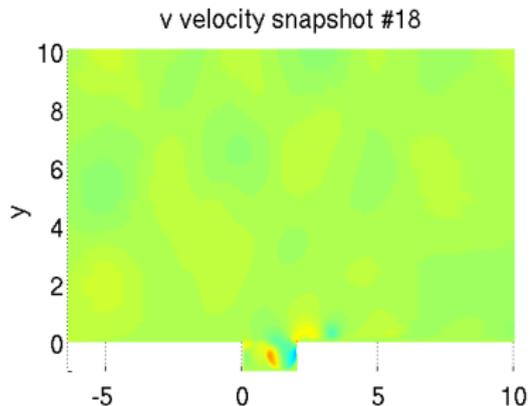
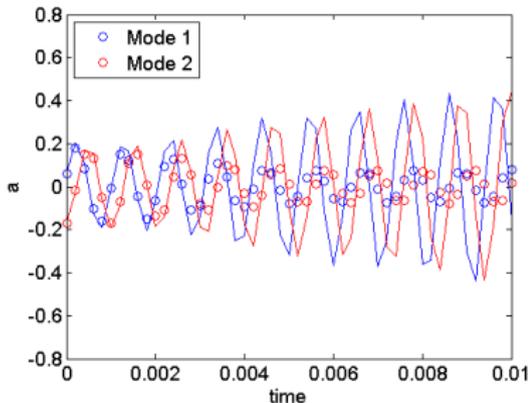
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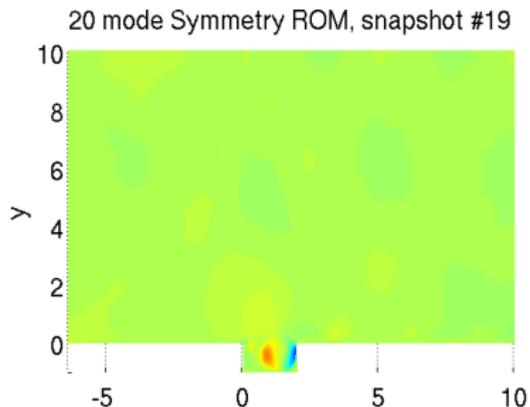
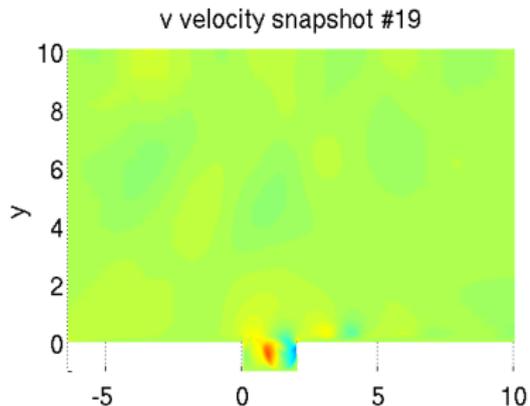
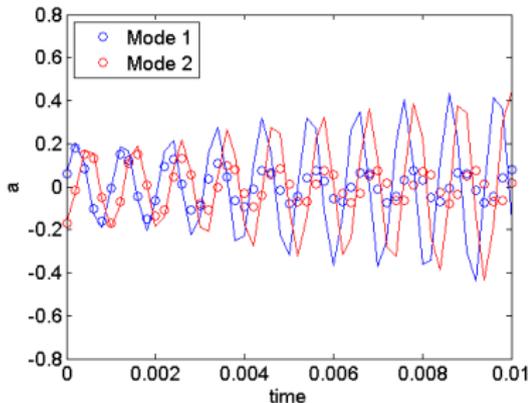
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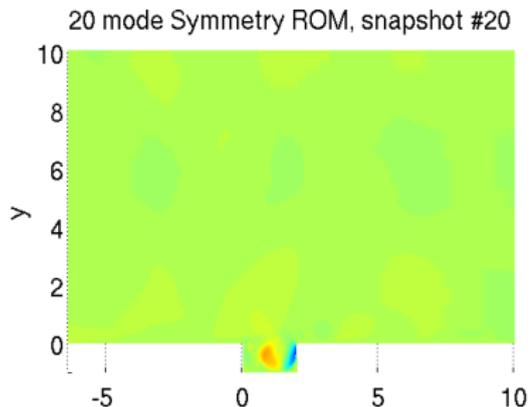
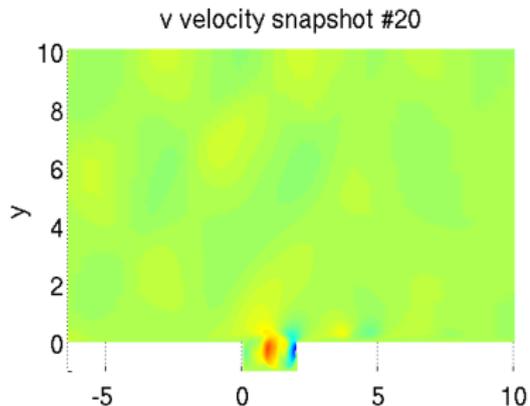
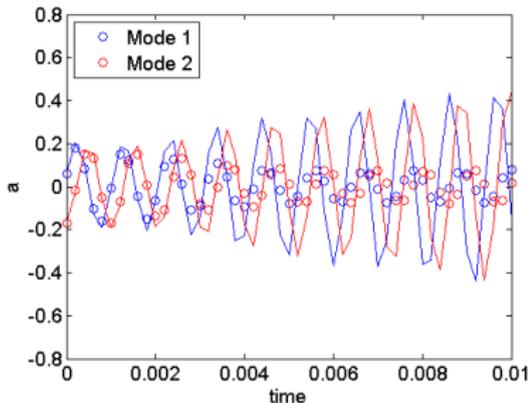
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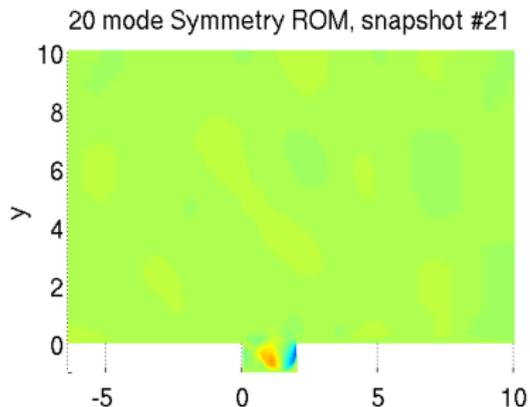
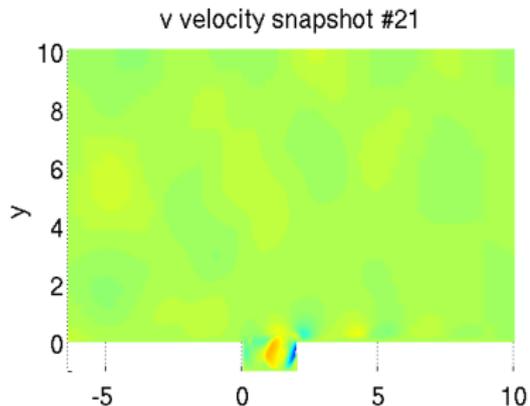
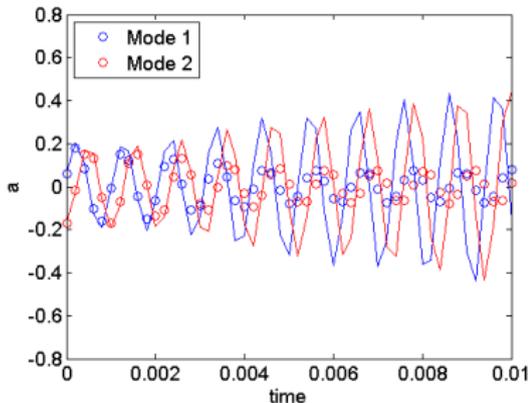
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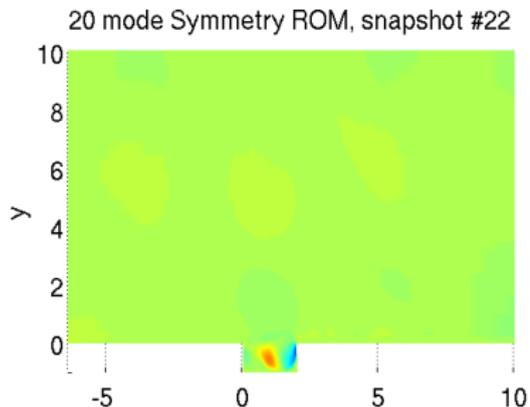
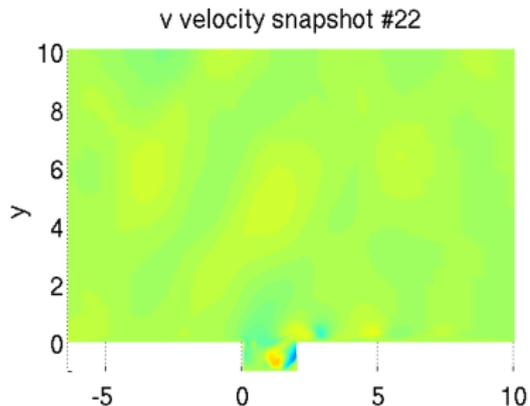
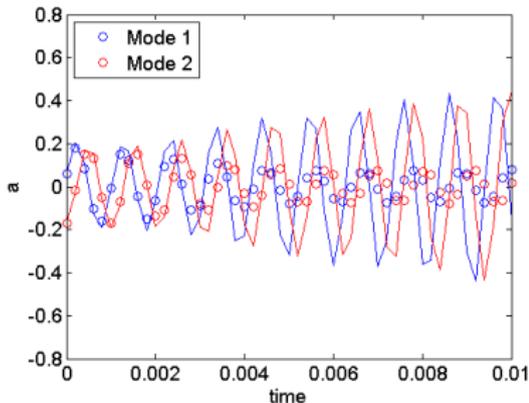
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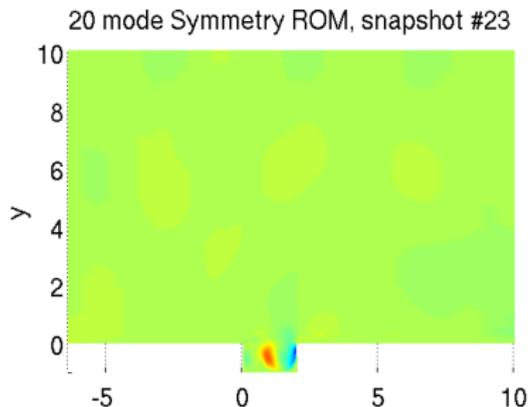
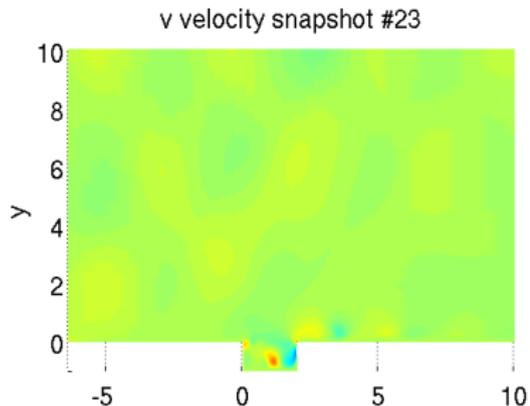
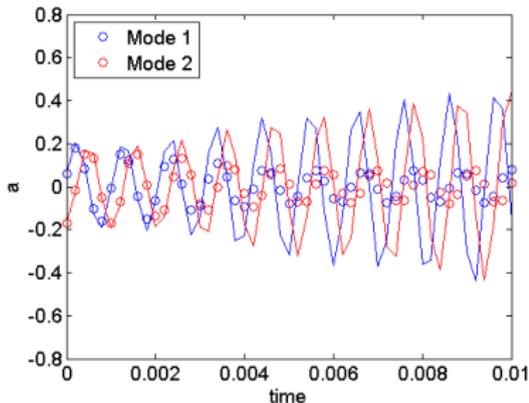
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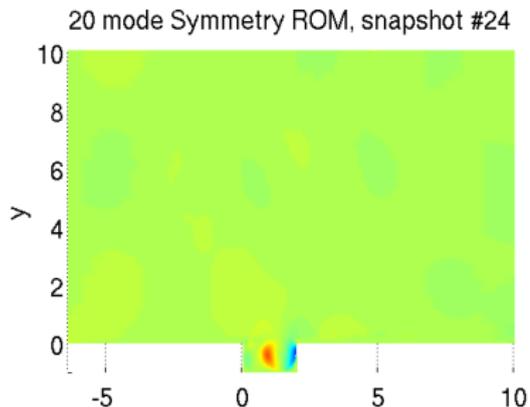
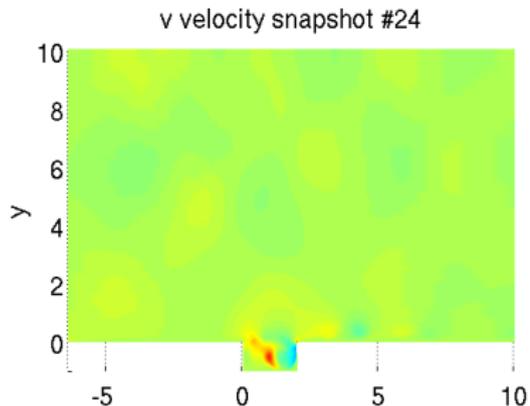
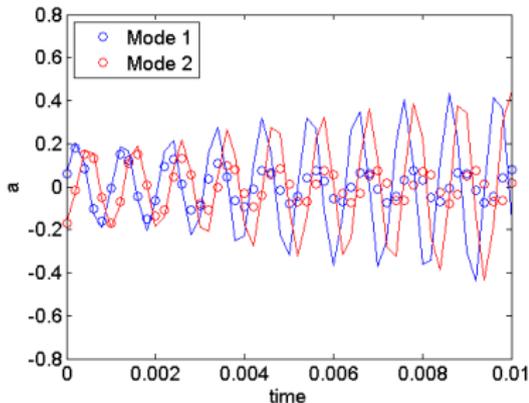
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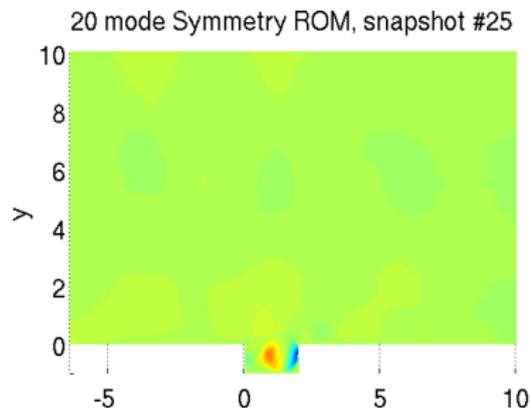
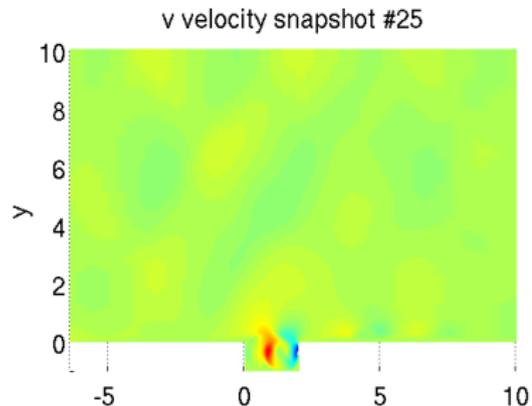
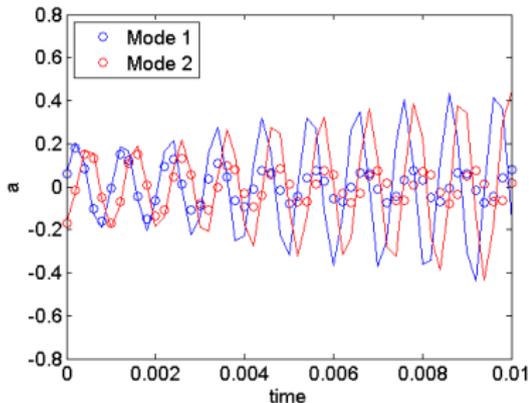
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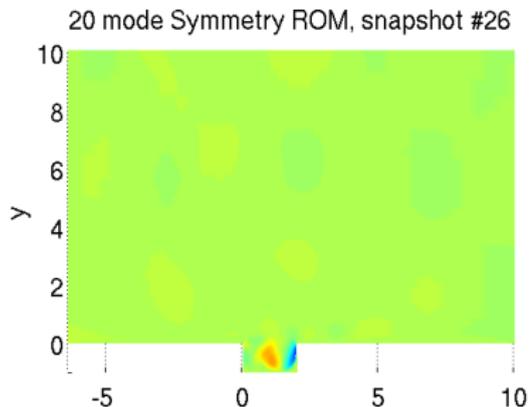
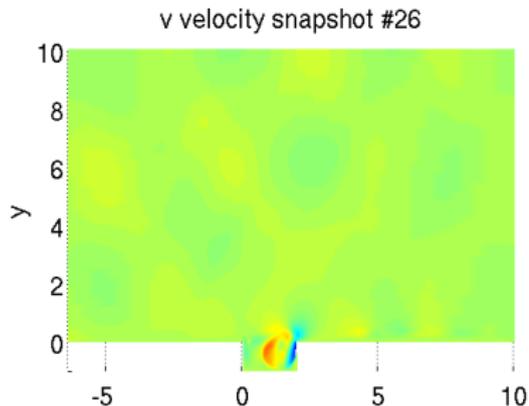
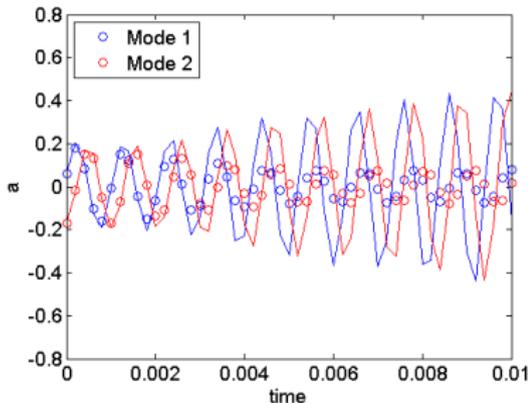
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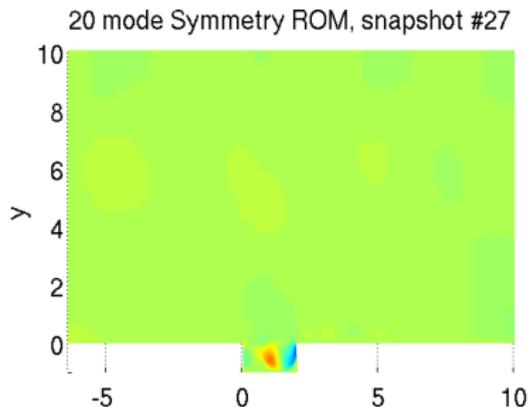
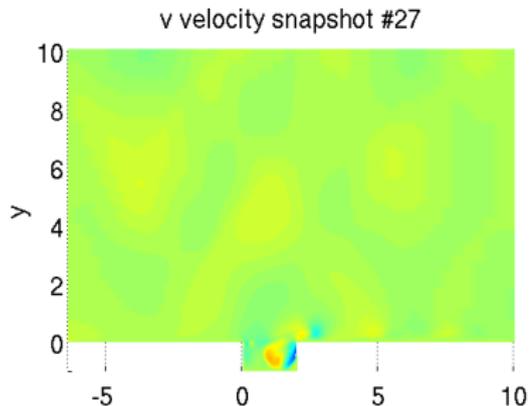
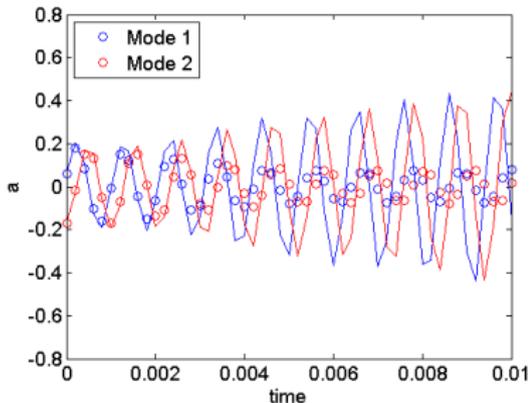
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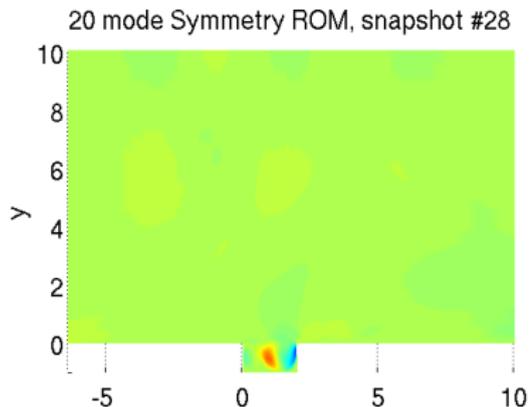
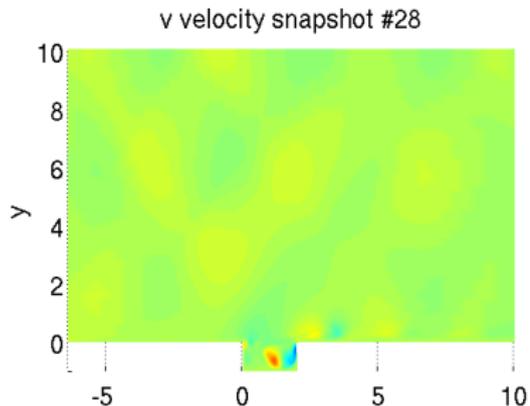
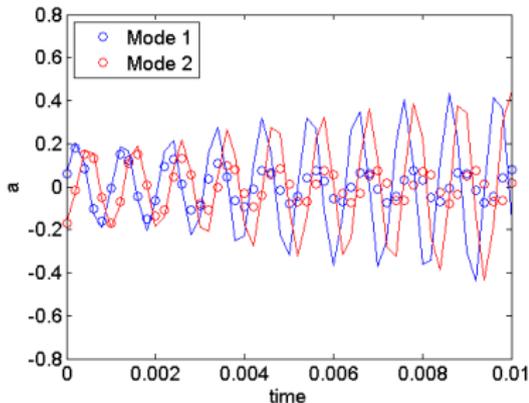
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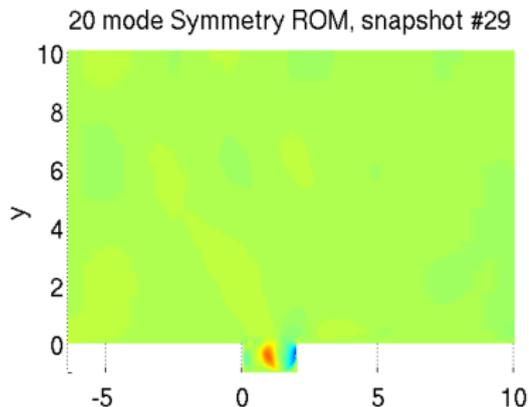
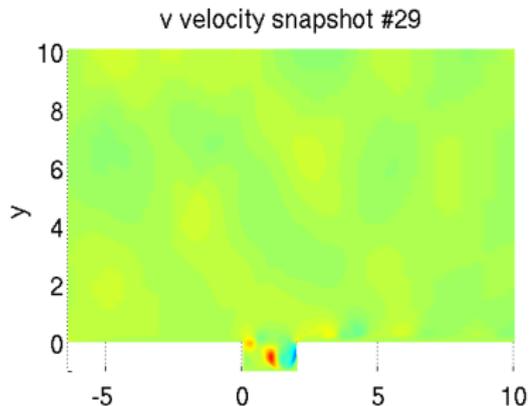
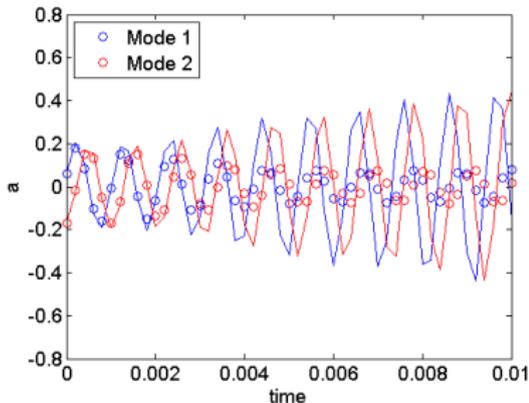
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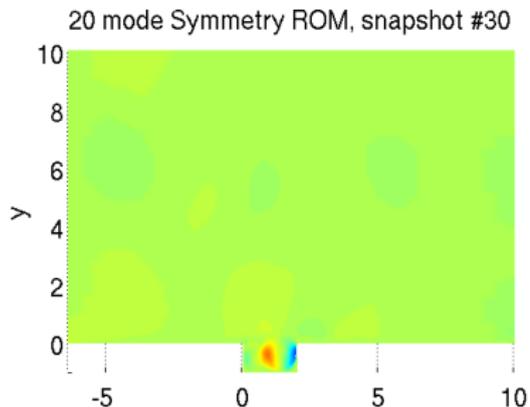
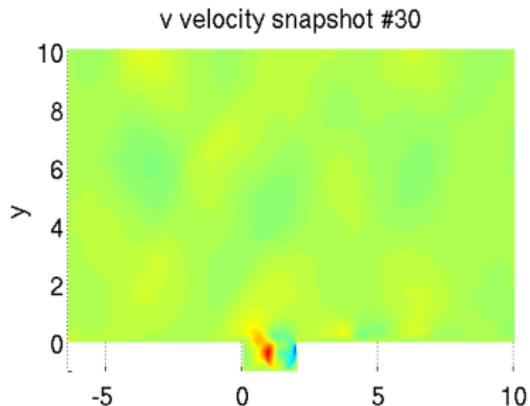
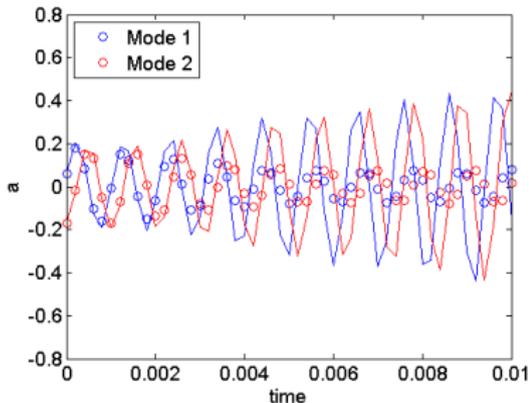
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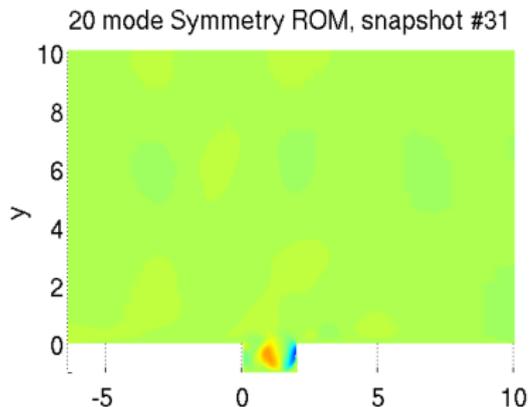
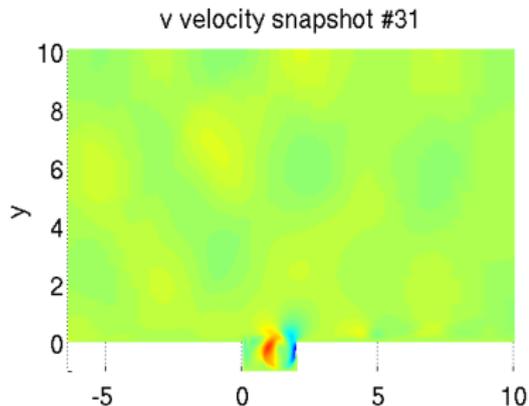
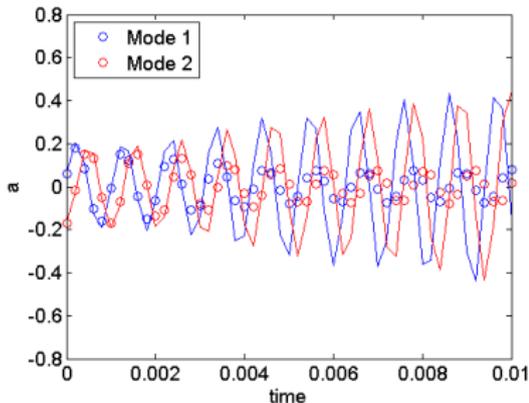
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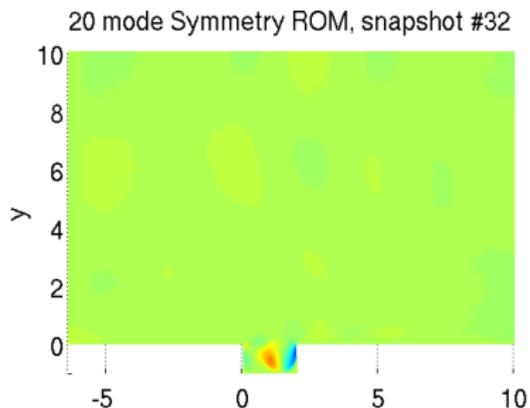
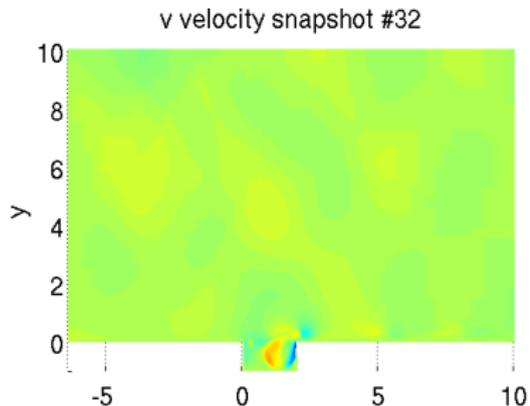
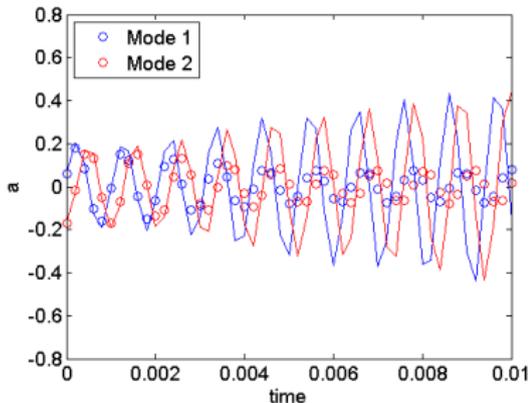
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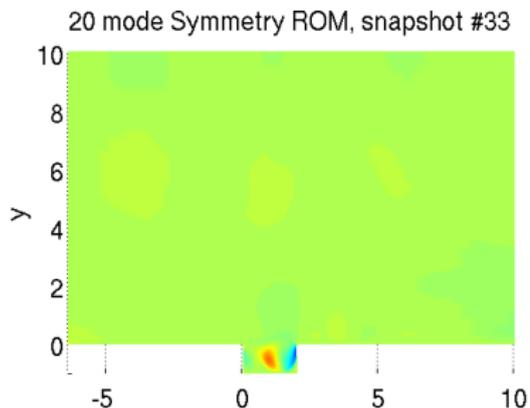
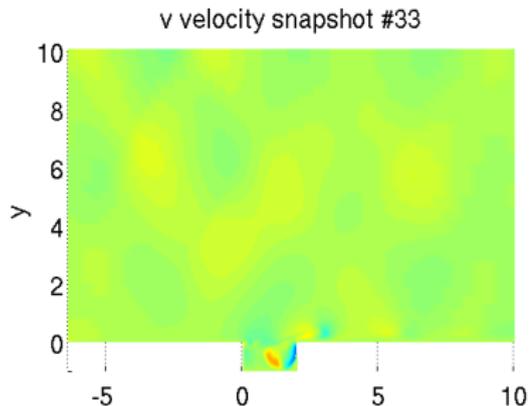
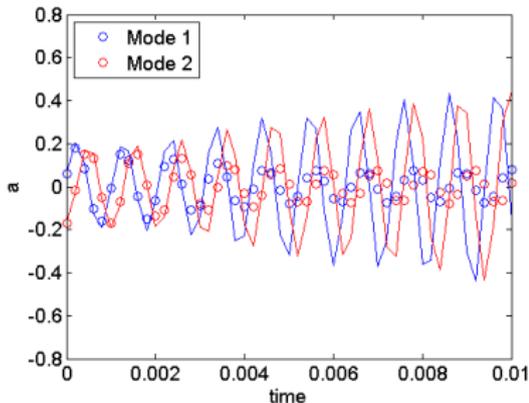
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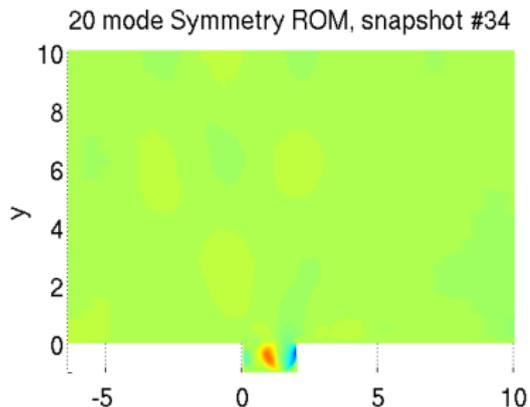
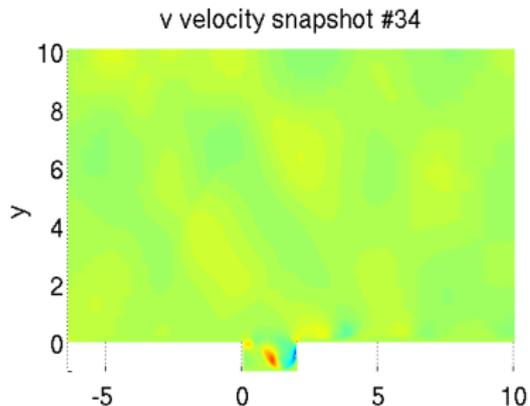
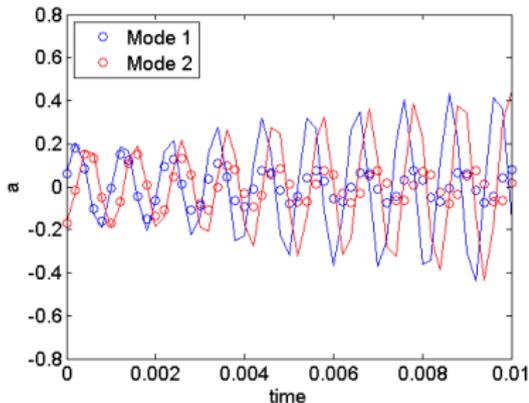
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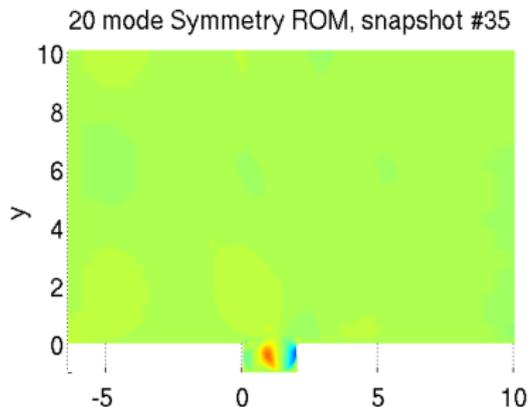
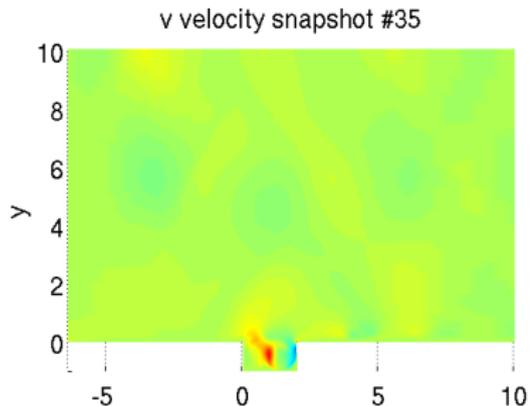
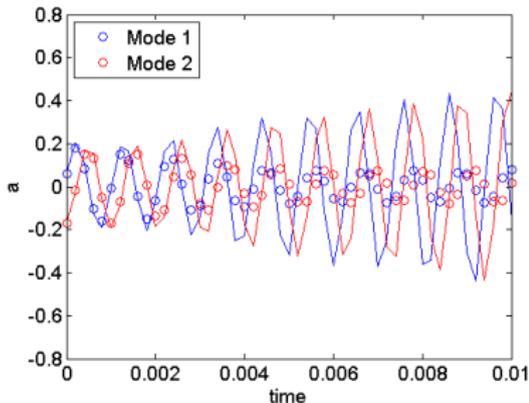
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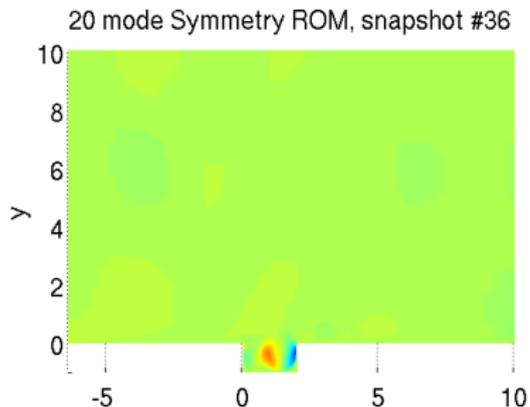
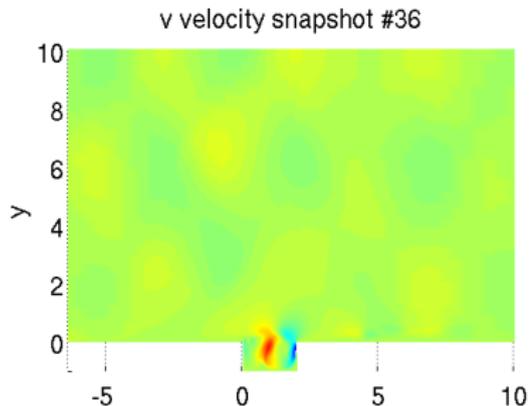
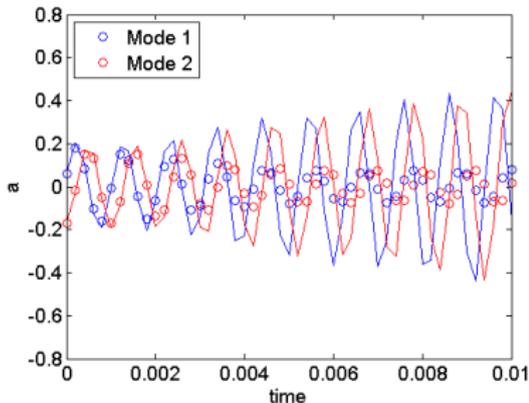
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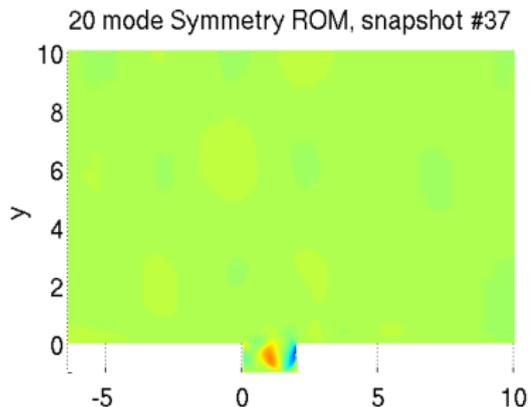
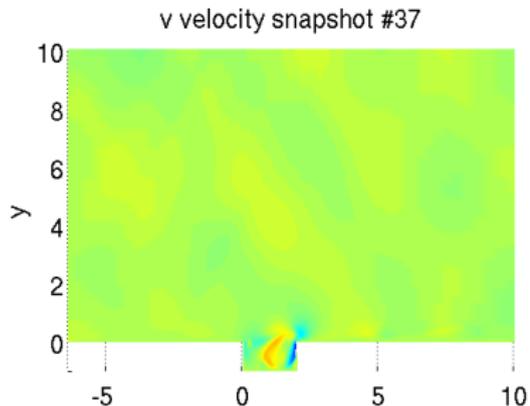
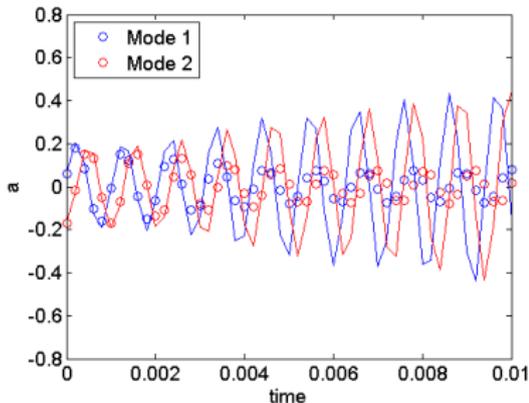
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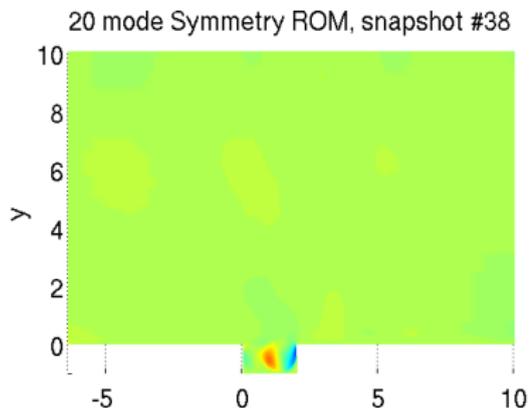
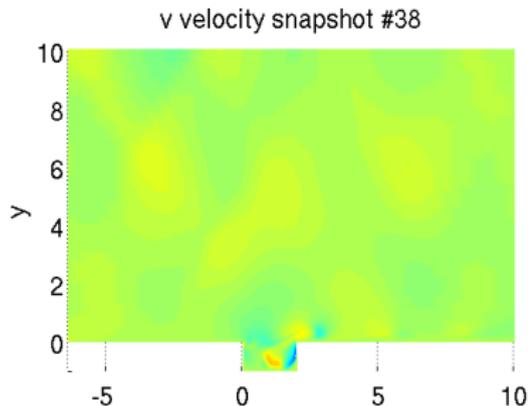
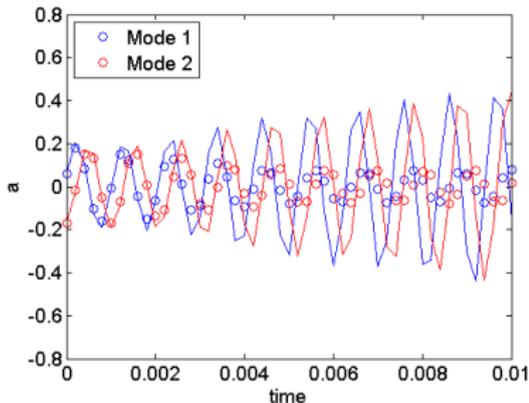
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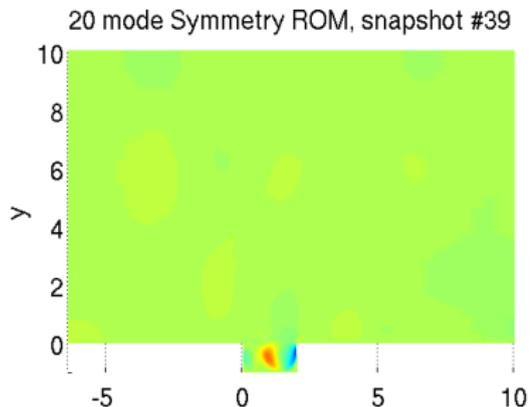
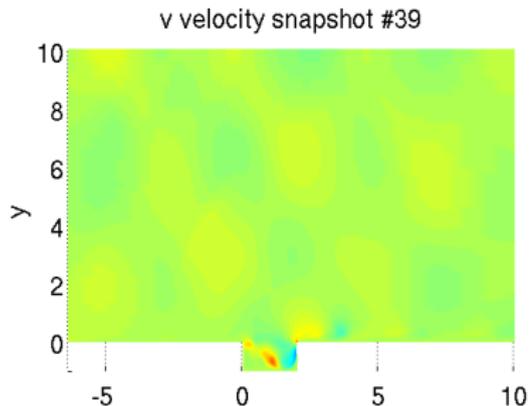
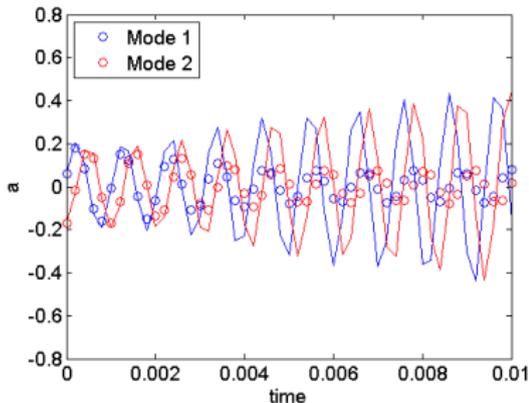
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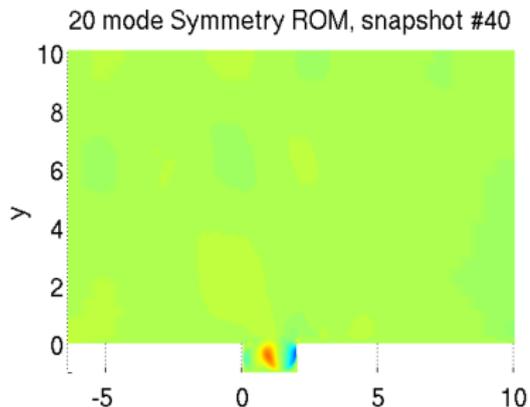
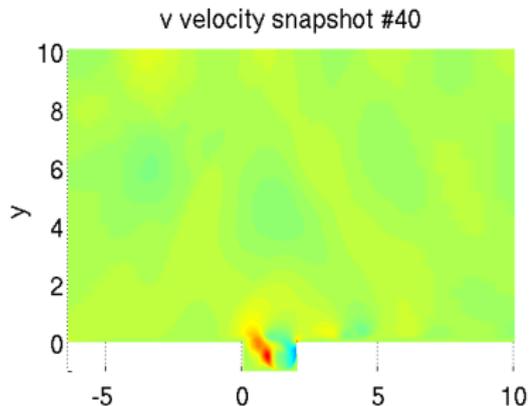
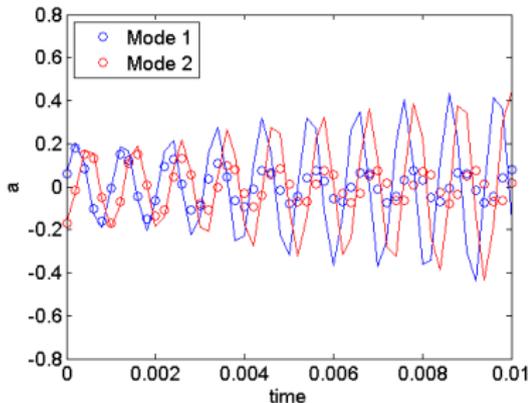
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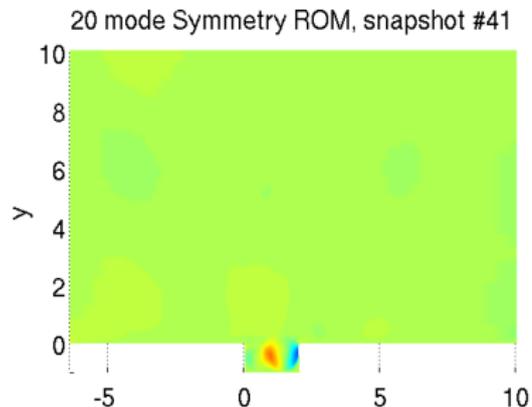
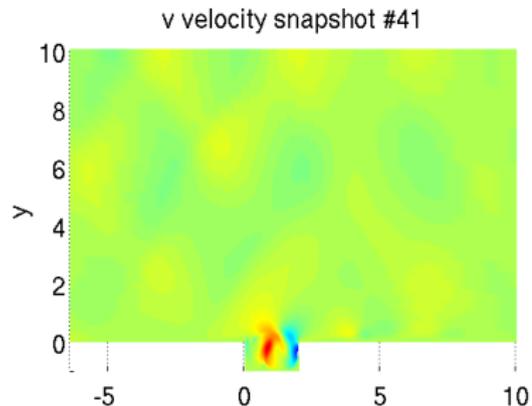
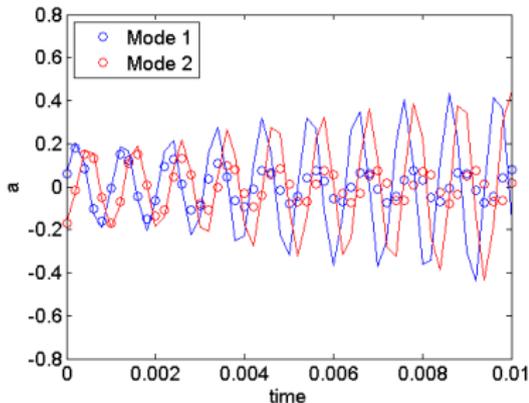
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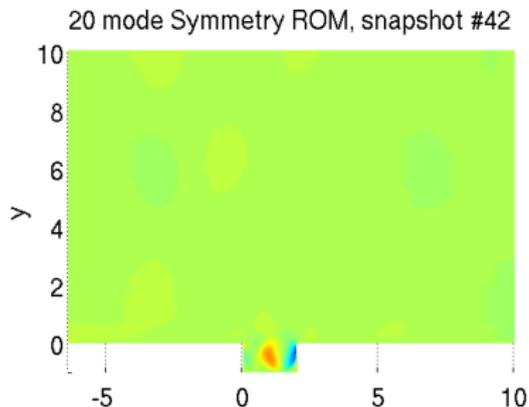
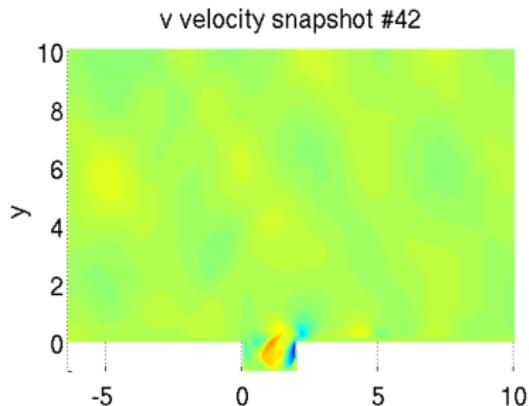
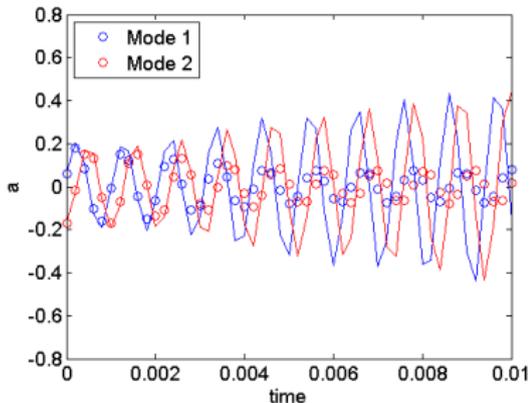
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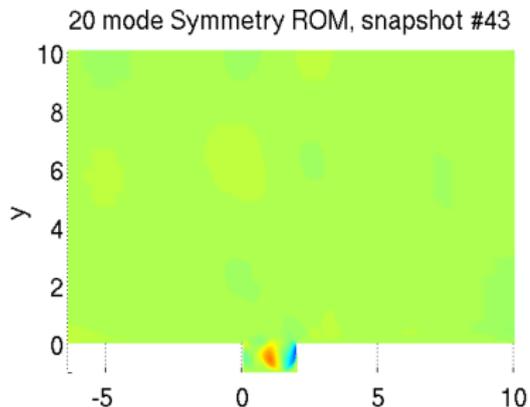
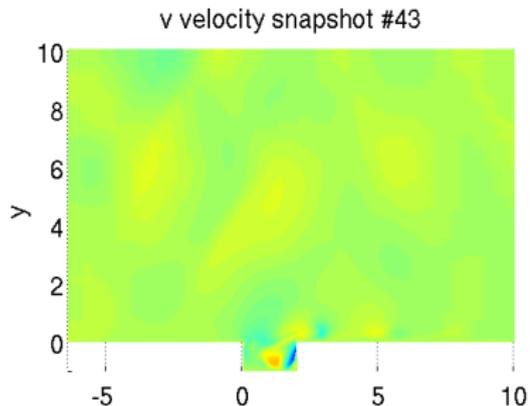
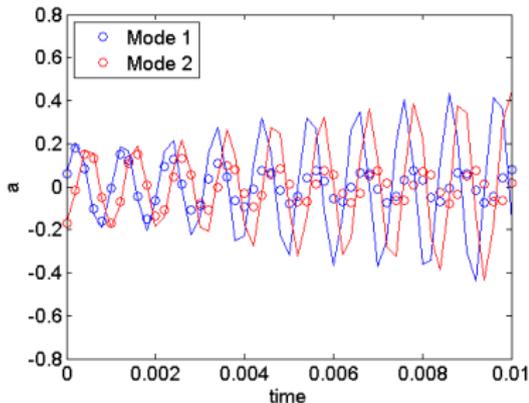
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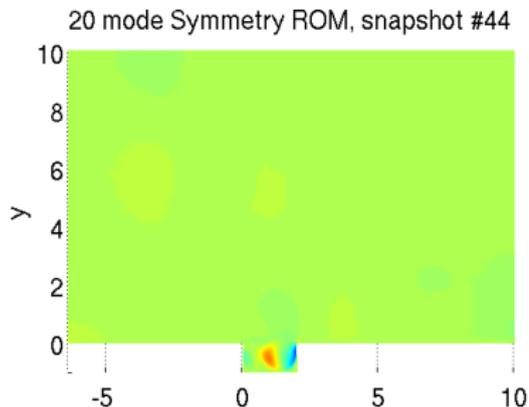
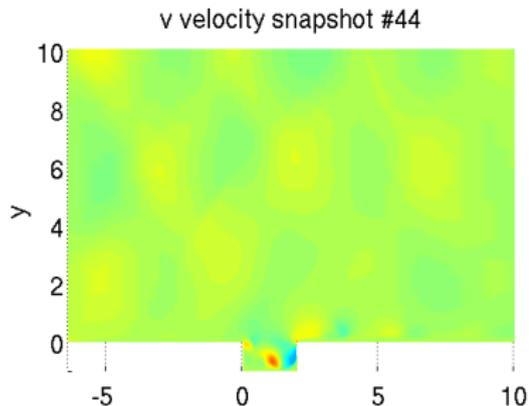
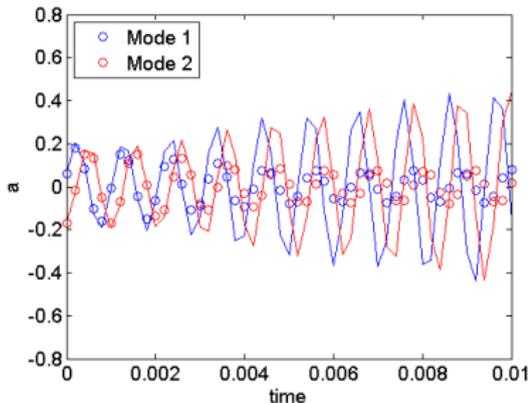
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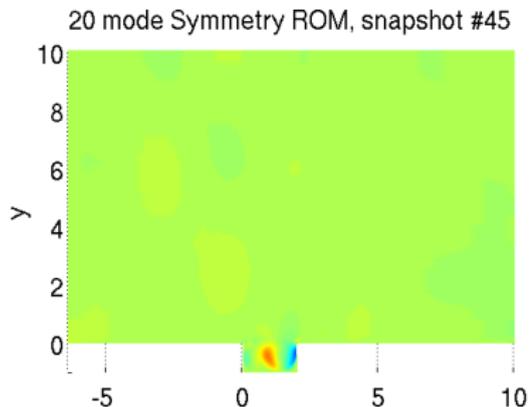
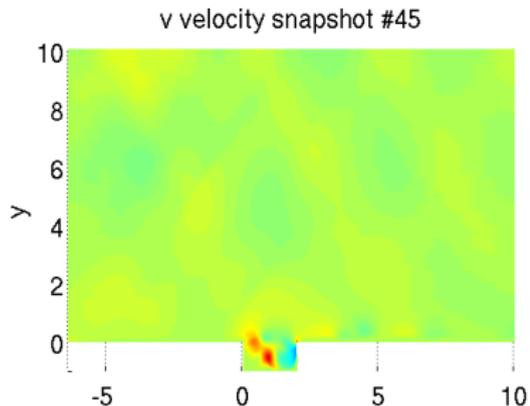
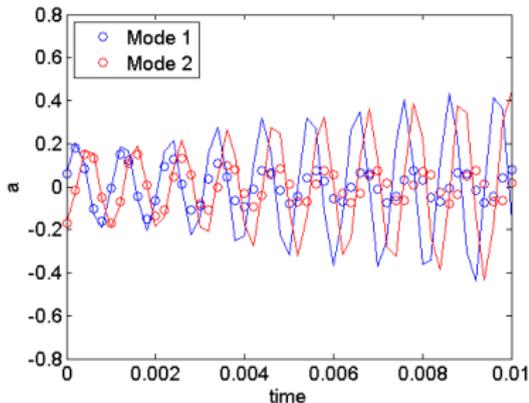
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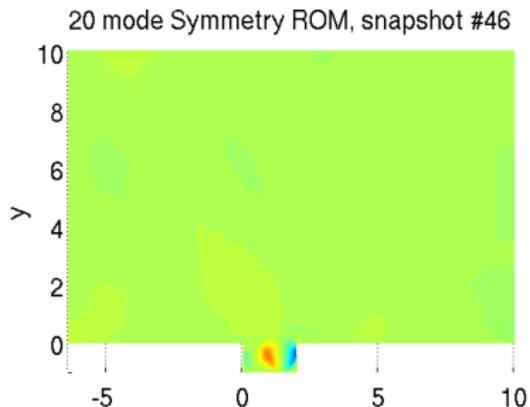
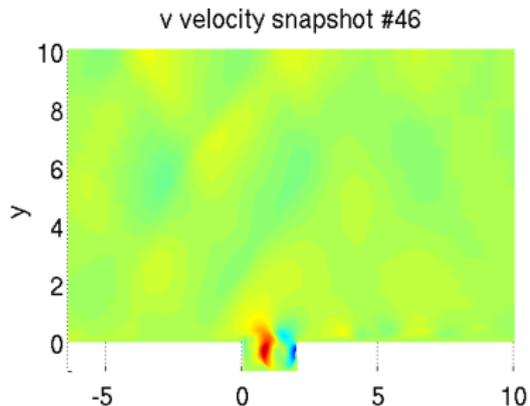
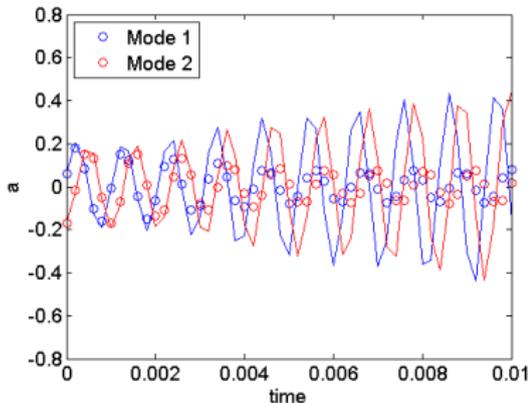
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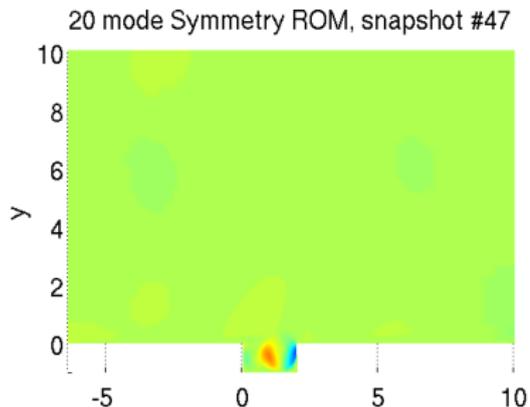
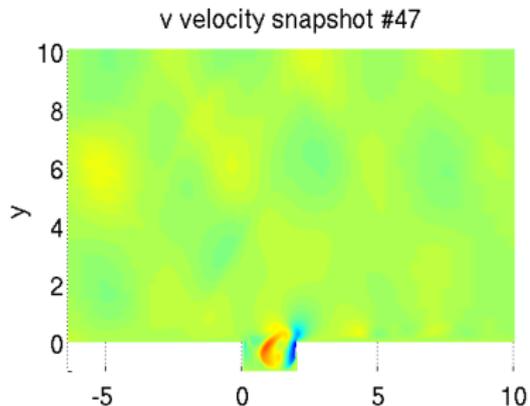
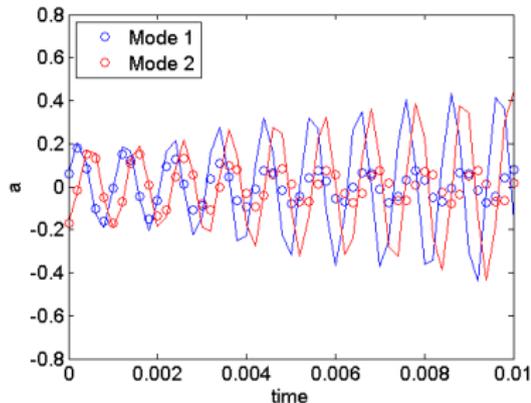
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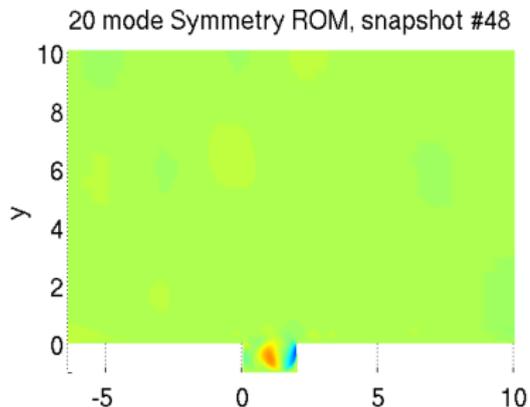
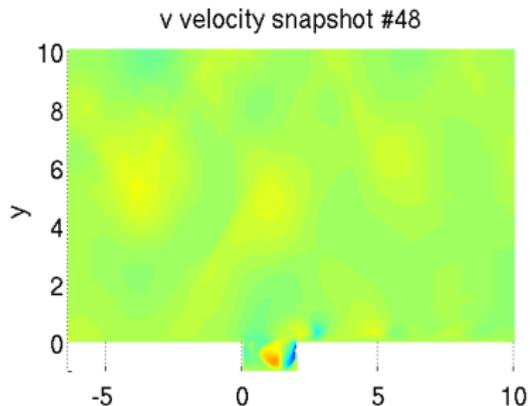
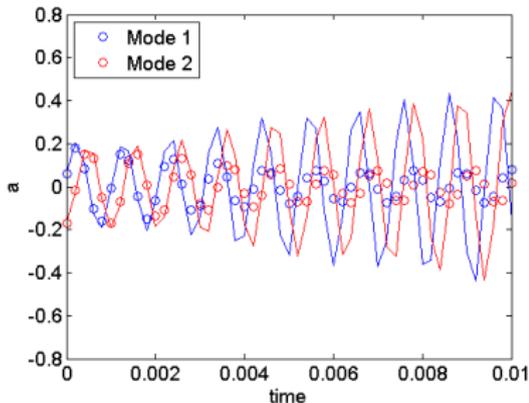
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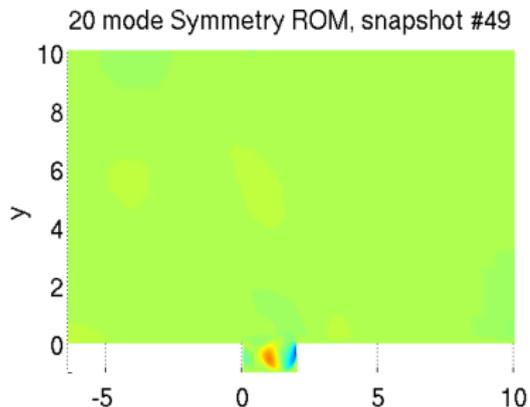
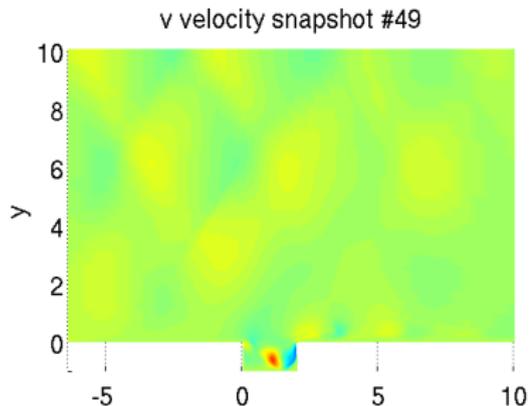
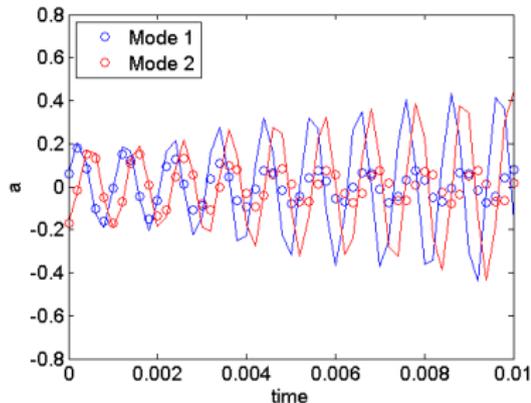
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  - $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Neglecting $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + \mathbf{A}_i(\bar{\mathbf{q}})\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} = \mathbf{F}$$

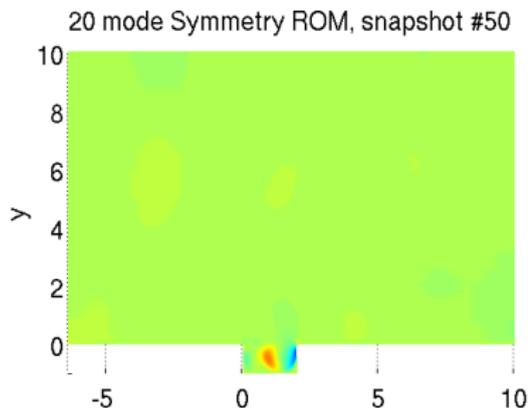
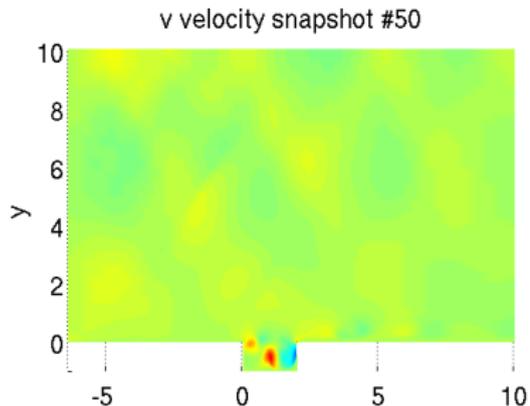
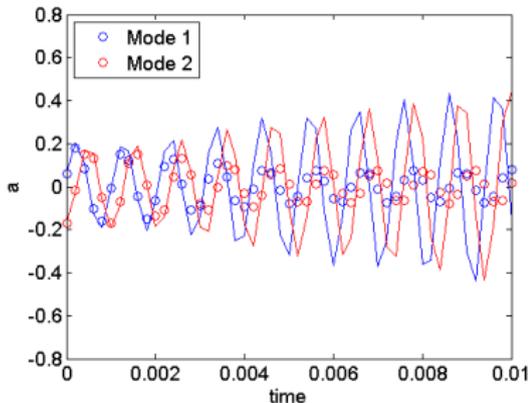
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Neglecting $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + \mathbf{A}_i(\bar{\mathbf{q}})\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} = \mathbf{F}$$

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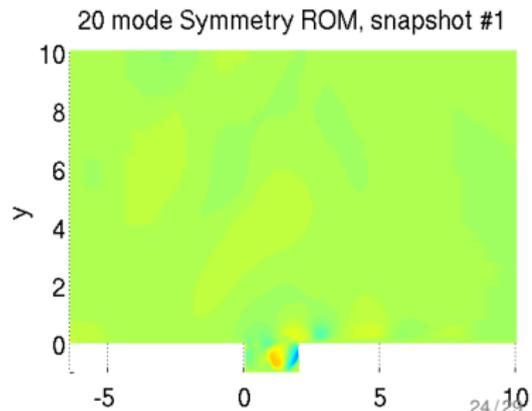
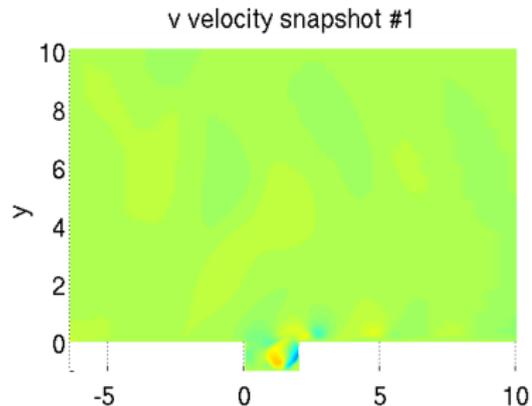
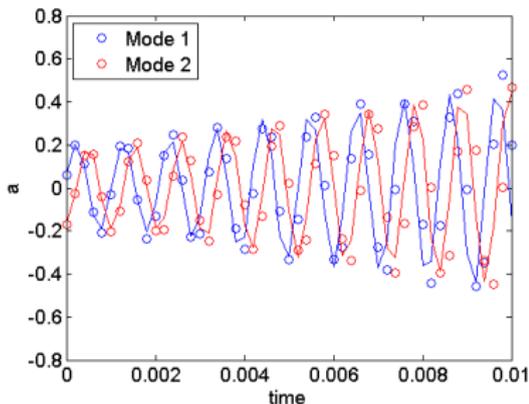


# ROM based on Linearized Navier-Stokes Neglecting $\nabla\bar{q}$ Terms

# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{q}) - \mathbf{K}_i^{vw}(\nabla\bar{q})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{q})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{q})\mathbf{q}' = \mathbf{F}$$

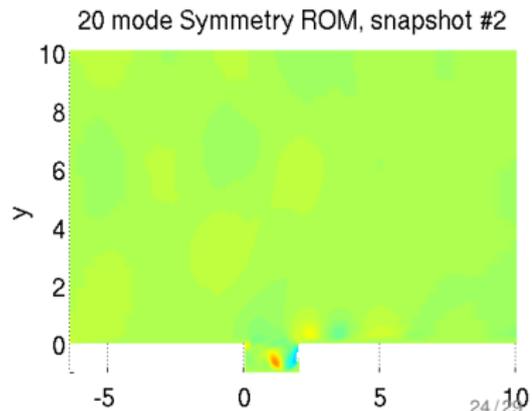
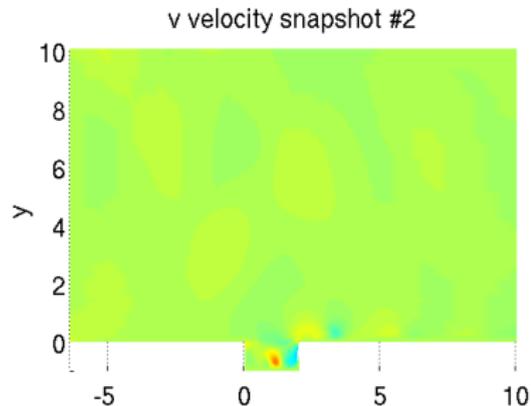
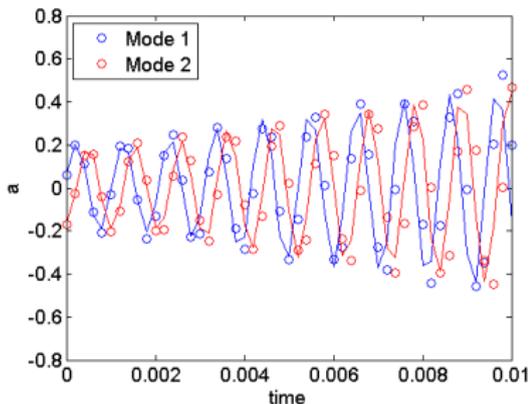
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

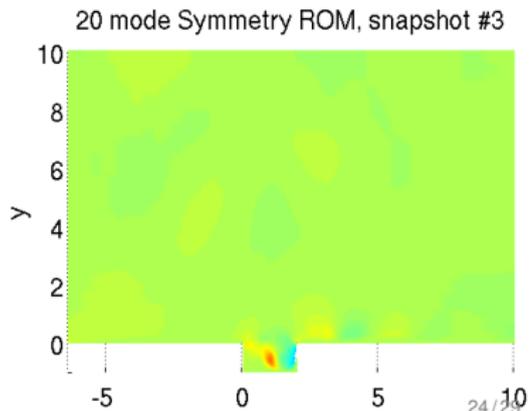
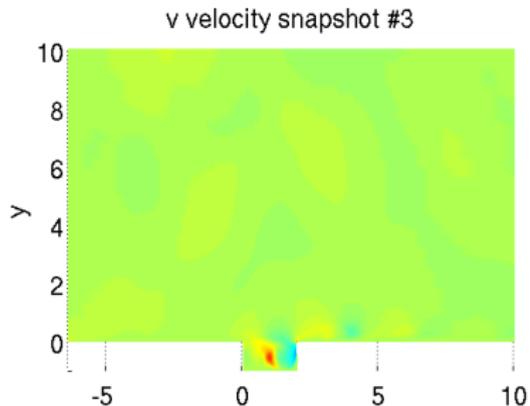
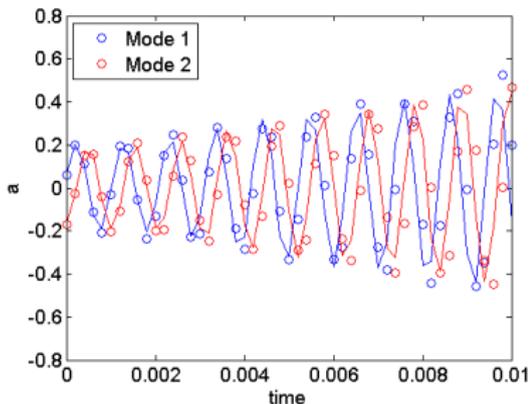
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

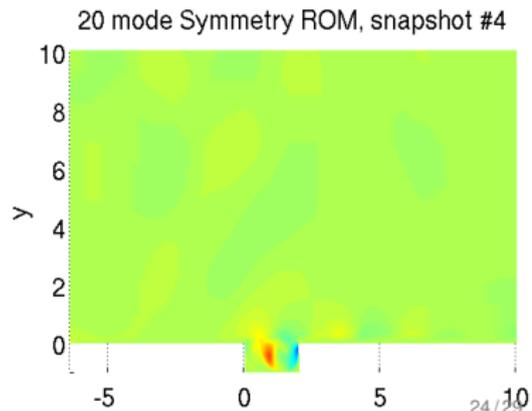
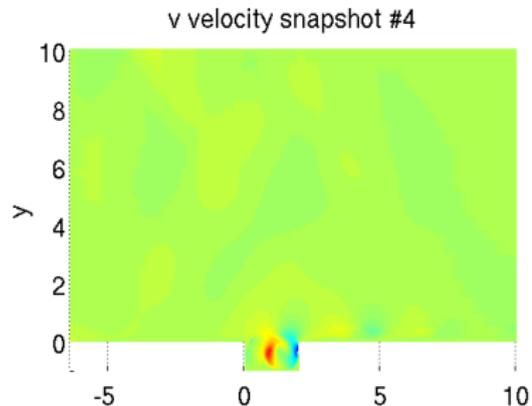
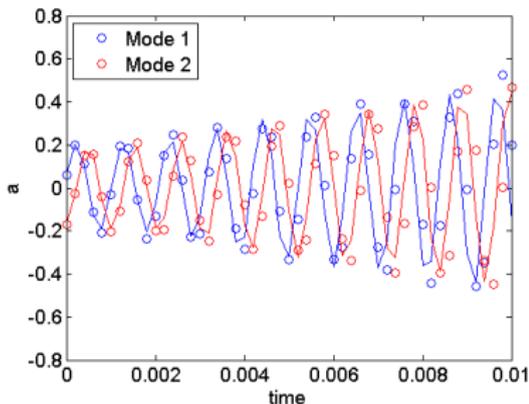
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

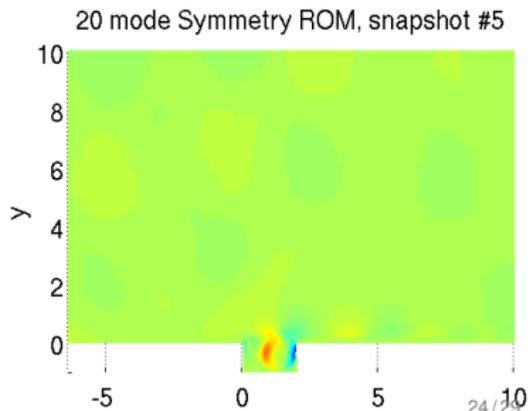
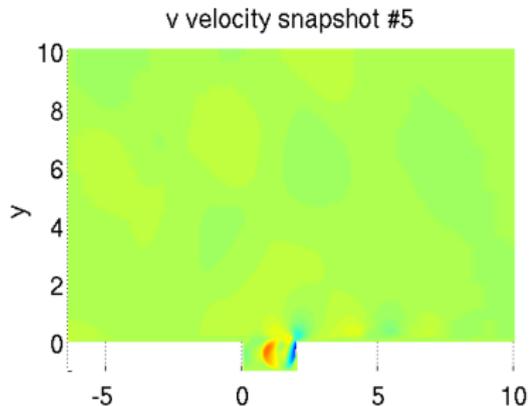
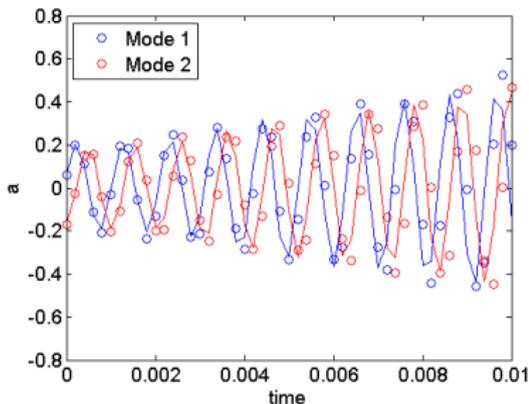
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

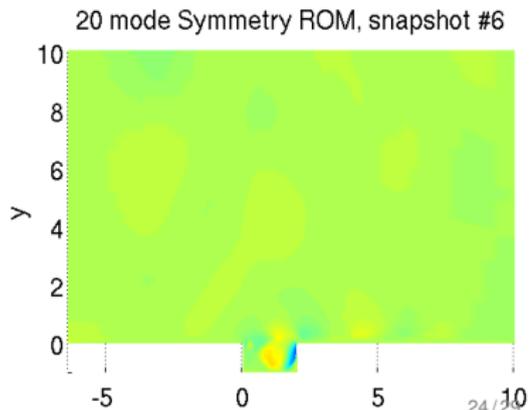
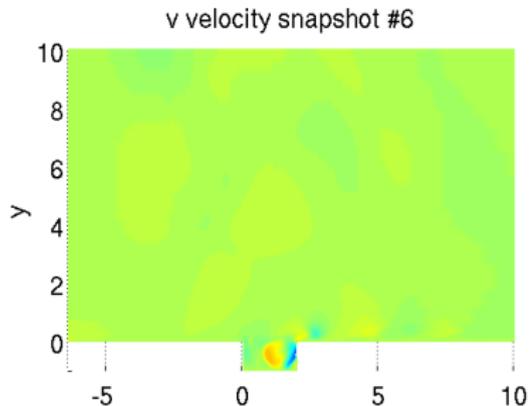
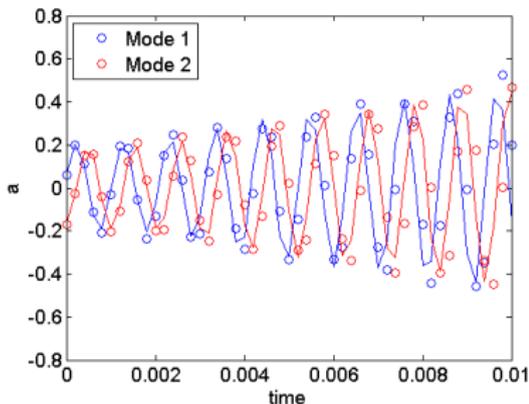
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

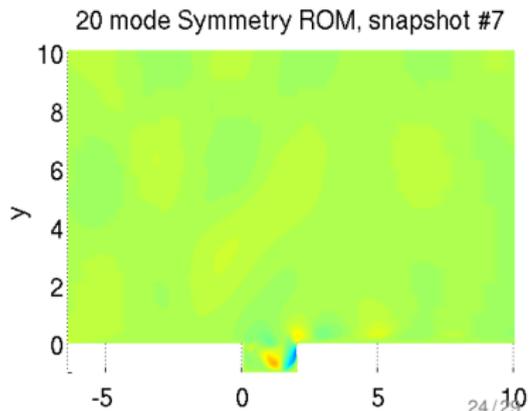
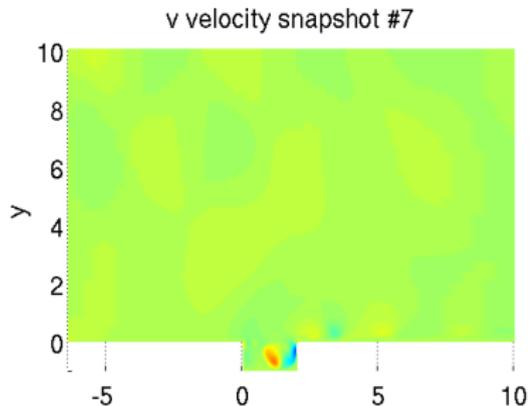
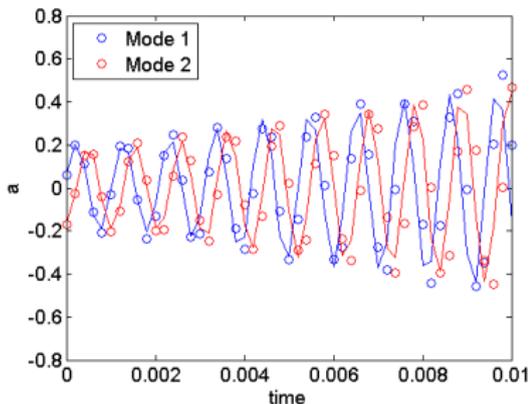
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

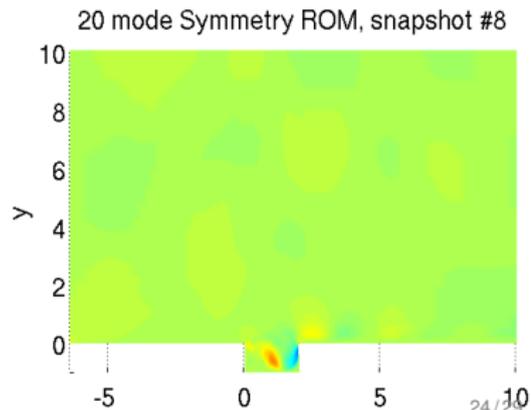
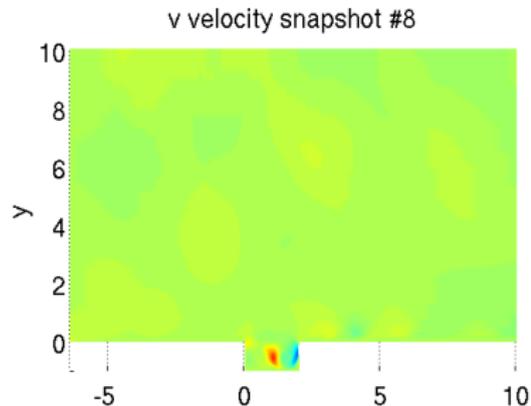
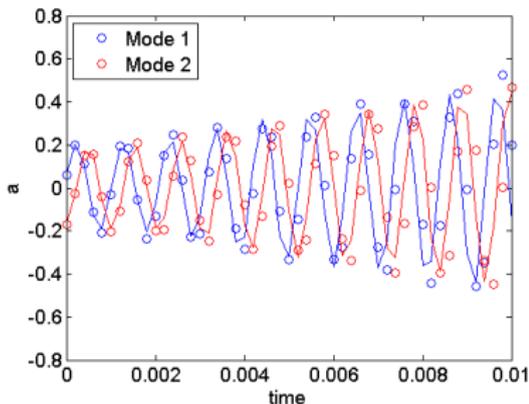
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

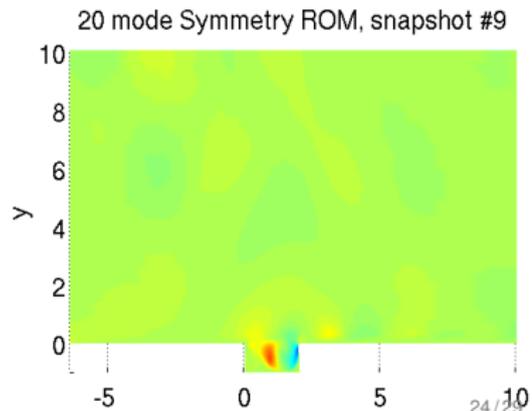
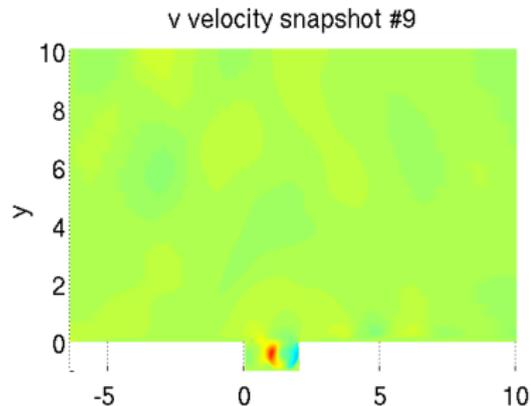
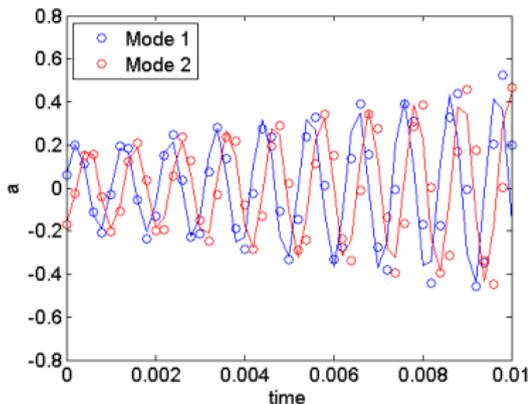
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

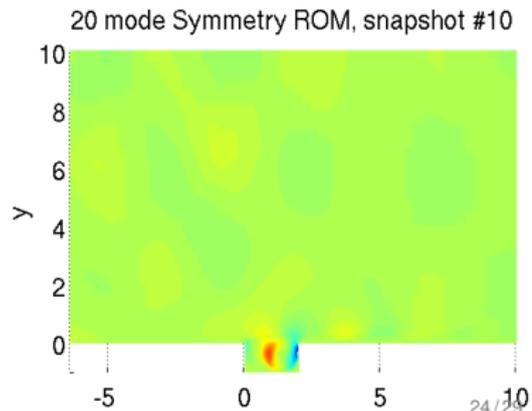
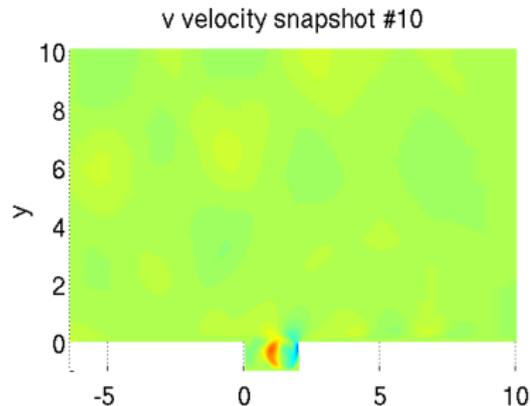
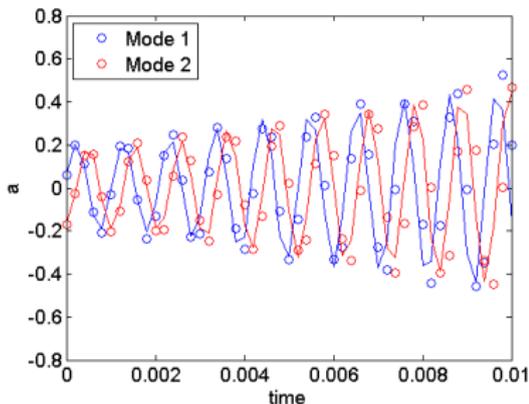
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

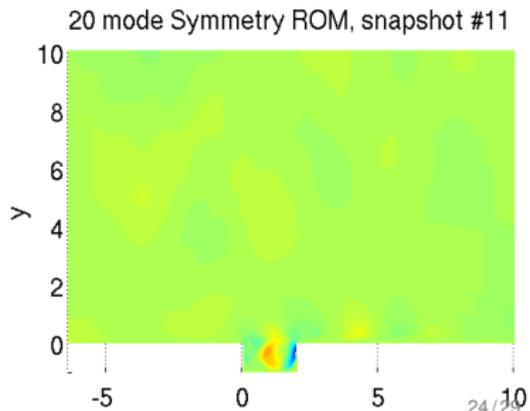
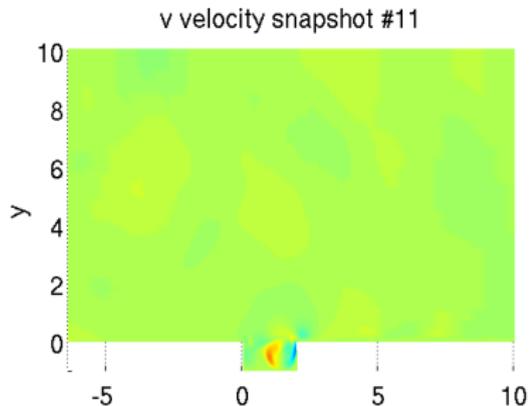
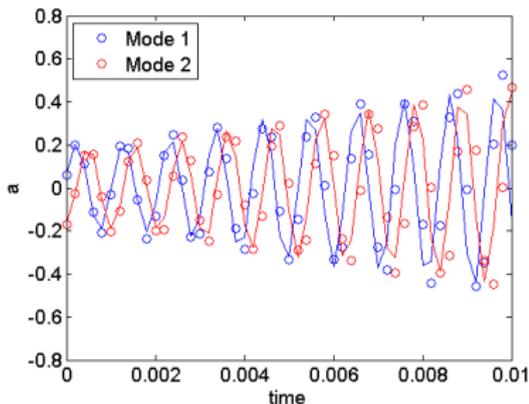
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

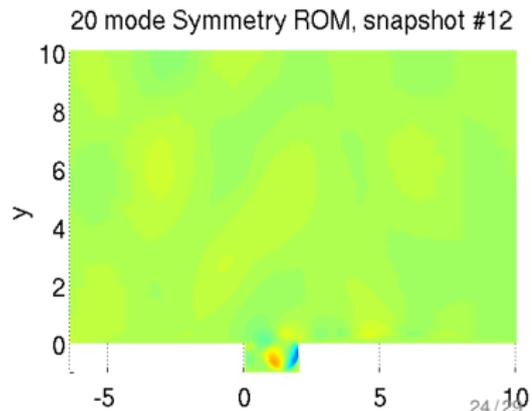
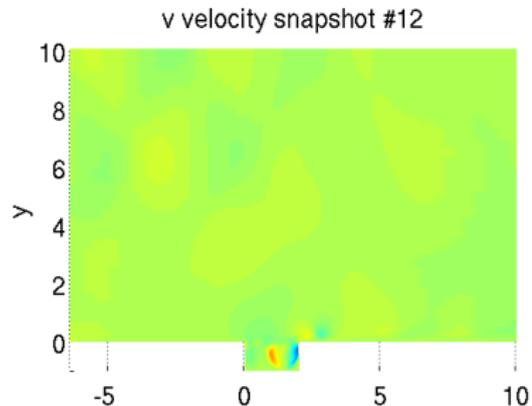
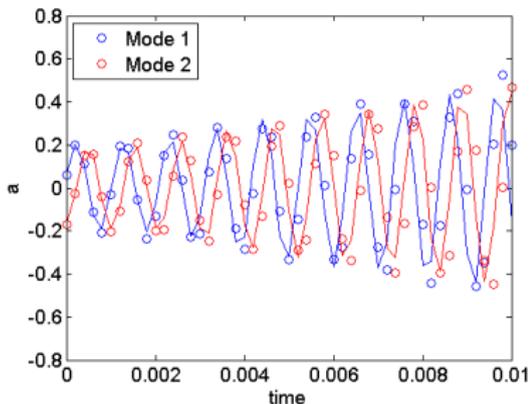
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

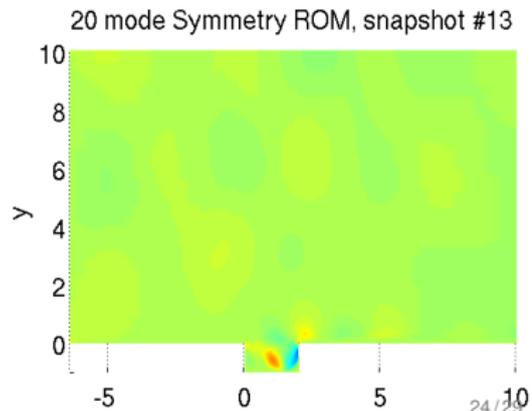
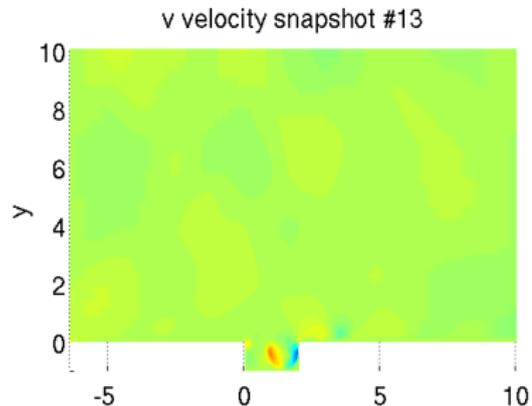
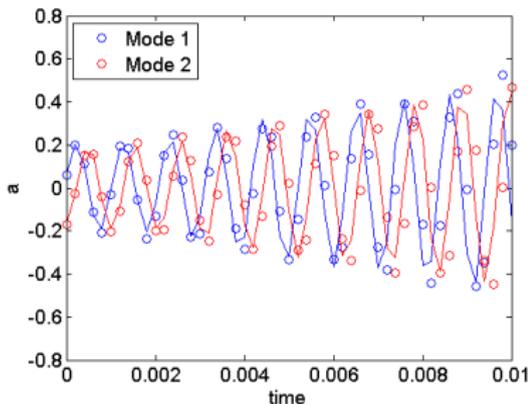
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

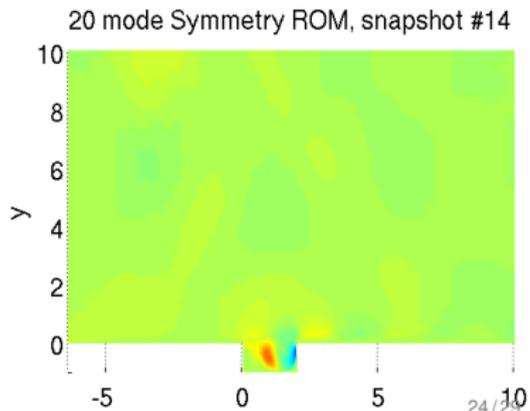
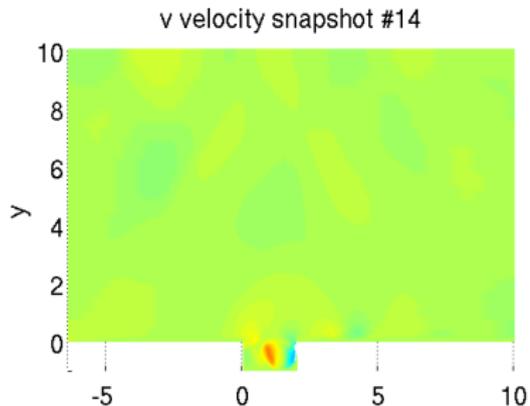
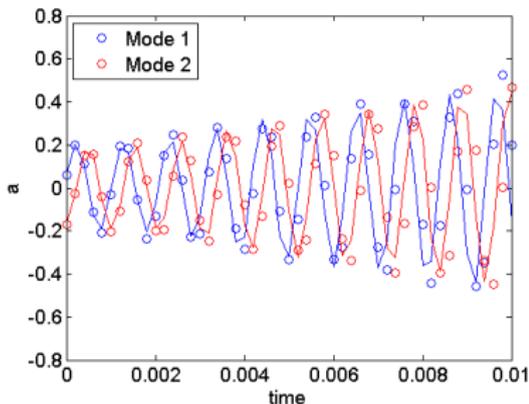
- Figure below shows:
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- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

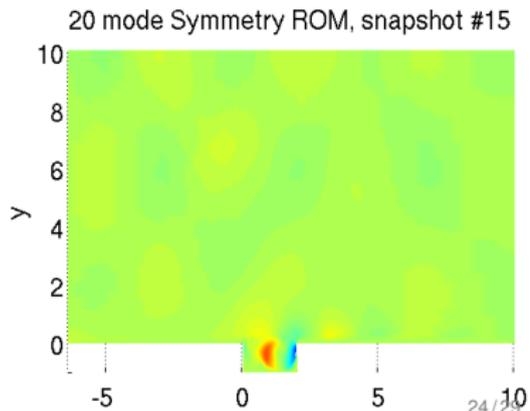
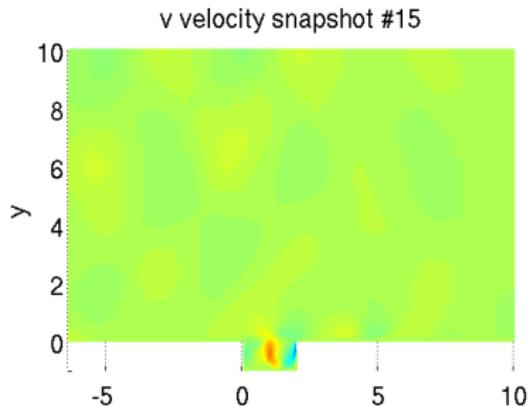
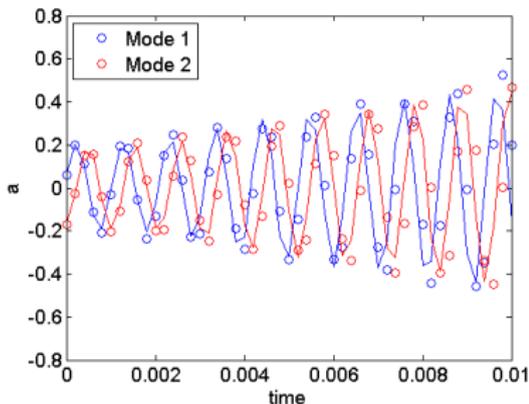
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

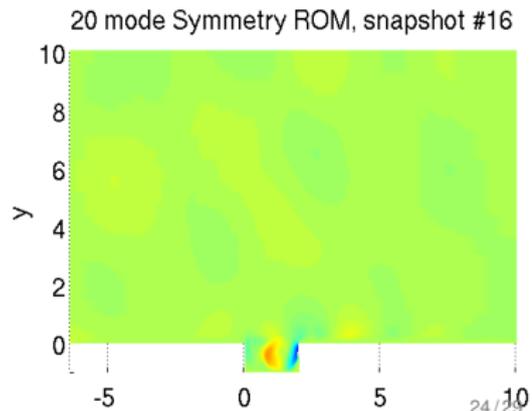
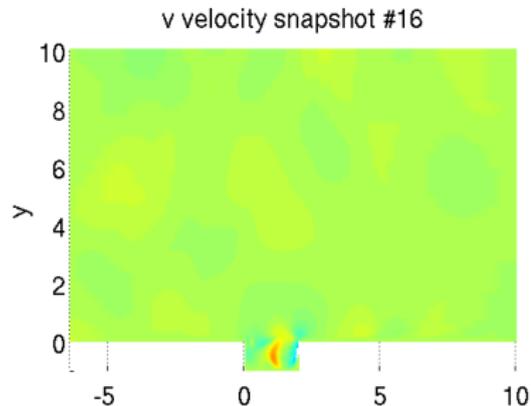
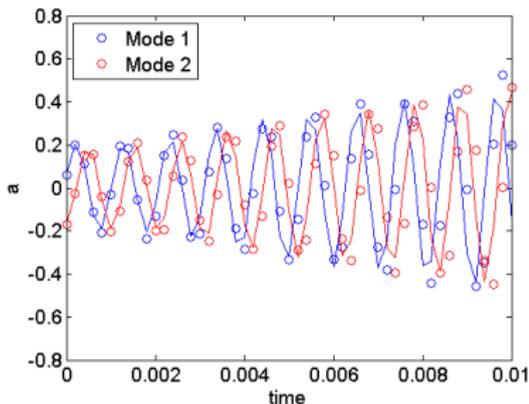
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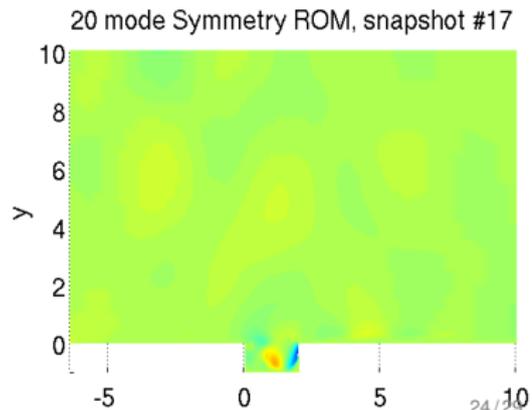
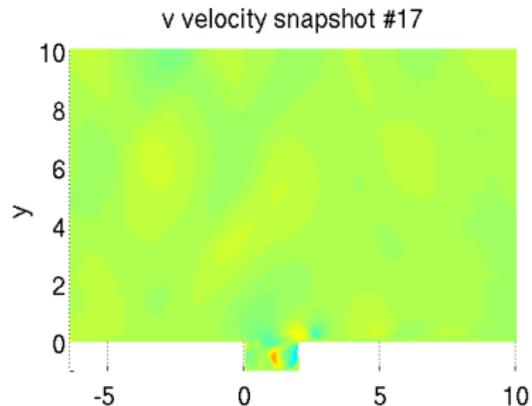
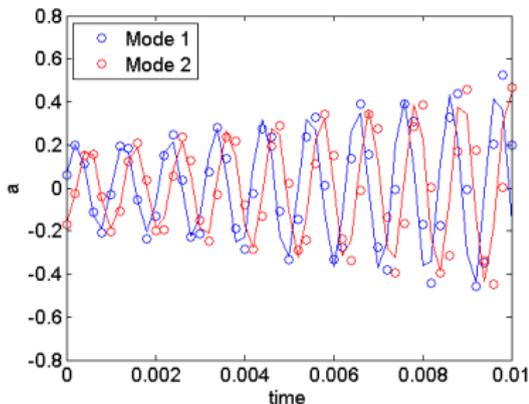
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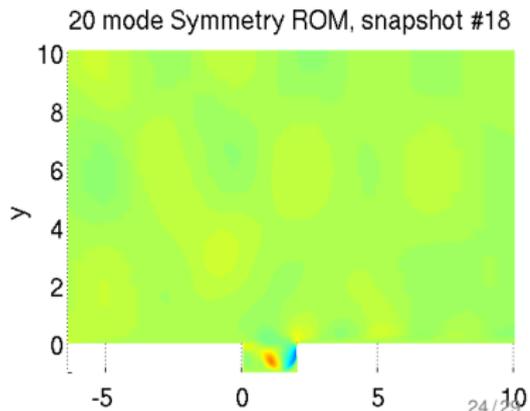
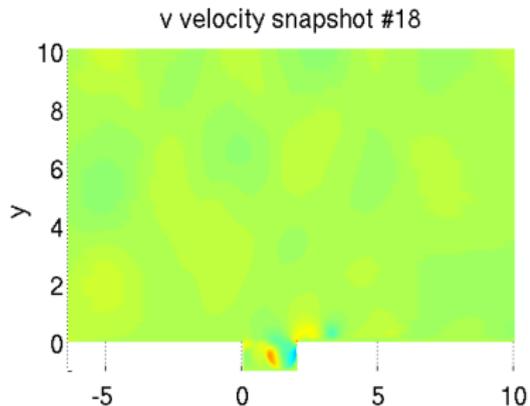
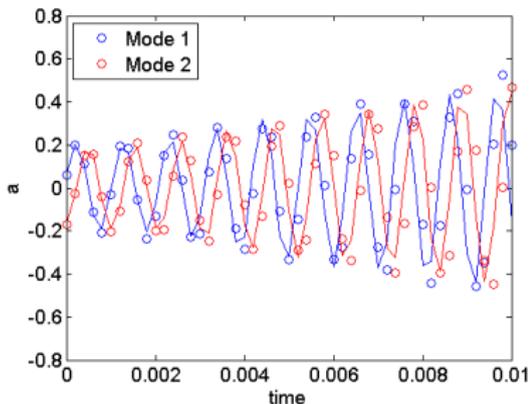
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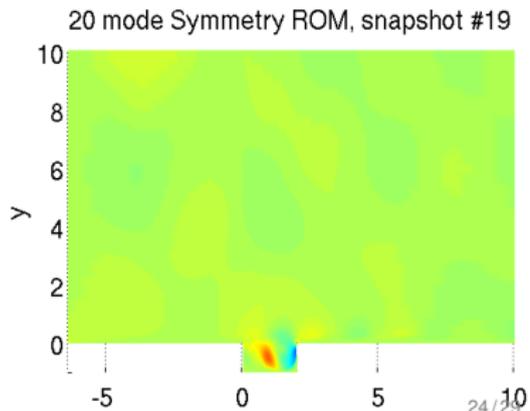
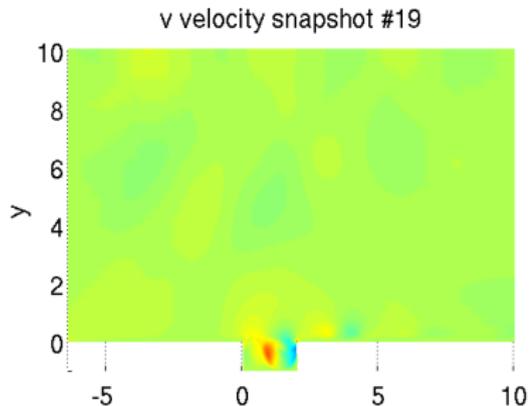
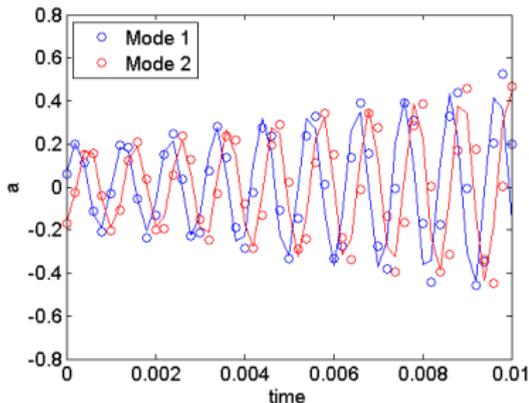
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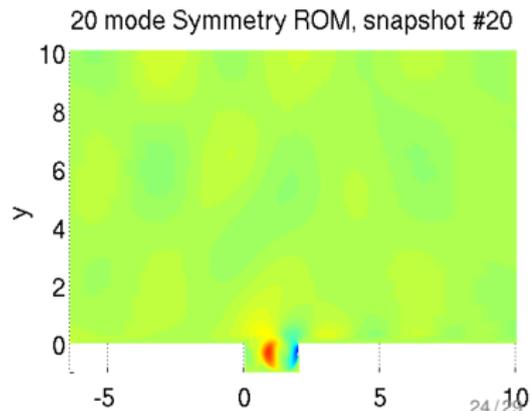
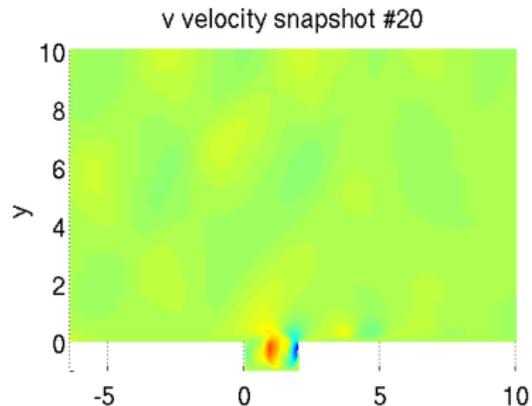
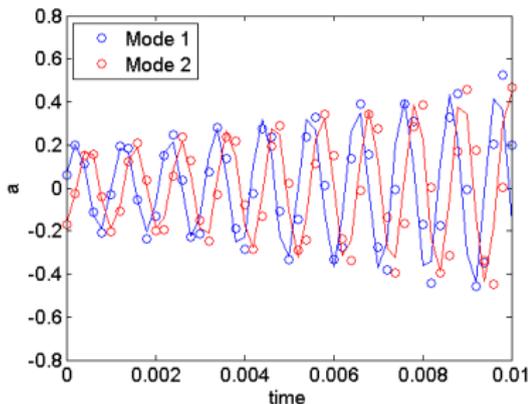
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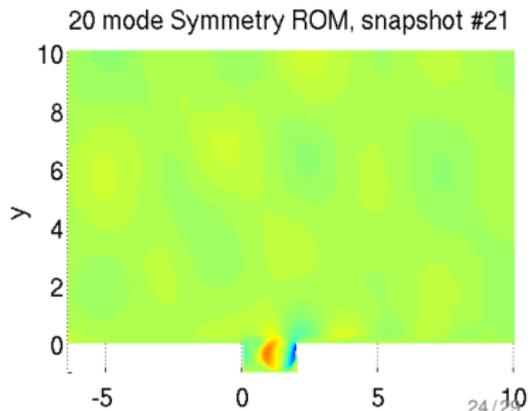
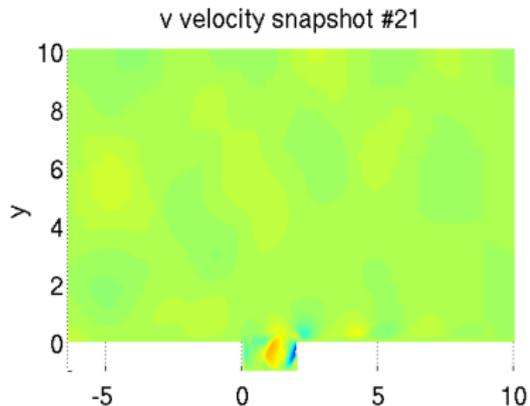
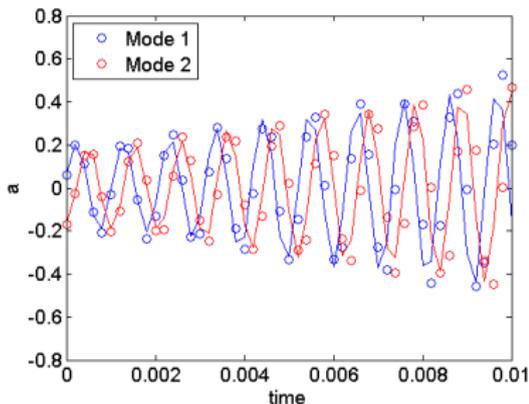
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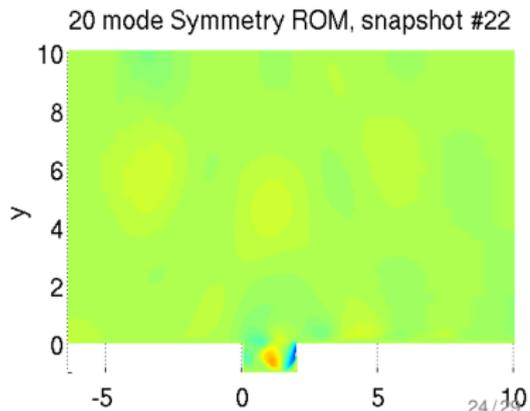
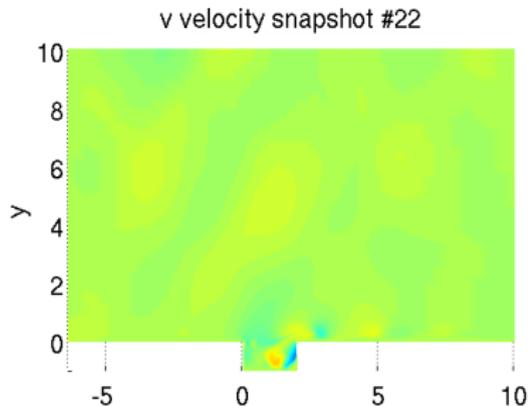
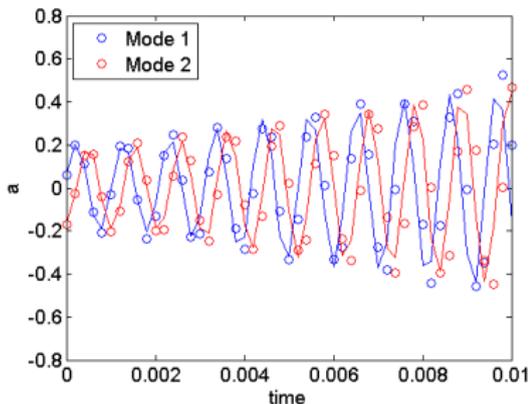
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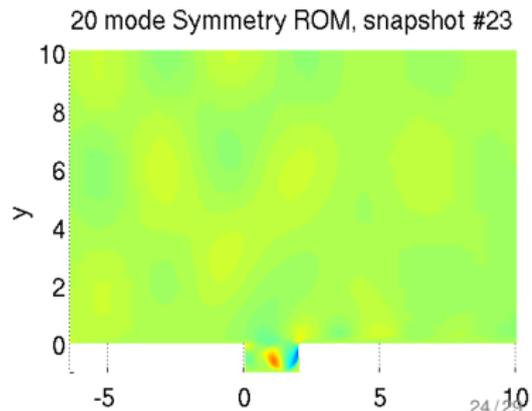
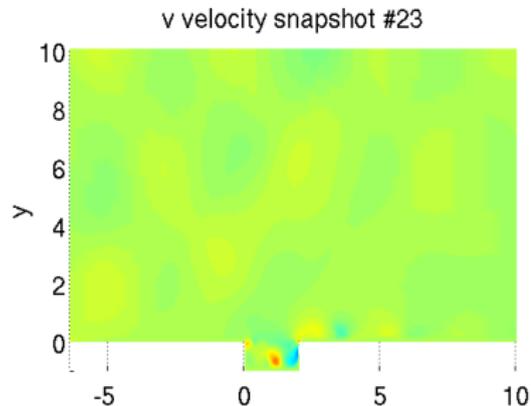
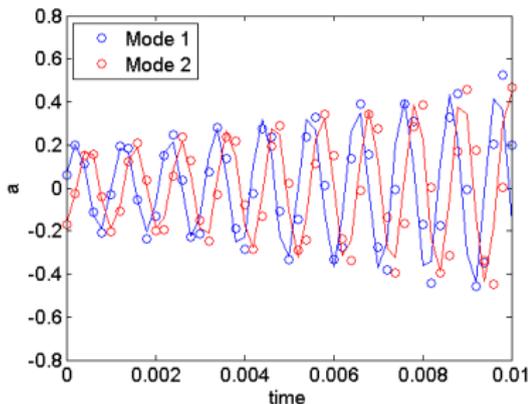
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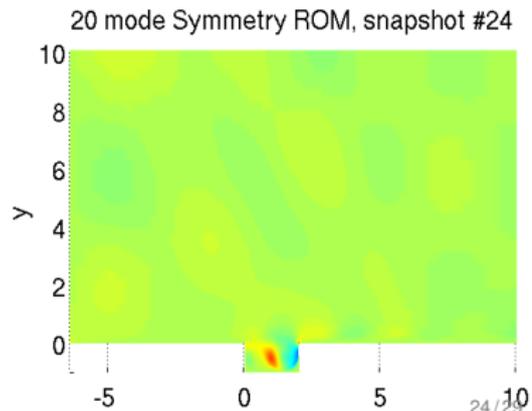
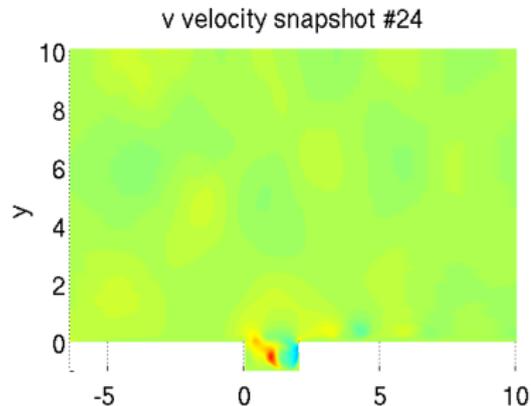
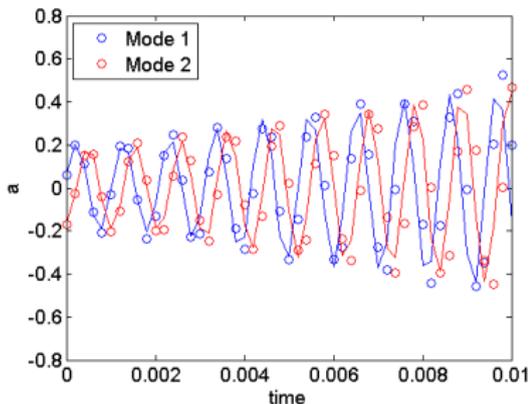
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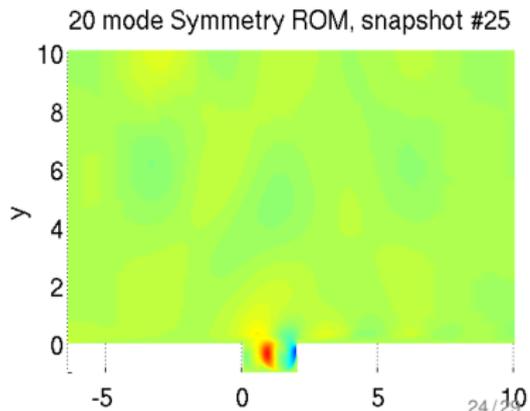
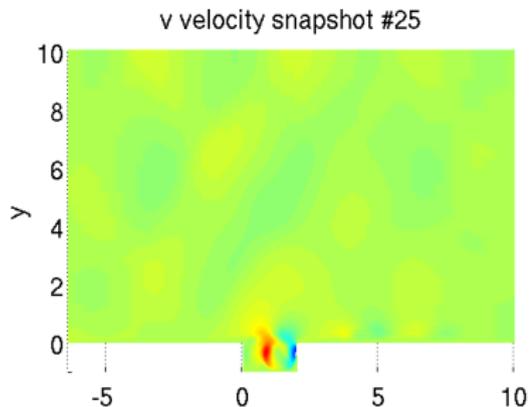
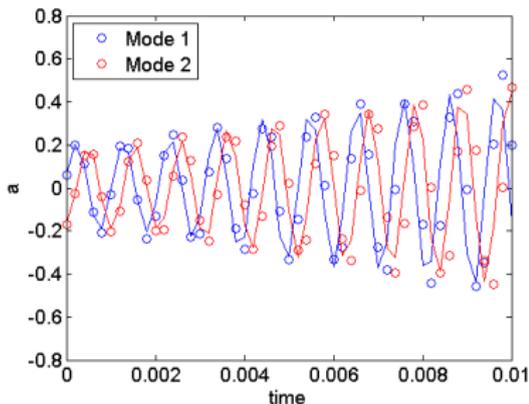
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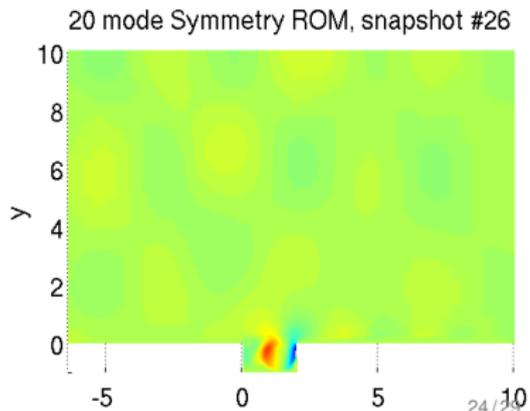
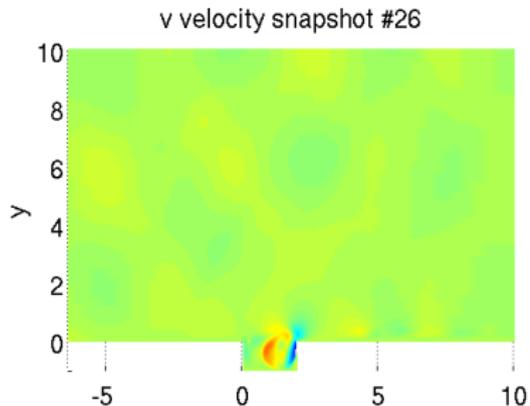
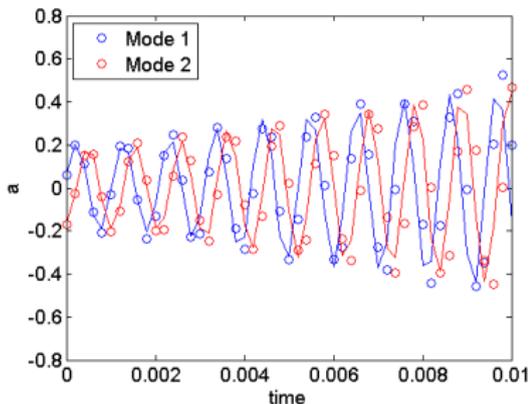
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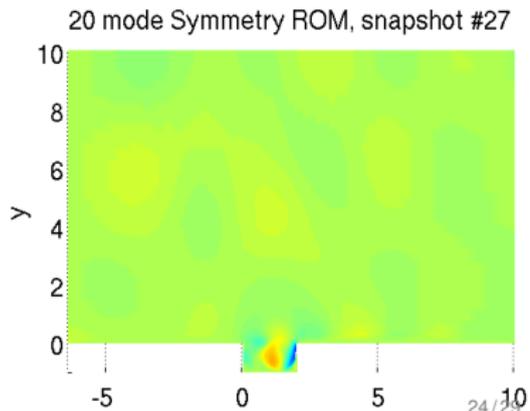
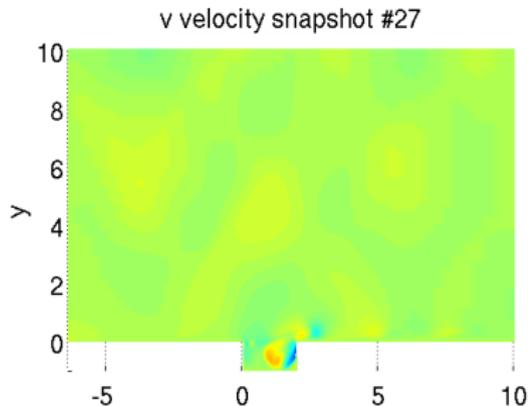
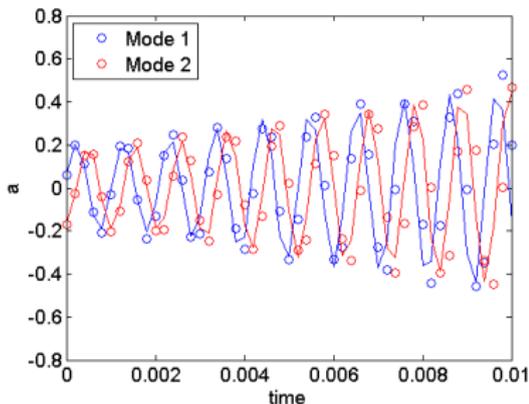
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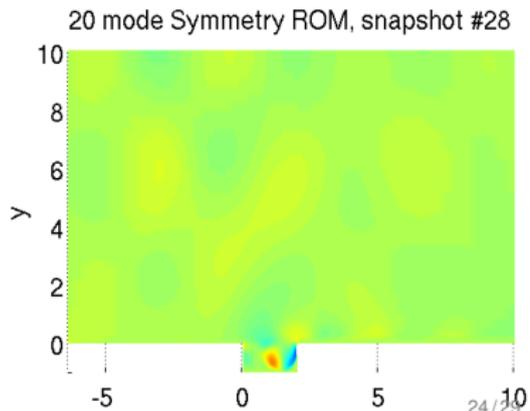
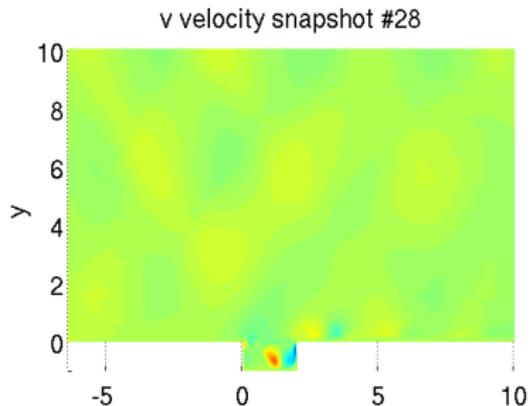
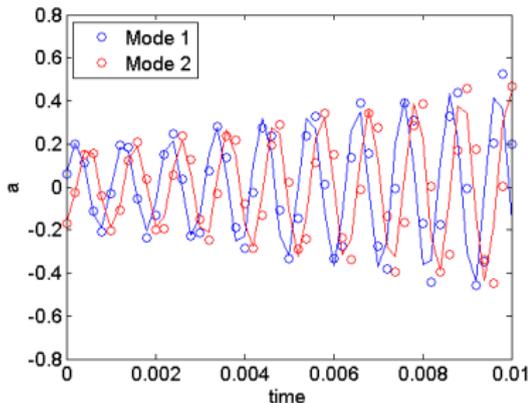
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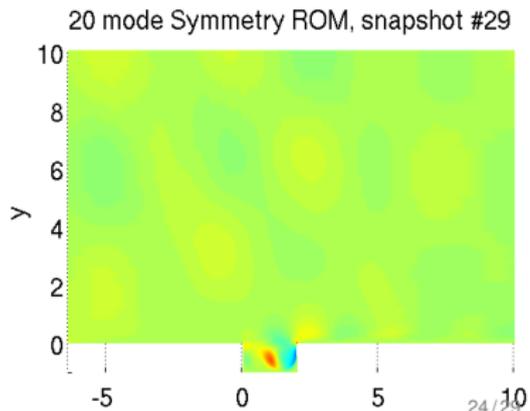
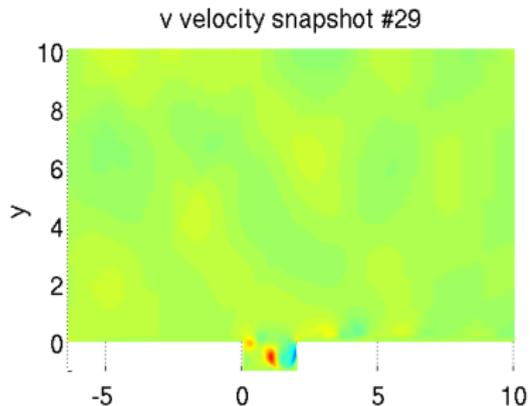
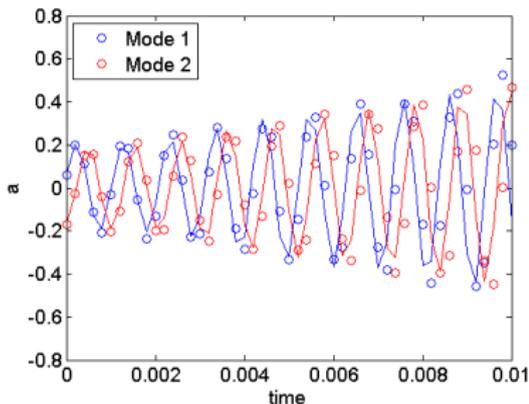
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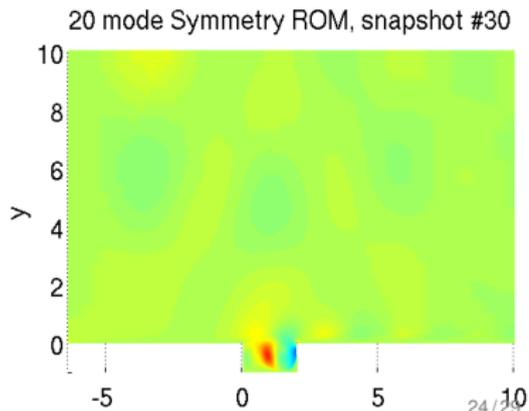
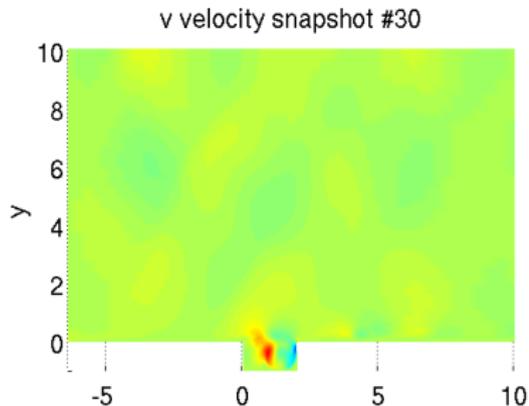
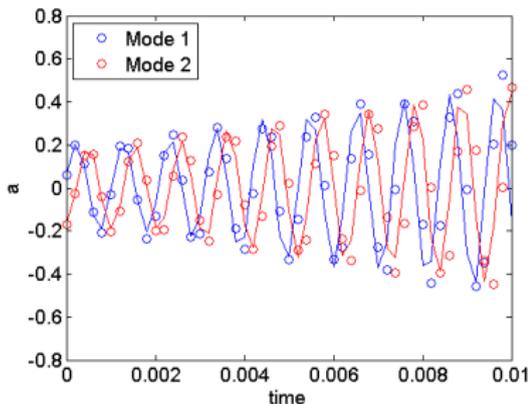
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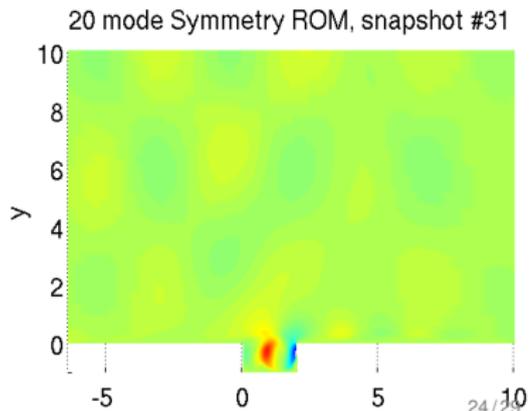
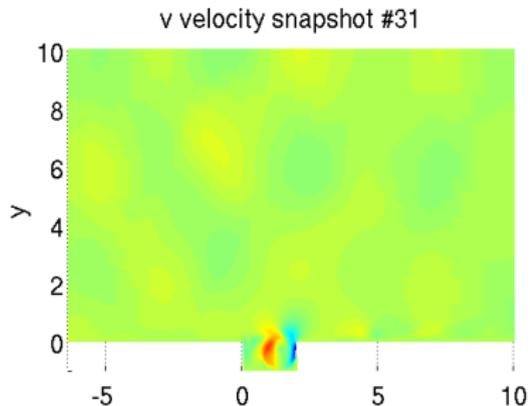
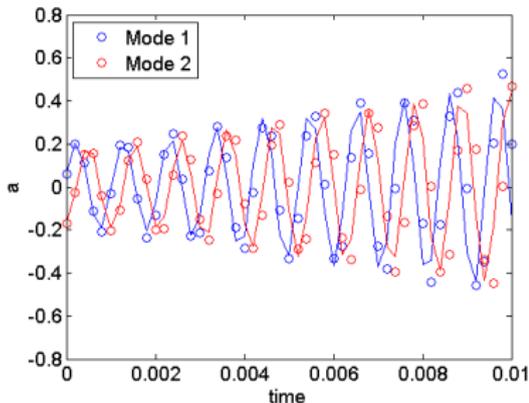
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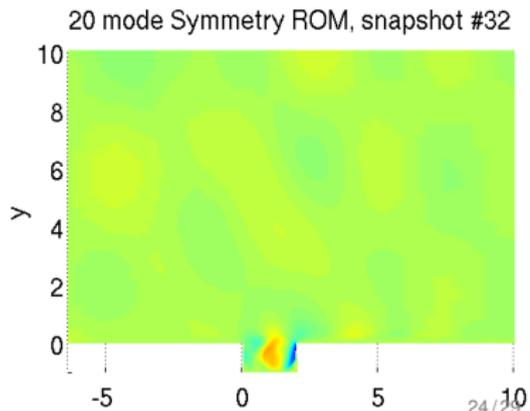
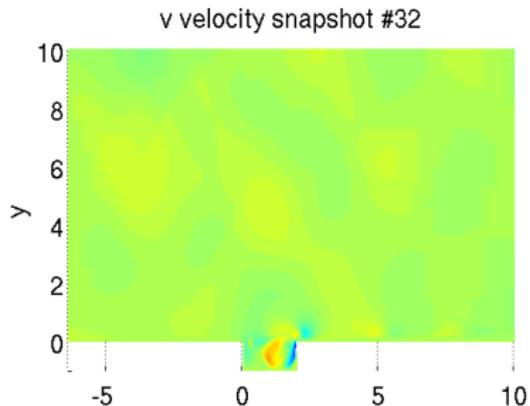
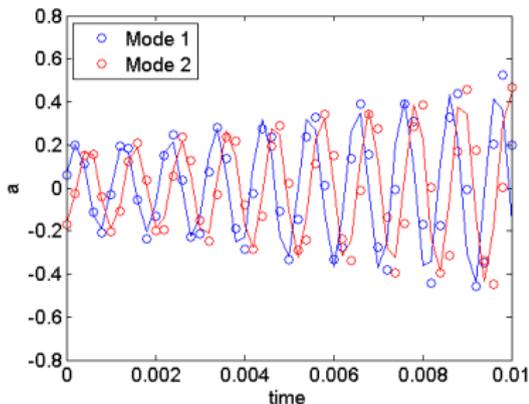
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

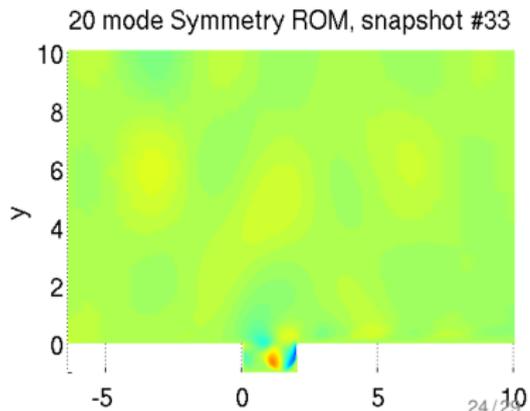
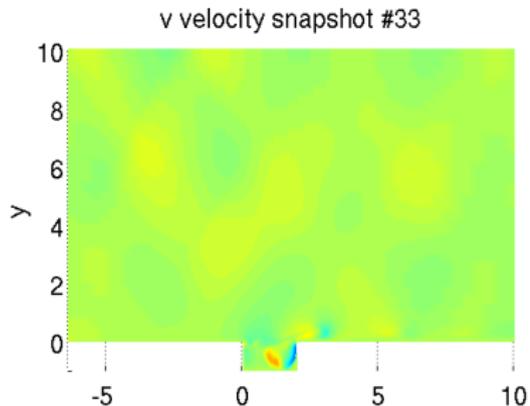
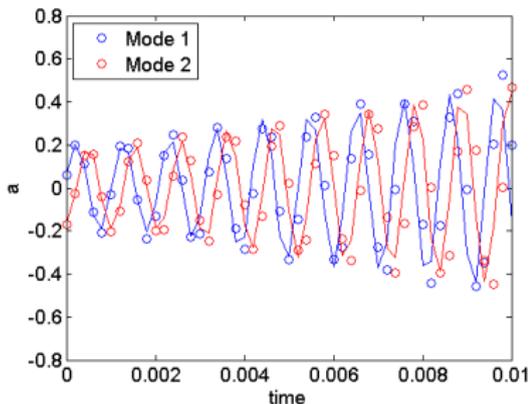
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

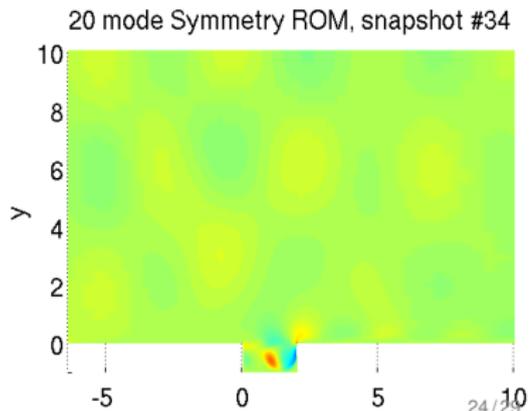
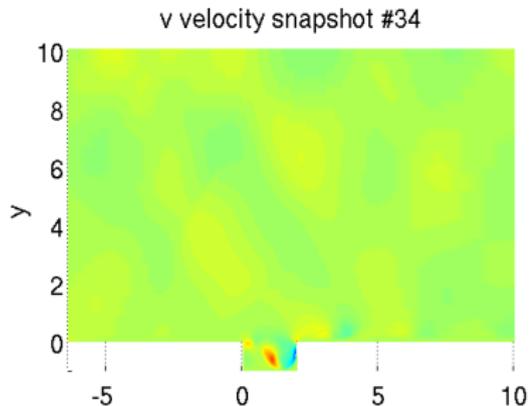
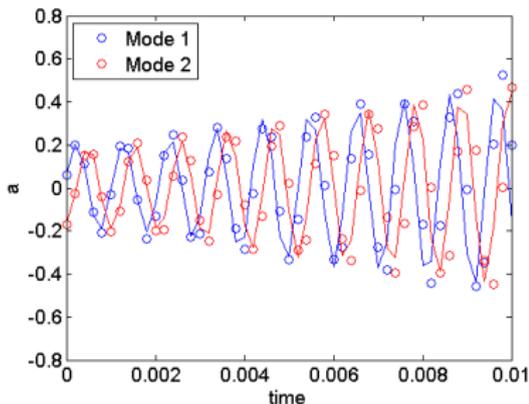
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{q}) - \mathbf{K}_i^{vw}(\nabla\bar{q})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{q})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{q})\mathbf{q}' = \mathbf{F}$$

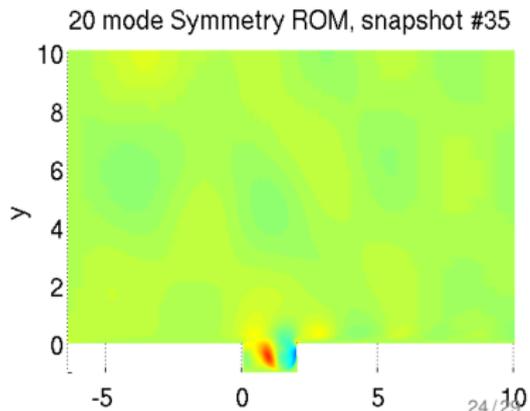
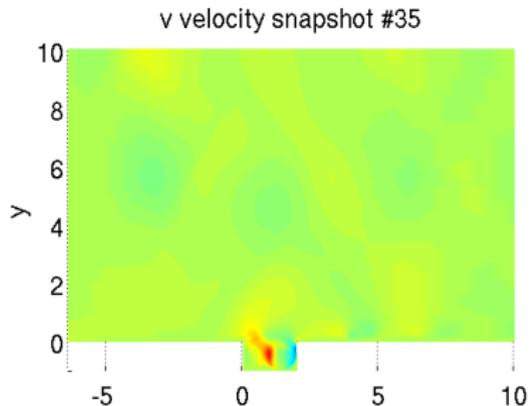
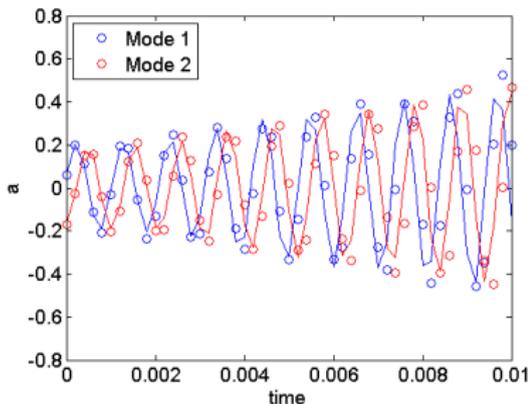
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

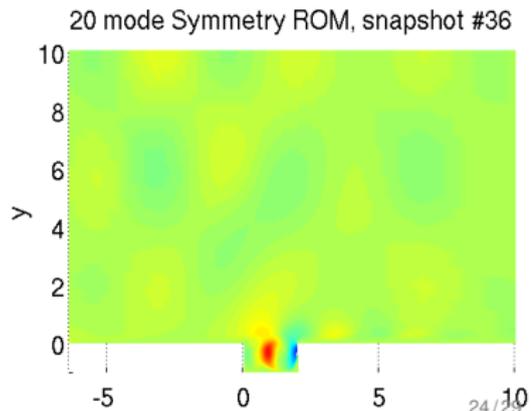
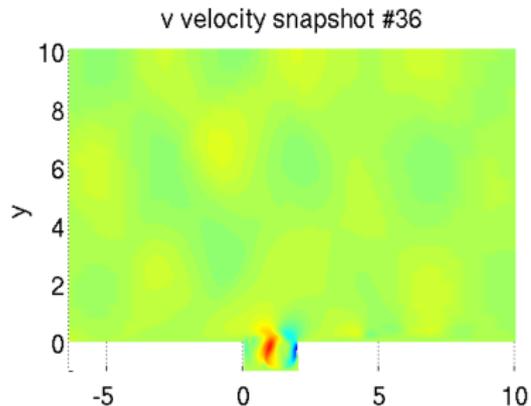
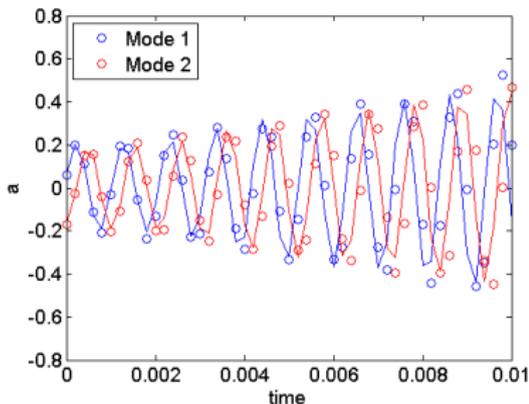
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

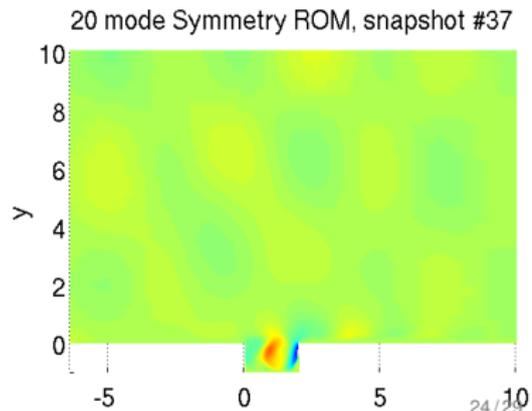
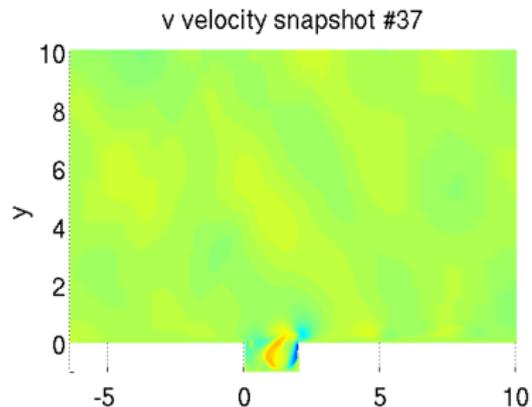
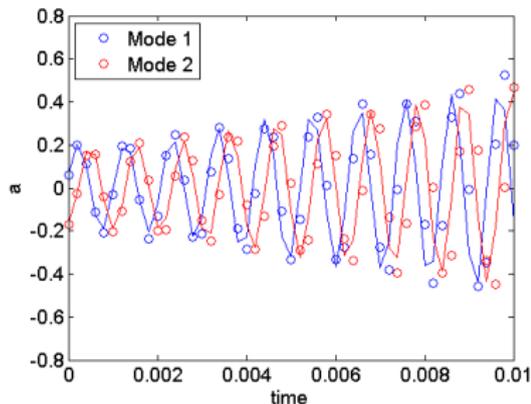
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

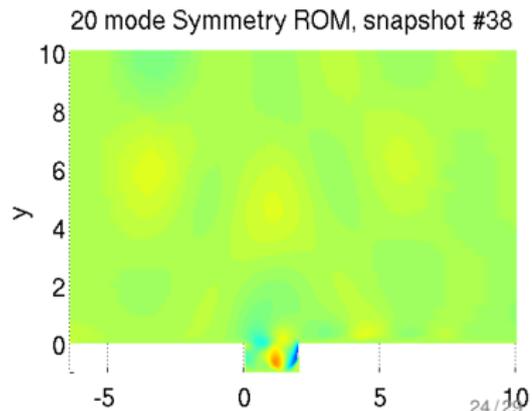
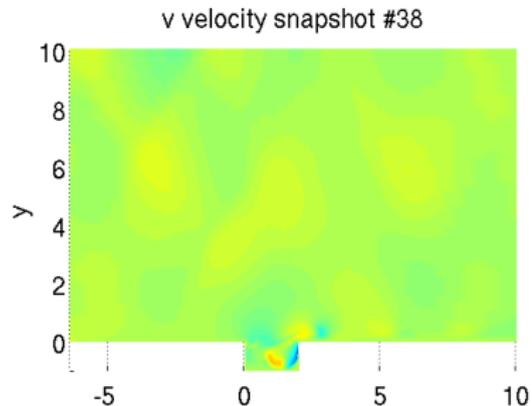
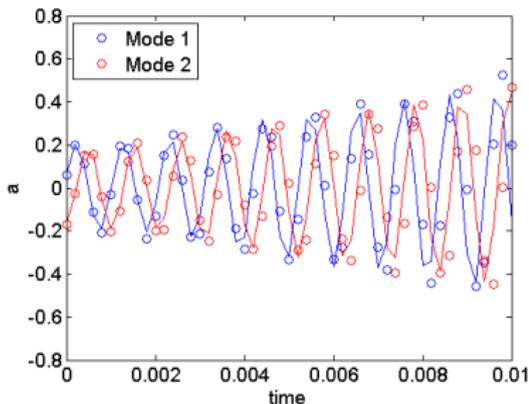
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

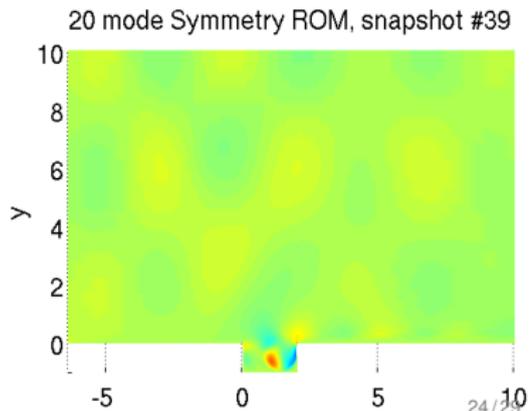
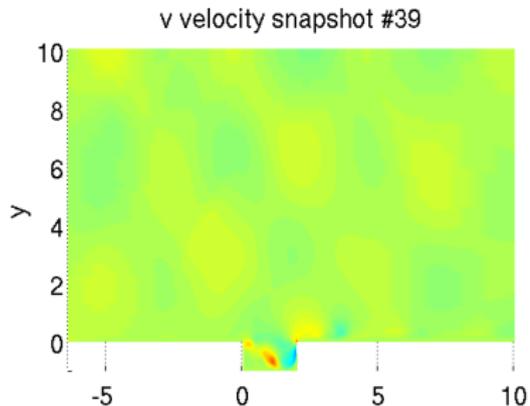
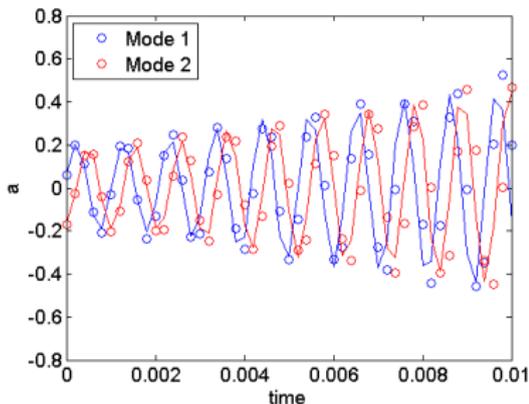
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

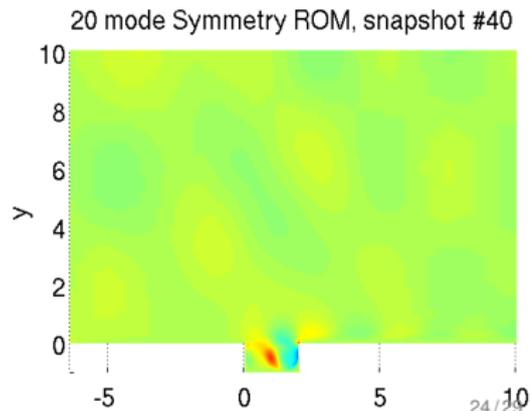
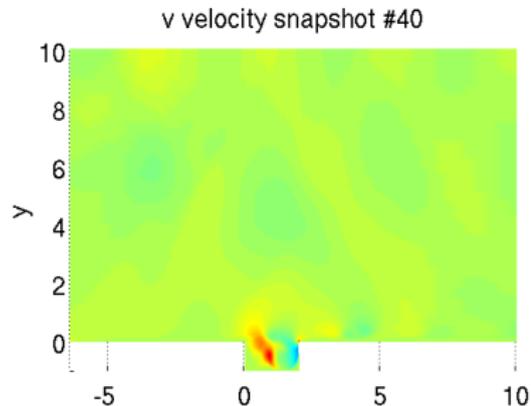
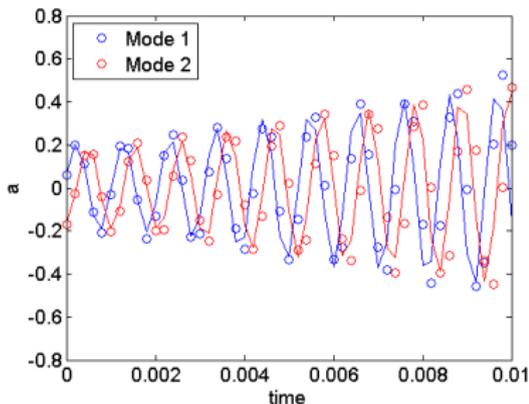
- Figure below shows:
  - $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{q}) - \mathbf{K}_i^{vw}(\nabla\bar{q})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{q})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{q})\mathbf{q}' = \mathbf{F}$$

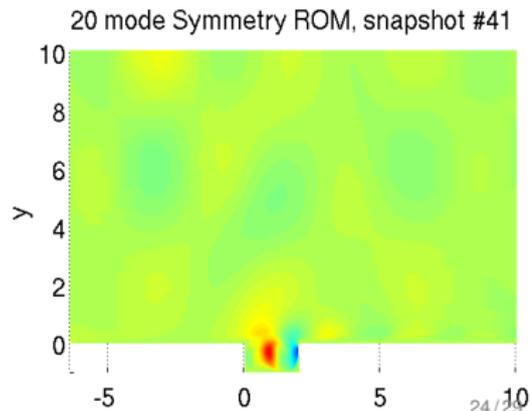
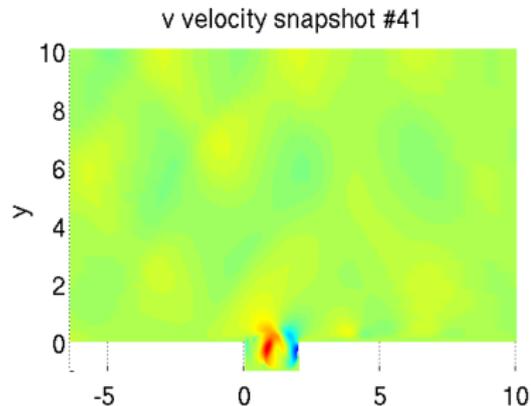
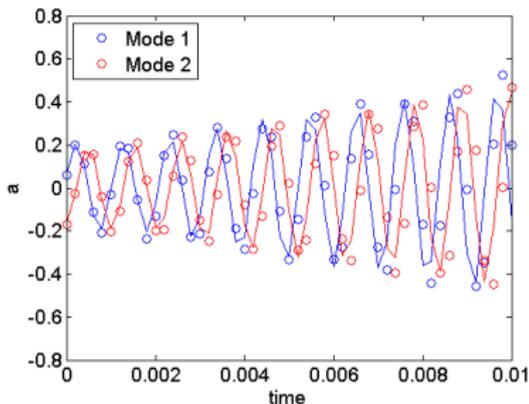
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

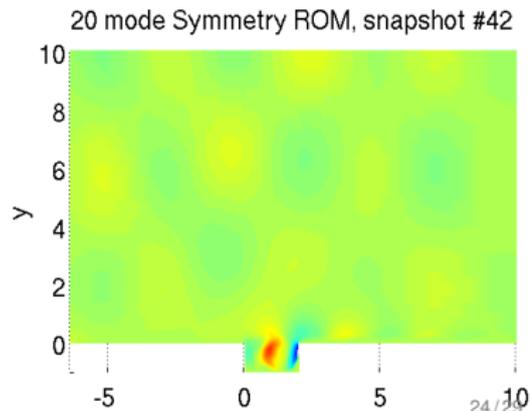
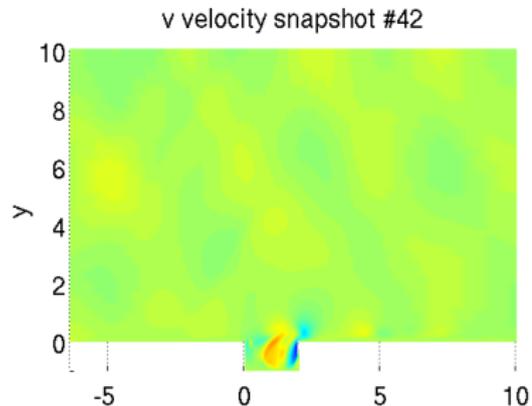
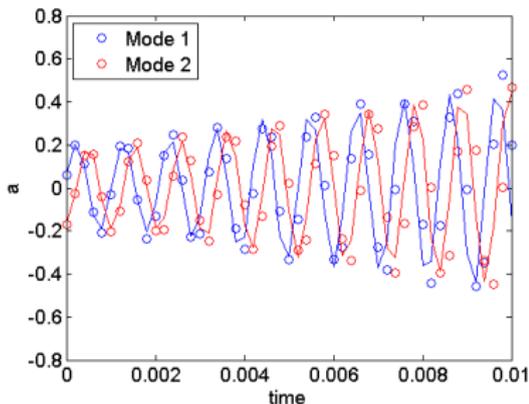
- Figure below shows:
  - $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

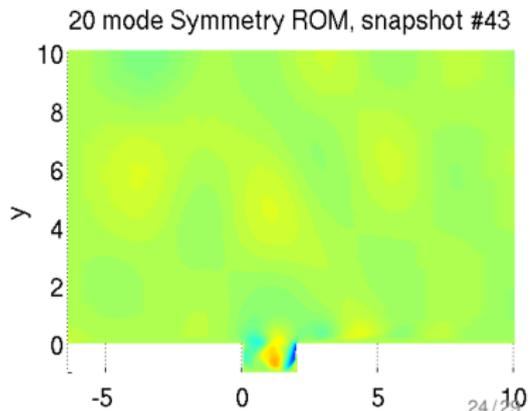
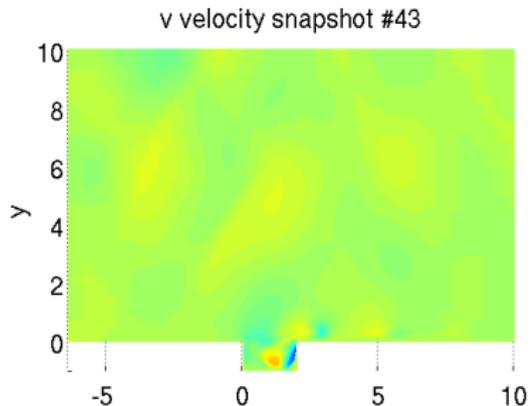
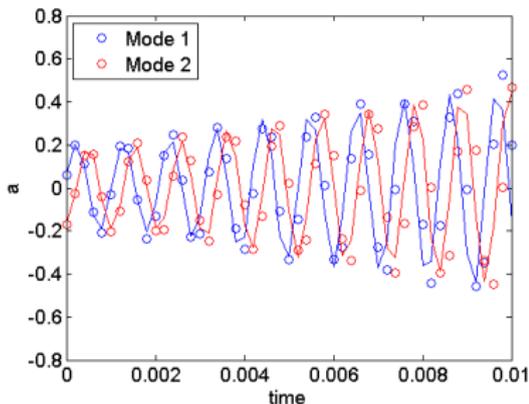
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

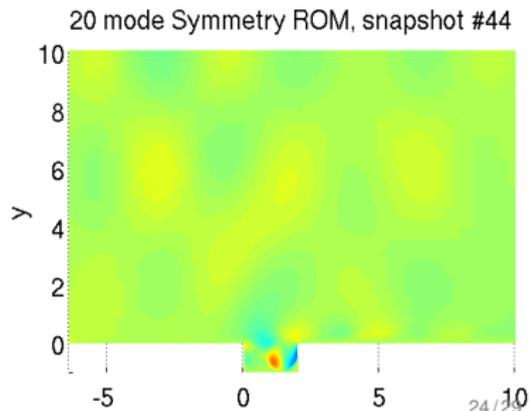
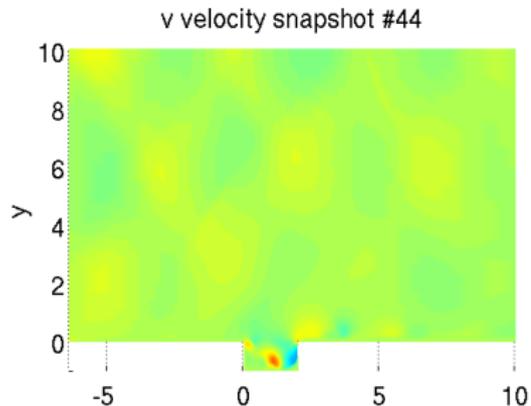
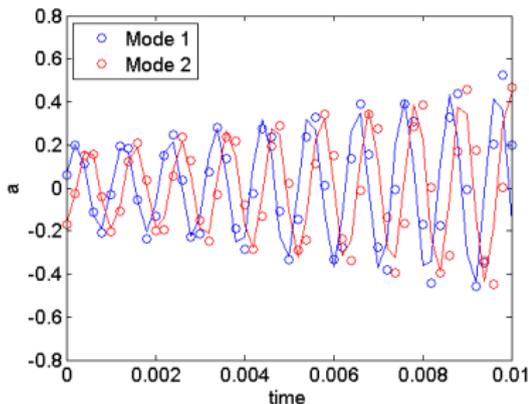
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

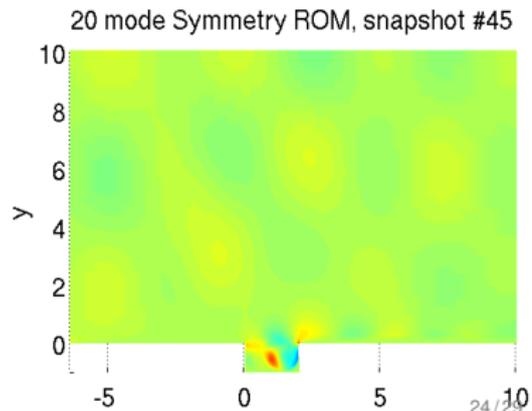
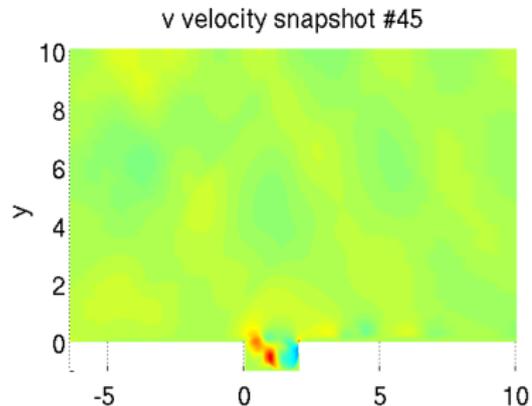
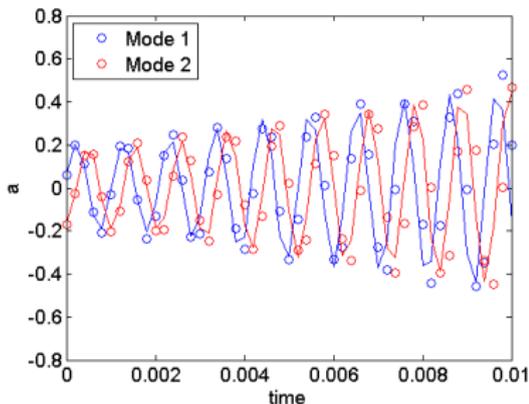
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

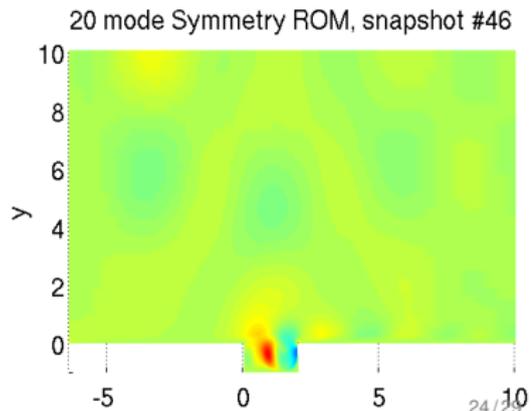
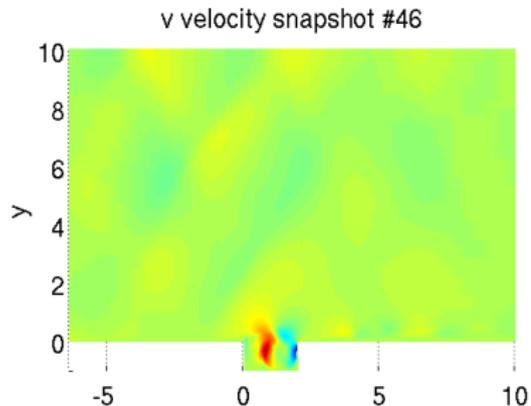
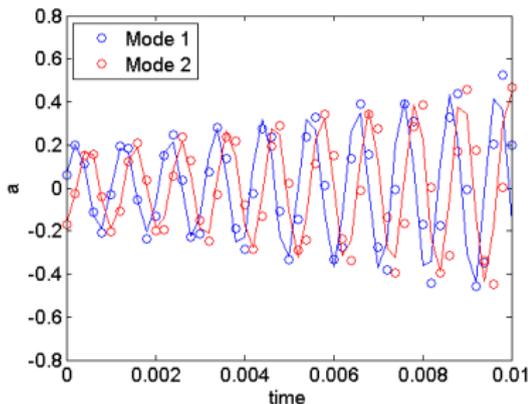
- Figure below shows:
  - ▶ ○:  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶ —:  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

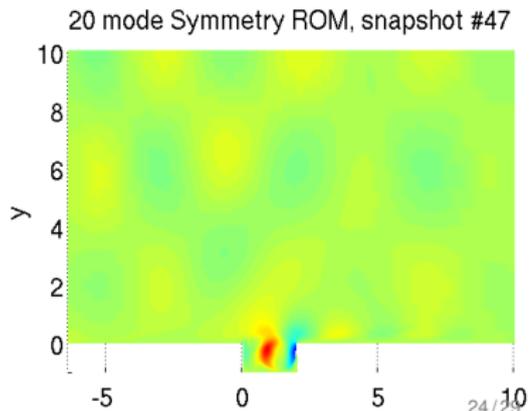
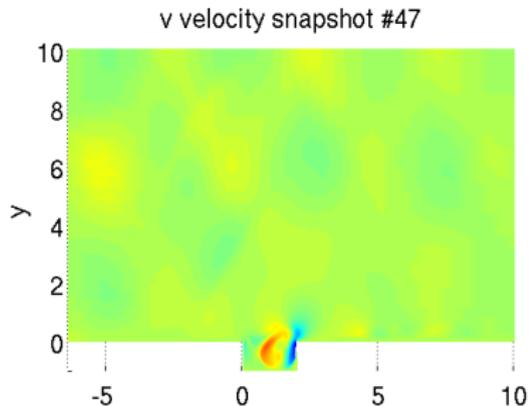
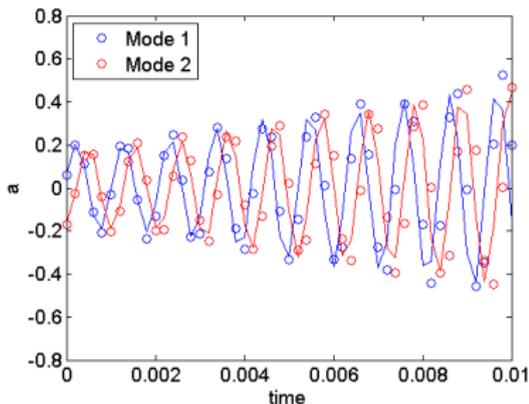
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
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# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

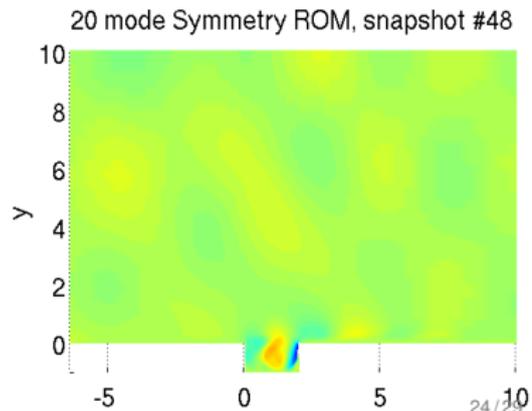
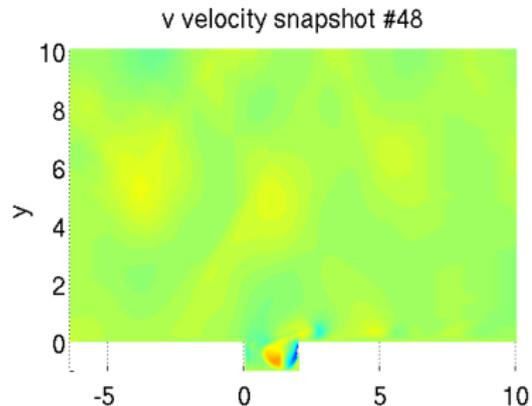
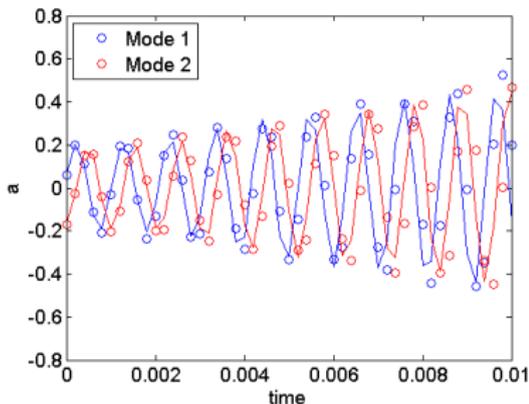
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_j]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

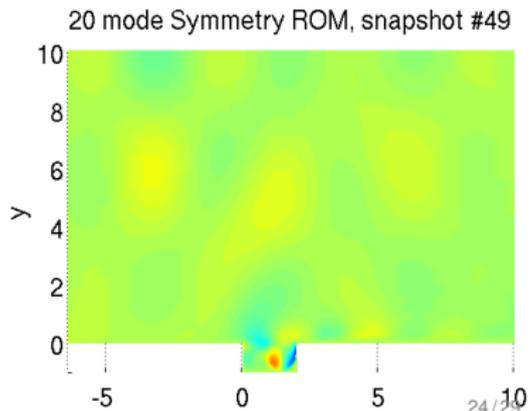
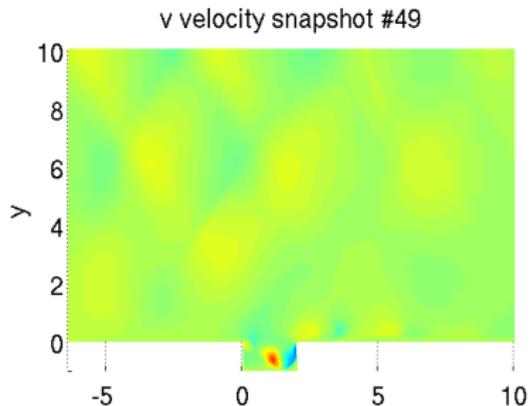
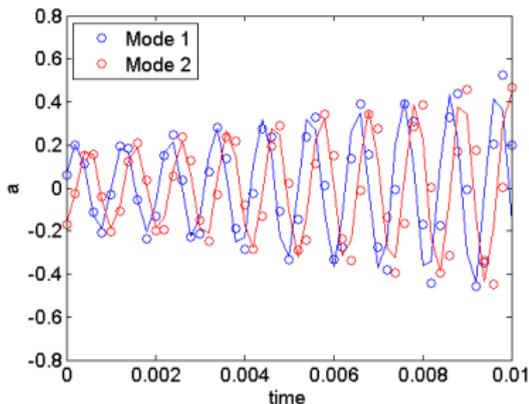
- Figure below shows:
  - ▶ ○:  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶ —:  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_t + [\mathbf{A}_i(\bar{q}) - \mathbf{K}_i^{vw}(\nabla\bar{q})]\mathbf{q}'_i - [\mathbf{K}_{ij}(\bar{q})\mathbf{q}'_j]_i + \mathbf{C}(\nabla\bar{q})\mathbf{q}' = \mathbf{F}$$

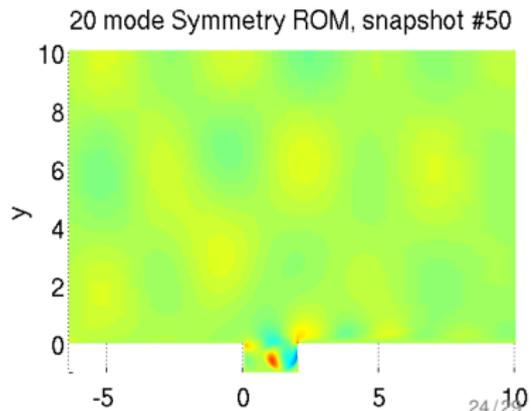
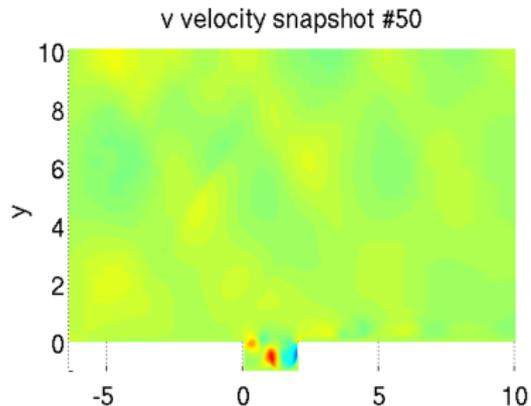
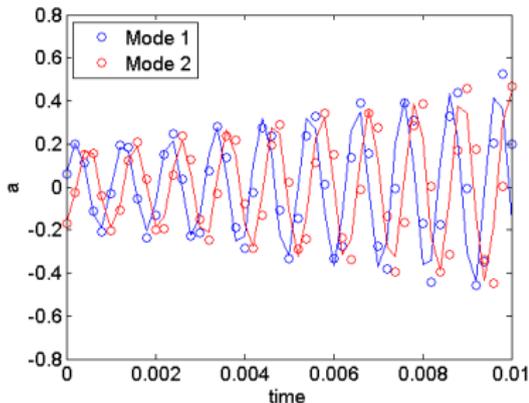
- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).



# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

$$\mathbf{q}'_{,t} + [\mathbf{A}_i(\bar{\mathbf{q}}) - \mathbf{K}_i^{vw}(\nabla\bar{\mathbf{q}})]\mathbf{q}'_{,i} - [\mathbf{K}_{ij}(\bar{\mathbf{q}})\mathbf{q}'_{,j}]_{,i} + \mathbf{C}(\nabla\bar{\mathbf{q}})\mathbf{q}' = \mathbf{F}$$

- Figure below shows:
  - ▶  $\circ$ :  $t$  vs.  $a_i(t)$  (ROM coefficients).
  - ▶  $-$ :  $t$  vs.  $(\mathbf{q}'_{CFD}(\mathbf{x}, t), \phi_i(\mathbf{x}))$  (projection of snapshots onto modes).
- Movie on right shows  $v$ -velocity snapshot (top) vs. 20 mode symmetry ROM solution  $v$  (bottom).





# ROM based on Linearized Navier-Stokes Retaining $\nabla\bar{q}$ Terms

# Summary & Future Work

- A Galerkin ROM in which the *continuous* equations are projected onto the basis modes in a *continuous* inner product is proposed.
- The choice of inner product for the Galerkin projection step is crucial to stability of the ROM.
  - ▶ For linearized compressible flow, Galerkin projection in the “symmetry” inner product leads to a ROM that is stable for any choice of basis.
  - ▶ Continuous “symmetry” inner product has discrete counterpart that can be determined in a black box fashion for *any* stable linear system.
- Extensions to non-linear compressible flows based on a local linearization of the governing equations prior to projection is described.
- Performance of the proposed POD/Galerkin ROM is examined on a linear as well as a non-linear test case.
  - ▶ LQR controller design/performance demonstrated on linear test case (driven inviscid pulse).
  - ▶ Importance of retaining velocity gradient terms in ROM equations illustrated on non-linear test case (driven cavity)

**Future Work:** Controller design for non-linear cavity problems

# References

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- [2] **I. Kalashnikova**, M.F. Barone. "On the Stability and Convergence of a Galerkin Reduced Order Model (ROM) of Compressible Flow with Solid Wall and Far-Field Boundary Treatment". *Int. J. Numer. Meth. Engng.* **83** (2010) 1345-1375.
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Thank you! Questions?

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# Linearized ROM System Matrices

$$\mathbf{A}_1 = \begin{pmatrix} \bar{u}_1 & 0 & 0 & R & \frac{R\bar{T}}{\bar{\rho}} \\ 0 & \bar{u}_1 & 0 & 0 & 0 \\ 0 & 0 & \bar{u}_1 & 0 & 0 \\ \bar{T}(\gamma - 1) & 0 & 0 & \bar{u}_1 & 0 \\ \bar{\rho} & 0 & 0 & 0 & \bar{u}_1 \end{pmatrix}, \quad \mathbf{A}_2 = \begin{pmatrix} \bar{u}_2 & 0 & 0 & 0 & 0 \\ 0 & \bar{u}_2 & 0 & R & \frac{R\bar{T}}{\bar{\rho}} \\ 0 & 0 & \bar{u}_2 & 0 & 0 \\ 0 & \bar{T}(\gamma - 1) & 0 & \bar{u}_2 & 0 \\ 0 & \bar{\rho} & 0 & 0 & \bar{u}_2 \end{pmatrix}$$

$$\mathbf{A}_3 = \begin{pmatrix} \bar{u}_3 & 0 & 0 & 0 & 0 \\ 0 & \bar{u}_3 & 0 & 0 & 0 \\ 0 & 0 & \bar{u}_3 & R & \frac{R\bar{T}}{\bar{\rho}} \\ 0 & 0 & \bar{T}(\gamma - 1) & \bar{u}_3 & 0 \\ 0 & 0 & \bar{\rho} & 0 & \bar{u}_3 \end{pmatrix}, \quad \mathbf{K}_{11} \equiv \frac{1}{\bar{\rho}Re} \begin{pmatrix} 2\mu + \lambda & 0 & 0 & 0 & 0 \\ 0 & \mu & 0 & 0 & 0 \\ 0 & 0 & \mu & 0 & 0 \\ 0 & 0 & 0 & \frac{\gamma\kappa}{Pr} & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix},$$

$$\mathbf{K}_{12} \equiv \frac{1}{\bar{\rho}Re} \begin{pmatrix} 0 & \lambda & 0 & 0 & 0 \\ \mu & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{K}_{13} \equiv \frac{1}{\bar{\rho}Re} \begin{pmatrix} 0 & 0 & \lambda & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ \mu & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

$$\mathbf{K}_{21} \equiv \frac{1}{\bar{\rho}Re} \begin{pmatrix} 0 & \mu & 0 & 0 & 0 \\ \lambda & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{K}_{22} \equiv \frac{1}{\bar{\rho}Re} \begin{pmatrix} \mu & 0 & 0 & 0 & 0 \\ 0 & 2\mu + \lambda & 0 & 0 & 0 \\ 0 & 0 & \mu & 0 & 0 \\ 0 & 0 & 0 & \frac{\gamma\kappa}{Pr} & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

# Linearized ROM System Matrices (continued)

$$\mathbf{K}_{23} \equiv \frac{1}{\bar{\rho} Re} \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \lambda & 0 & 0 \\ 0 & \mu & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{K}_{31} \equiv \frac{1}{\bar{\rho} Re} \begin{pmatrix} 0 & 0 & \mu & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ \lambda & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

$$\mathbf{K}_{32} \equiv \frac{1}{\bar{\rho} Re} \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \mu & 0 & 0 \\ 0 & \lambda & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{K}_{33} \equiv \frac{1}{\bar{\rho} Re} \begin{pmatrix} \mu & 0 & 0 & 0 & 0 \\ 0 & \mu & 0 & 0 & 0 \\ 0 & 0 & 2\mu + \lambda & 0 & 0 \\ 0 & 0 & 0 & \frac{\gamma \kappa}{Pr} & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

$$\mathbf{K}_1^{vw} \equiv \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{11} & \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{12} & \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{13} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{K}_2^{vw} \equiv \begin{pmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{21} & \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{22} \\ 0 & 0 \end{pmatrix}$$

$$\mathbf{K}_3^{vw} \equiv \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{31} & \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{32} & \frac{(\gamma-1)}{R\bar{\rho}} \bar{\tau}_{33} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

# Linearized ROM System Matrices (continued)

$$\mathbf{C} = \begin{pmatrix} \frac{\partial \bar{u}}{\partial x} & \frac{\partial \bar{u}}{\partial y} & \frac{\partial \bar{u}}{\partial z} & \frac{R}{\bar{\rho}} \frac{\partial \bar{p}}{\partial x} & \frac{1}{\bar{\rho}} \left( \bar{\mathbf{u}} \cdot \nabla \bar{u} + R \frac{\partial \bar{T}}{\partial x} \right) \\ \frac{\partial \bar{v}}{\partial x} & \frac{\partial \bar{v}}{\partial y} & \frac{\partial \bar{v}}{\partial z} & \frac{R}{\bar{\rho}} \frac{\partial \bar{p}}{\partial y} & \frac{1}{\bar{\rho}} \left( \bar{\mathbf{u}} \cdot \nabla \bar{v} + R \frac{\partial \bar{T}}{\partial y} \right) \\ \frac{\partial \bar{w}}{\partial x} & \frac{\partial \bar{w}}{\partial y} & \frac{\partial \bar{w}}{\partial z} & \frac{R}{\bar{\rho}} \frac{\partial \bar{p}}{\partial z} & \frac{1}{\bar{\rho}} \left( \bar{\mathbf{u}} \cdot \nabla \bar{w} + R \frac{\partial \bar{T}}{\partial z} \right) \\ \frac{\partial \bar{T}}{\partial x} & \frac{\partial \bar{T}}{\partial y} & \frac{\partial \bar{T}}{\partial z} & (\gamma - 1) \nabla \cdot \bar{\mathbf{u}} & \frac{1}{\bar{\rho}} \left( \bar{\mathbf{u}} \cdot \nabla \bar{T} + (\gamma - 1) \bar{T} \nabla \cdot \bar{\mathbf{u}} \right) \\ \frac{\partial \bar{p}}{\partial x} & \frac{\partial \bar{p}}{\partial y} & \frac{\partial \bar{p}}{\partial z} & 0 & \nabla \cdot \bar{\mathbf{u}} \end{pmatrix}$$