

Peridynamic Modeling of Localization in Ductile Metals

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Peridynamics

WHAT IS PERIDYNAMICS?

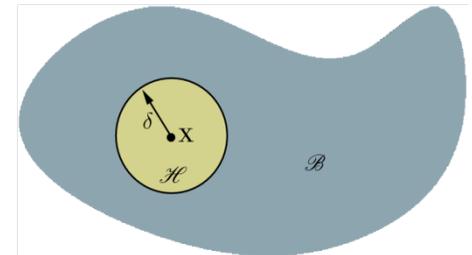
Peridynamics is a mathematical theory that unifies the mechanics of continuous media, cracks, and discrete particles

HOW DOES IT WORK?

- Peridynamics is a *nonlocal* extension of continuum mechanics
- Remains valid in presence of discontinuities, including cracks
- Balance of linear momentum is based on an *integral equation*:

$$\rho(\mathbf{x})\ddot{\mathbf{u}}(\mathbf{x}, t) = \underbrace{\int_{\mathcal{B}} \{ \underline{\mathbf{T}}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle - \underline{\mathbf{T}}'[\mathbf{x}', t] \langle \mathbf{x} - \mathbf{x}' \rangle \}}_{\text{Divergence of stress replaced with integral of nonlocal forces.}} dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

The point X interacts directly with all points within its horizon



S.A. Silling. Reformulation of elasticity theory for discontinuities and long-range forces. *Journal of the Mechanics and Physics of Solids*, 48:175-209, 2000.

Silling, S.A. and Lehoucq, R. B. Peridynamic Theory of Solid Mechanics. *Advances in Applied Mechanics* 44:73-168, 2010.

Peridynamics

CONSTITUTIVE LAWS IN PERIDYNAMICS

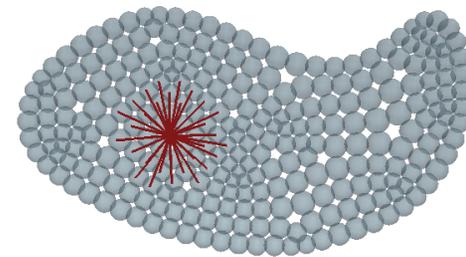
- Peridynamic *bonds* connect any two material points that interact directly
- Peridynamic forces are determined by *force states* acting on bonds

$$\underbrace{\underline{\mathbf{T}}[\mathbf{x}, t]}_{\text{Force State}} \quad \underbrace{\langle \mathbf{x}'_i - \mathbf{x} \rangle}_{\text{Bond}}$$

- Force states are determined by constitutive laws and are functions of the deformations of all points within a neighborhood
- *Material failure* is modeled through the breaking of peridynamic bonds
 - Example: critical stretch bond breaking law

DISCRETIZATION OF A PERIDYNAMIC BODY

A body may be represented by a finite number of sphere elements



$$\rho(\mathbf{x}) \ddot{\mathbf{u}}_h(\mathbf{x}, t) = \sum_{i=0}^N \left\{ \underline{\mathbf{T}}[\mathbf{x}, t] \langle \mathbf{x}'_i - \mathbf{x} \rangle - \underline{\mathbf{T}}'[\mathbf{x}'_i, t] \langle \mathbf{x} - \mathbf{x}'_i \rangle \right\} \Delta V_{\mathbf{x}'_i} + \mathbf{b}(\mathbf{x}, t)$$

State-based Peridynamic Material Models

LINEAR PERIDYNAMIC SOLID (ELASTIC MODEL)

$$\theta(\underline{e}) = \frac{3}{m} (\underline{\omega} \underline{x}) \bullet \underline{e}$$

$$\underline{t} = \frac{3k\theta}{m} \underline{\omega} \underline{x} + \frac{15\mu}{m} \underline{\omega} \underline{e}^d$$

ELASTIC-PLASTIC MODEL

$$\underline{t} = \frac{3k\theta}{m} \underline{\omega} \underline{x} + \frac{15\mu}{m} \underline{\omega} (\underline{e}^d - \underline{e}^{dp})$$

S.A. Silling, M. Epton, O. Weckner, J. Xu, and E. Askari, Peridynamic states and constitutive modeling, *Journal of Elasticity*, 88, 2007.

J.A. Mitchell. A nonlocal, ordinary, state-based plasticity model for peridynamics. Sandia Report SAND2011-3166, 2011.

Adaptation of Classical Material Models for Peridynamics

APPROACH: NON-ORDINARY STATE-BASED PERIDYNAMICS

- Apply existing (local) constitutive models within nonlocal peridynamic framework
- Utilize approximate deformation gradient based on positions and deformations of all elements in the neighborhood

- ① Compute regularized deformation gradient

$$\bar{\mathbf{F}} = \left(\sum_{i=0}^N \underline{\omega}_i \underline{\mathbf{Y}}_i \otimes \underline{\mathbf{X}}_i \Delta V_{\mathbf{x}_i} \right) \mathbf{K}^{-1} \quad \mathbf{K} = \sum_{i=0}^N \underline{\omega}_i \underline{\mathbf{X}}_i \otimes \underline{\mathbf{X}}_i \Delta V_{\mathbf{x}_i}$$

- ② Classical material model computes stress based on regularized deformation gradient
- ③ Convert stress to peridynamic force densities

$$\underline{\mathbf{T}} \langle \mathbf{x}' - \mathbf{x} \rangle = \underline{\omega} \sigma \mathbf{K}^{-1} \langle \mathbf{x}' - \mathbf{x} \rangle$$

- ④ Apply peridynamic hourglass forces as required to stabilize simulation (optional)

S. Silling, M. Epton, O. Weckner, J. Xu, and E. Askari. Peridynamic states and constitutive modeling. *Journal of Elasticity*, 88(2):151-184, 2007.

Suppression of Zero-Energy Modes

APPROACH: PENALIZE DEFORMATION THAT DEVIATES FROM REGULARIZED DEFORMATION GRADIENT

Predicted location of neighbor

$$\mathbf{x}'_n{}^* = \mathbf{x}_n + \bar{\mathbf{F}}_n (\mathbf{x}'_o - \mathbf{x}_o)$$

Hourglass vector

$$\mathbf{\Gamma}_{\text{hg}} = \mathbf{x}'_n{}^* - \mathbf{x}'_n$$

Hourglass vector projected onto bond

$$\gamma_{\text{hg}} = \mathbf{\Gamma}_{\text{hg}} \cdot (\mathbf{x}'_n - \mathbf{x}_n)$$

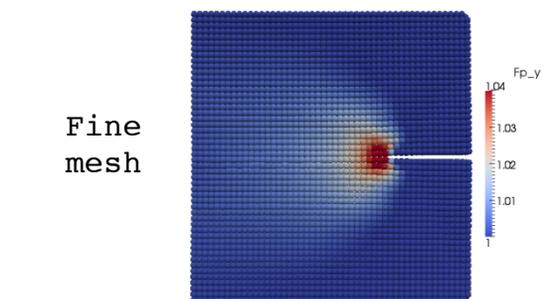
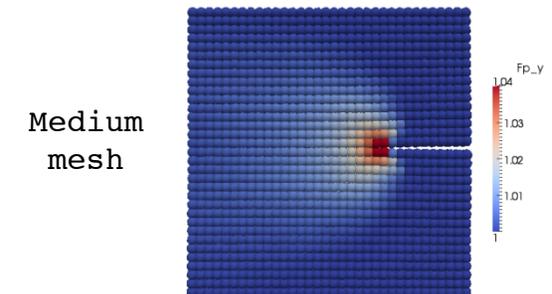
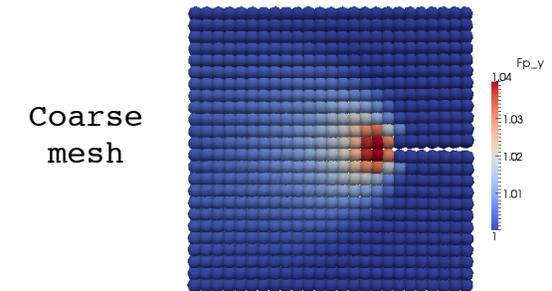
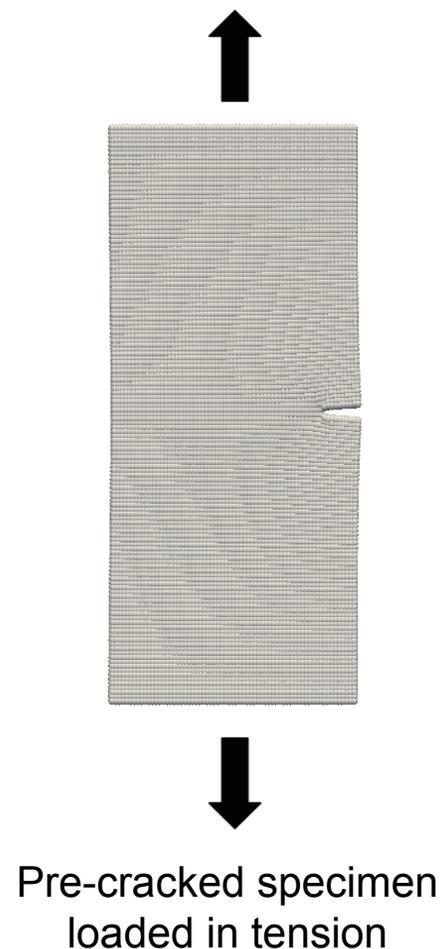
Hourglass force

$$\begin{array}{c} \text{Hourglass force} \\ \longrightarrow \mathbf{f}_{\text{hg}} = -C_{\text{hg}} \underbrace{\left(\frac{18k}{\pi\delta^4} \right)}_{\text{micro-modulus}} \underbrace{\frac{\gamma_{\text{hg}}}{\|\mathbf{x}'_o - \mathbf{x}_o\|}}_{\text{hourglass stretch}} \underbrace{\frac{\mathbf{x}'_n - \mathbf{x}_n}{\|\mathbf{x}'_n - \mathbf{x}_n\|}}_{\text{bond unit vector}} \Delta V_x \Delta V_{x'} \end{array}$$

Peridynamic Horizon Provides a Length Scale

NONLOCALITY YIELDS MESH INDEPENDENCE AT CRACK TIP

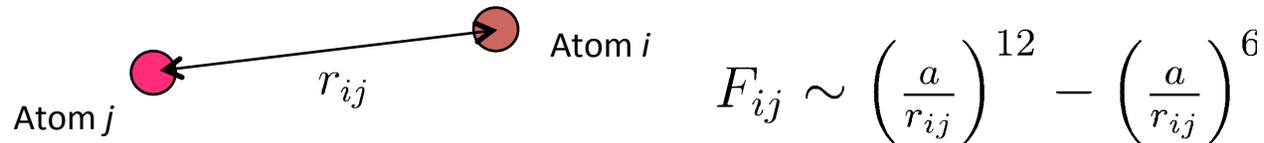
- The peridynamic horizon introduces a length scale that is independent of the mesh size.
- Decoupling from the mesh size enables consistent modeling of material response in the vicinity of discontinuities.
- Example: Mesh independent plastic zone in the vicinity of a crack.



Can the Peridynamic Horizon Have Physical Meaning?

MANY PHYSICAL PROBLEMS HAVE NATURAL LENGTH SCALE(S)

- Interatomic forces

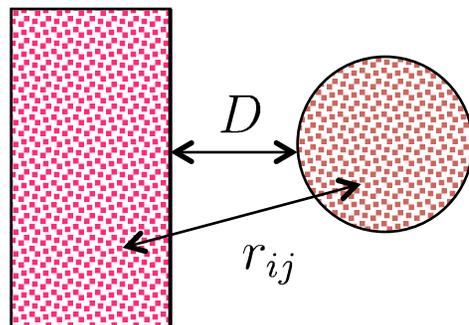


- Van der Waals forces

- Force between a pair of atoms as they are separated:

$$F_{ij} \sim 1/r_{ij}^6$$

- Net force between half-space and sphere occurs over a much larger length scale*



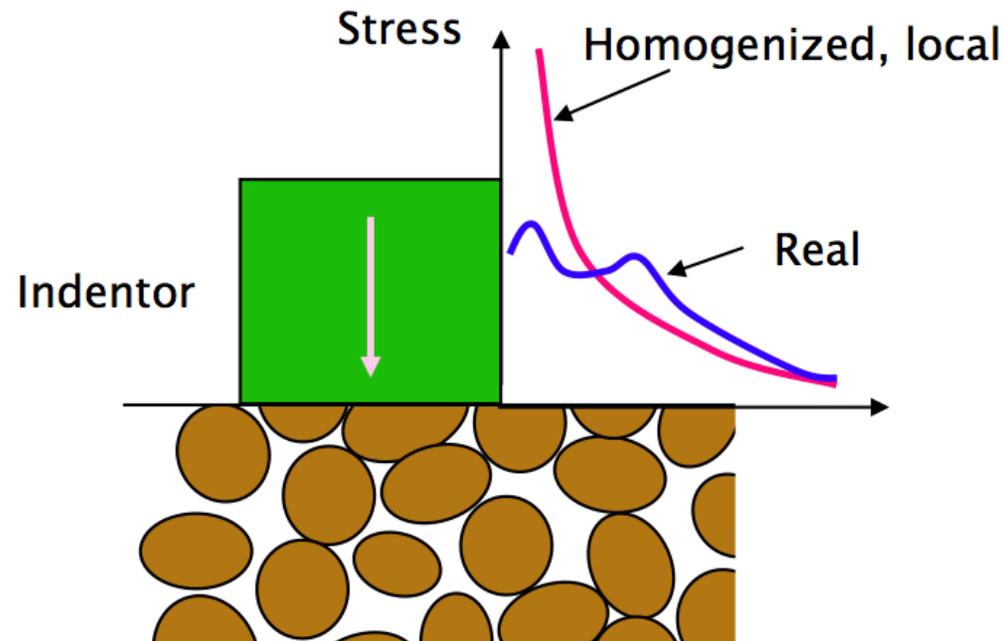
$$F_{\text{sphere}} \sim 1/D$$

*See J. Israelachvili, *Intermolecular and Surfaces Forces*, pp. 177.

Physical Interpretation of Peridynamic Horizon

NONLOCALITY AS A RESULT OF HOMOGENIZATION

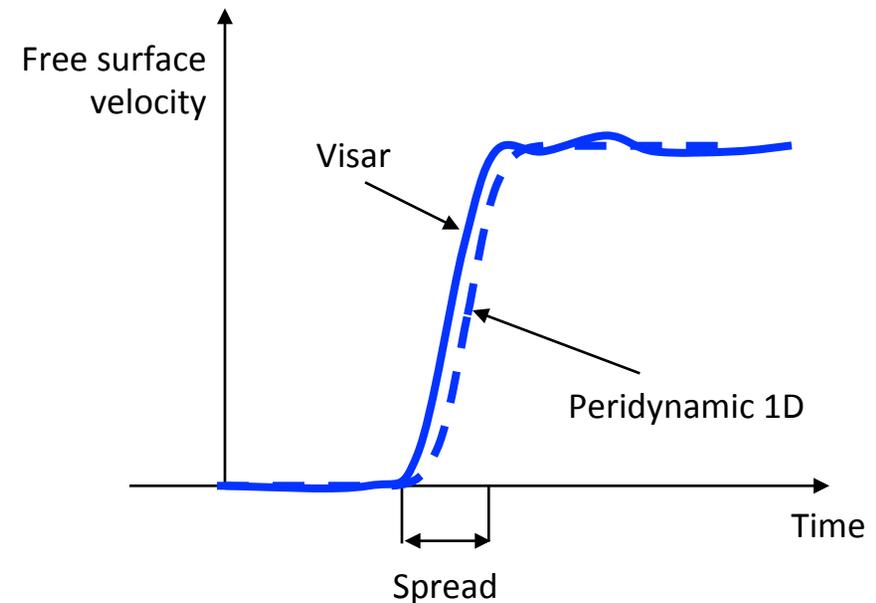
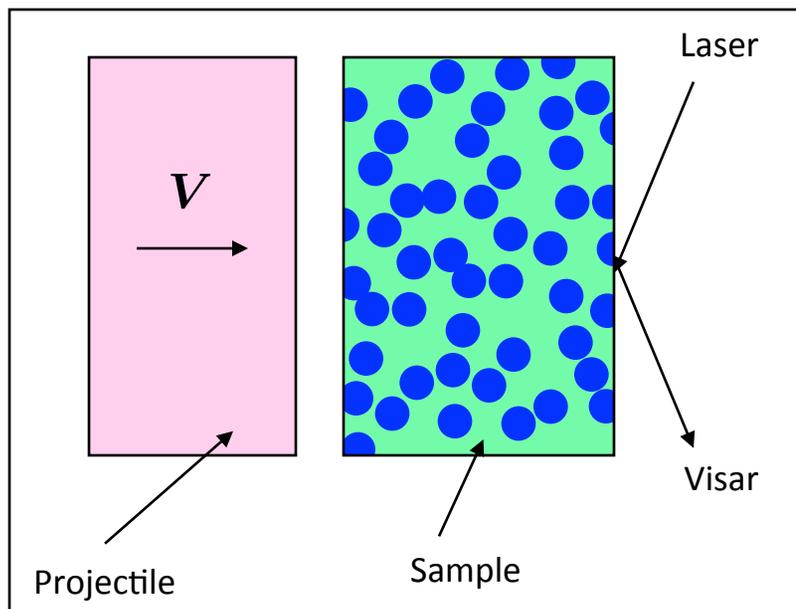
- Homogenization (neglecting natural length scales) often leads to poor results
- Nonlocality (length scale) can be an essential feature of a realistic homogenized model of a heterogeneous material
- Example: Concrete indenter



Physical Interpretation of Peridynamic Horizon

PROPOSED EXPERIMENTAL METHOD FOR MEASURING THE PERIDYNAMIC HORIZON

- Measure how much a step wave spreads as it goes through a heterogeneous sample
- Fit the horizon in a peridynamic model to match observed spread



Local model would predict zero spread

Peridynamics and Higher-Order Gradient Methods

- Local models contain no length scale

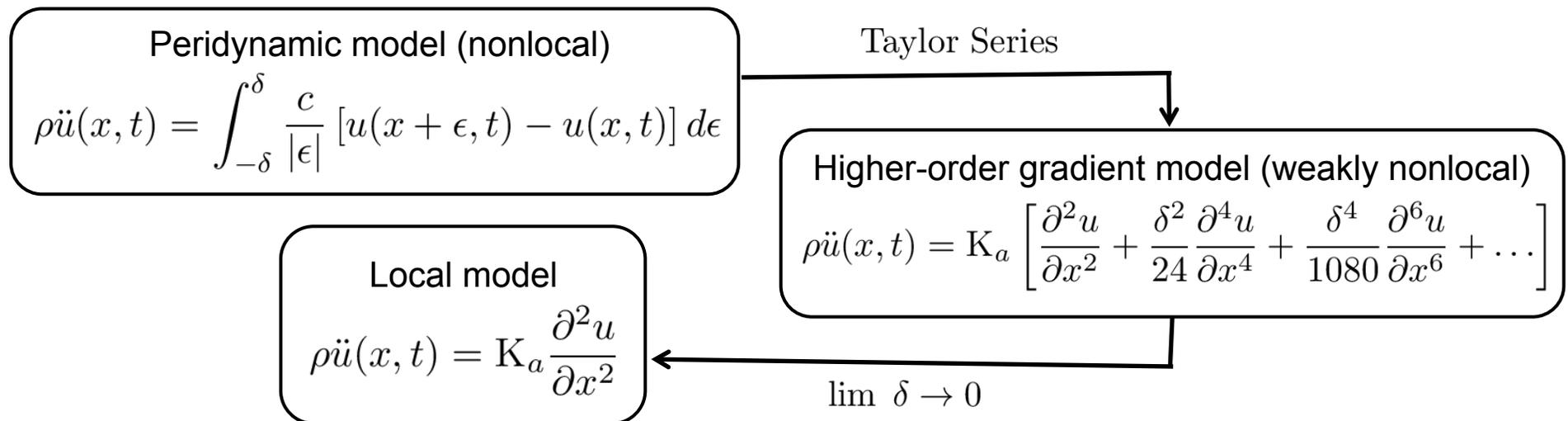
$$\ddot{u}(x) = au''(x)$$

- Higher-order gradients introduce length scale in a weak sense

$$\ddot{u}(x) = au''(x) + bu''''(x)$$

➔ Dimensional analysis shows that $\sqrt{b/a}$ has units of length

- Peridynamics is a (strongly) nonlocal model



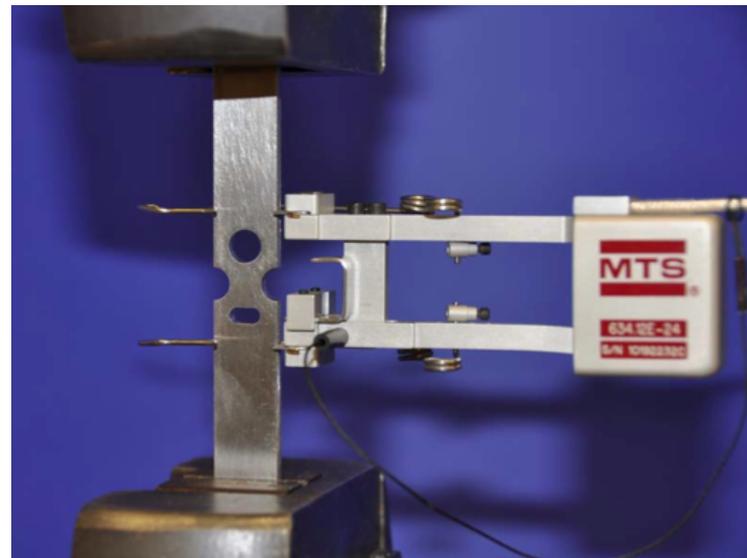
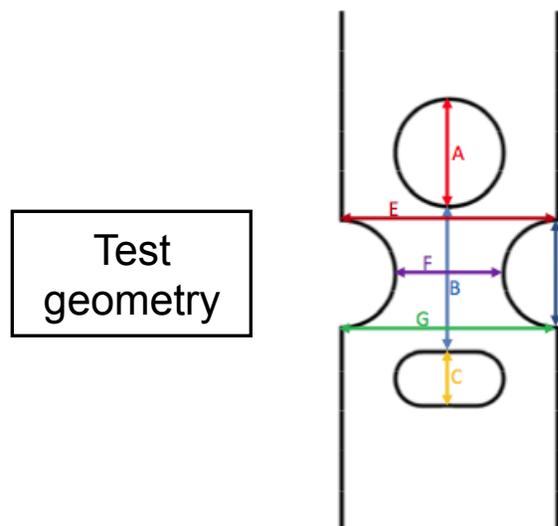
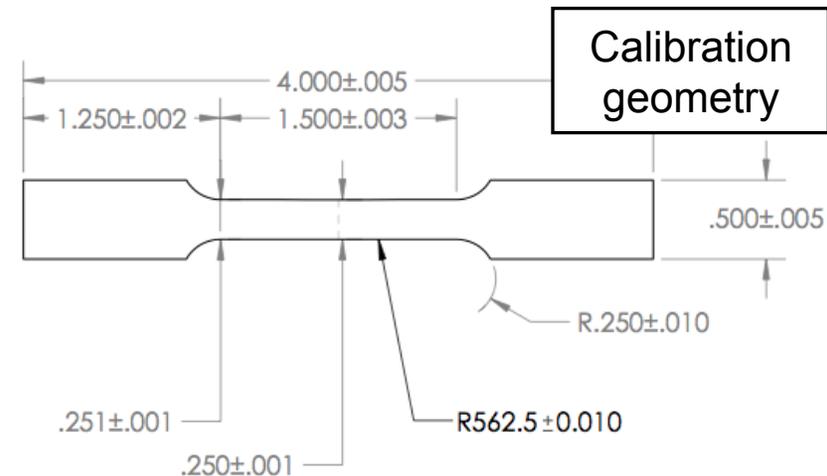
S.A. Silling and R.B. Lehoucq, Convergence of peridynamics to classical elasticity theory, *Journal of Elasticity*, 93(1), 2008.

Pablo Seleson, Michael L. Parks, Max Gunzburger, and Richard B. Lehoucq. Peridynamics as an upscaling of molecular dynamics. *Multiscale Modeling and Simulation*, 8(1), 2009.

Necking Experiment

CAN A PERIDYNAMIC MODEL PREDICT LOCALIZATION?

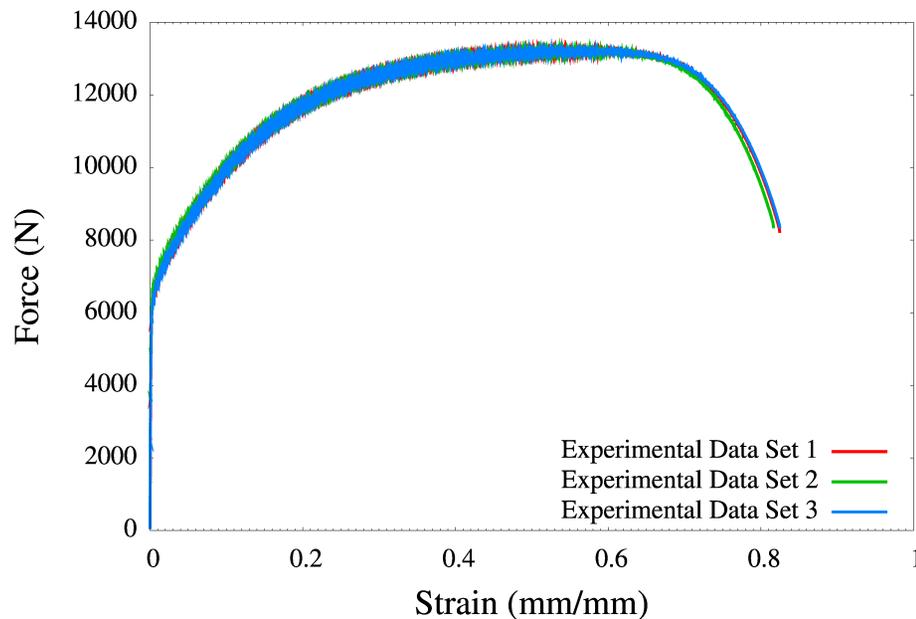
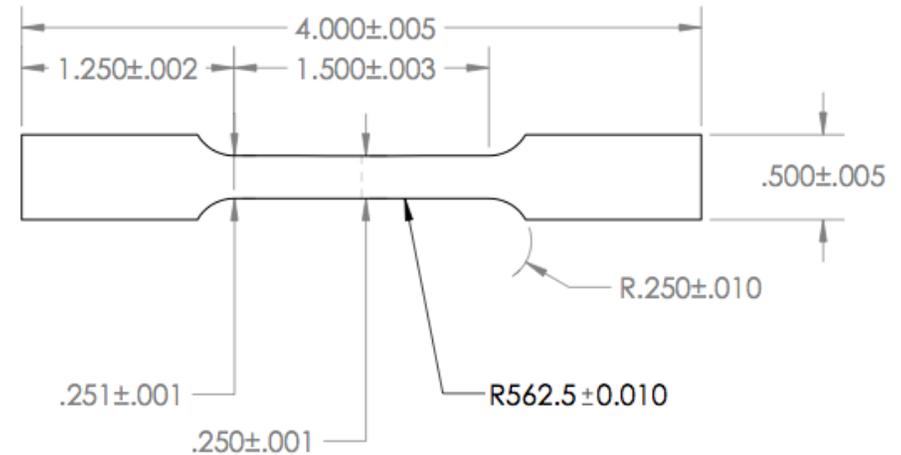
- Test setup:
 - 304L stainless steel (very ductile)
 - Quasi-static loading conditions
 - Standard tensile test results provided for calibration
- Challenge:
 - Predict force and engineering strain at peak load
 - Predict engineering strain when force has dropped to 95% of peak load
 - Predict chord lengths when force has dropped to 95% of peak load



Necking Experiment: Calibration of Peridynamic Model

TENSILE TEST CALIBRATION DATA

- Force versus engineering strain
- Cross-sectional area at the point where the force dropped to 75% of peak load



Cross-sectional Area

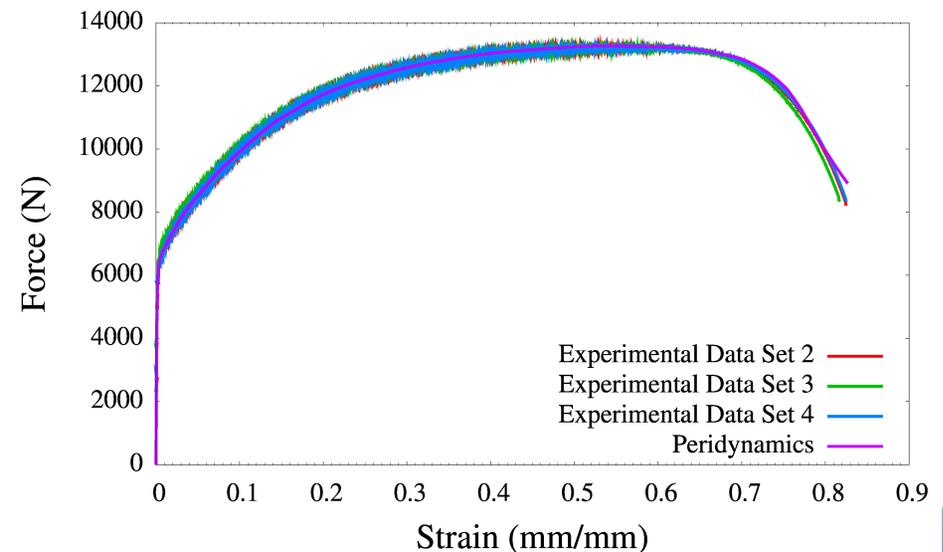
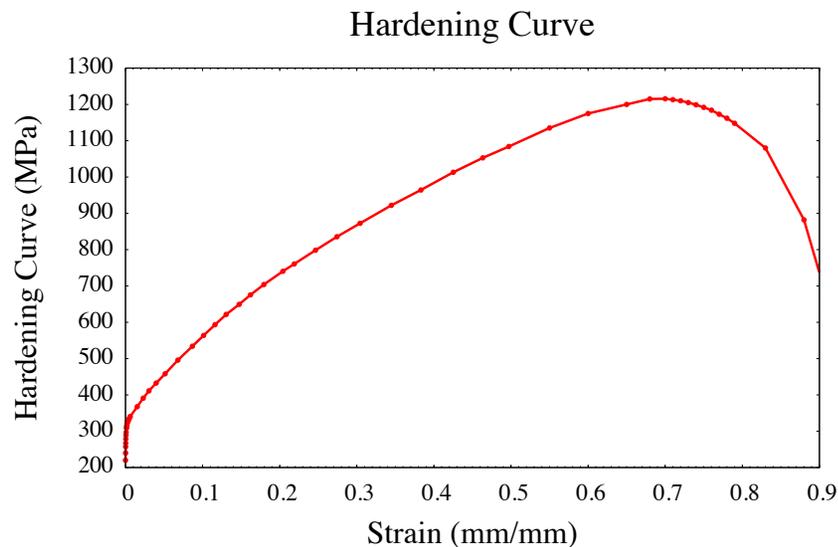
Initial value: 0.0310 in^2
At 75% peak load: 0.0107 in^2

Necking Experiment: Calibration of Peridynamic Model

ELASTIC-PLASTIC MODEL WITH PIECEWISE LINEAR HARDENING CURVE

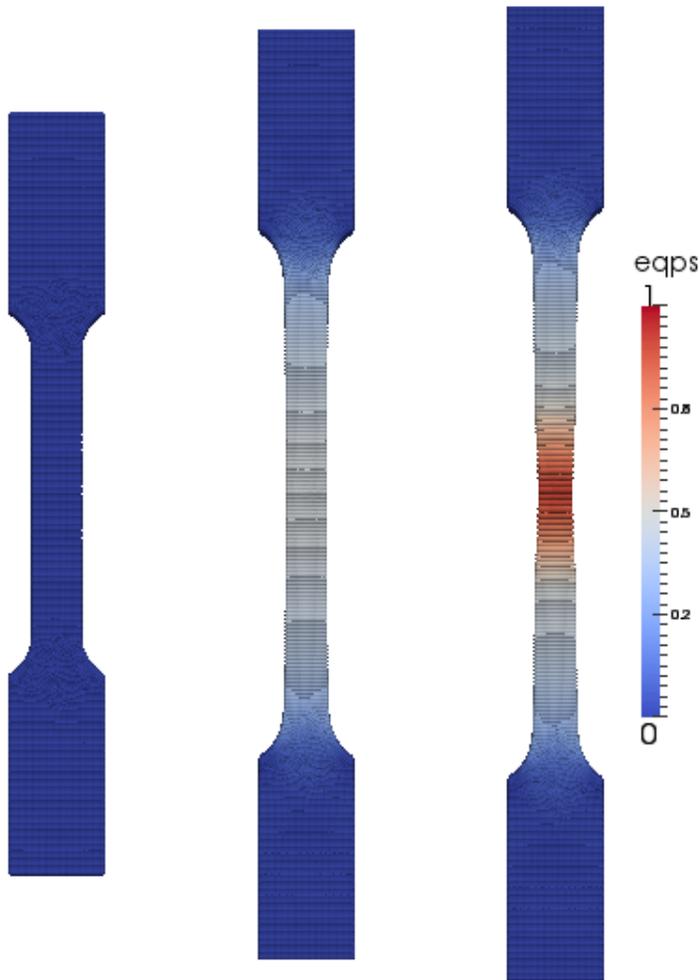
- Quasi-static simulations carried out with *Sierra/SolidMechanics*
- Initial calibration taken from classical finite-element model of tensile test (automated calibration tool)
- Hardening curve manually adjusted past ultimate tensile strength

Young's Modulus	199.95e3 MPa
Poisson's Ratio	0.285
Yield Stress	220.0 MPa



Necking Experiment: Calibration of Peridynamic Model

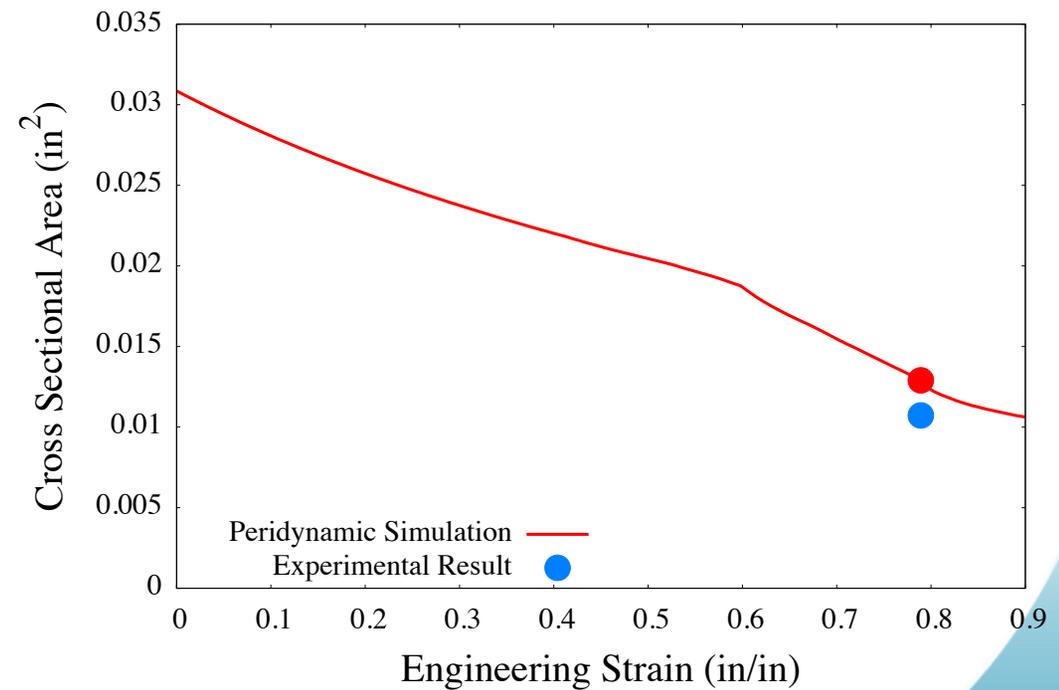
LOCALIZATION IN TENSILE TEST



Cross-sectional Area

Initial value: 0.031 in²

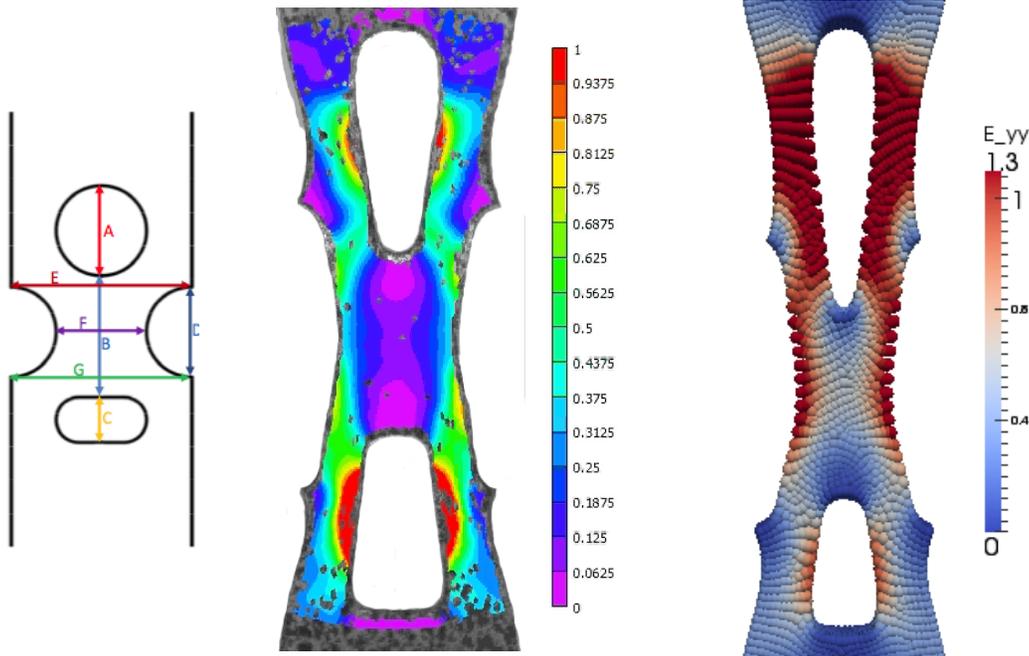
Simulation at 75% peak load: 0.0129 in²



Necking Experiment: Test Geometry

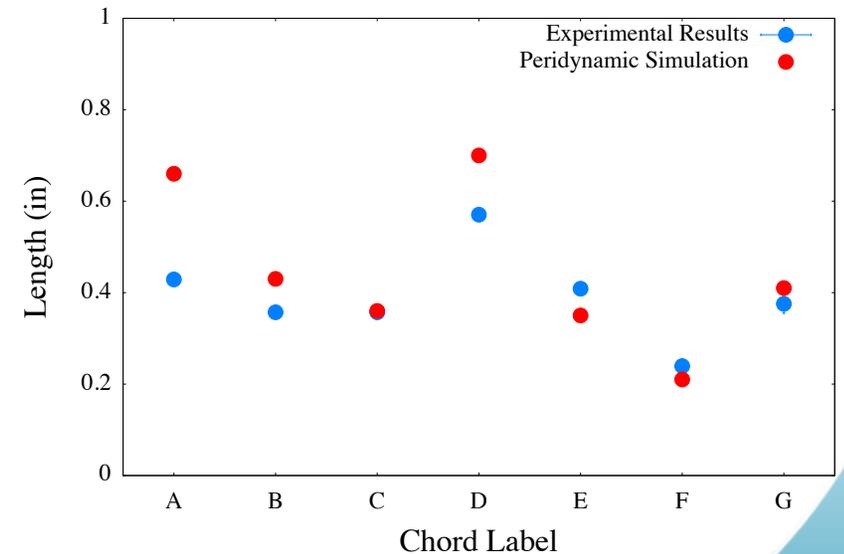
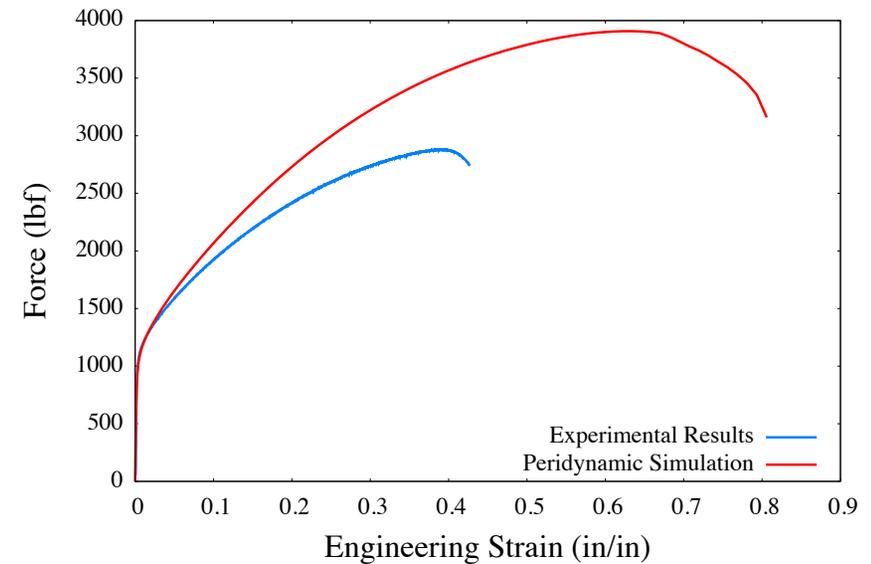
DIRECT TRANSFER OF CALIBRATION PARAMETERS

- Peridynamic horizon and mesh refinement were sufficient for calibration geometry but insufficient for test geometry
- Failed to predict response of test geometry



Experimental DIC image [Boyce]

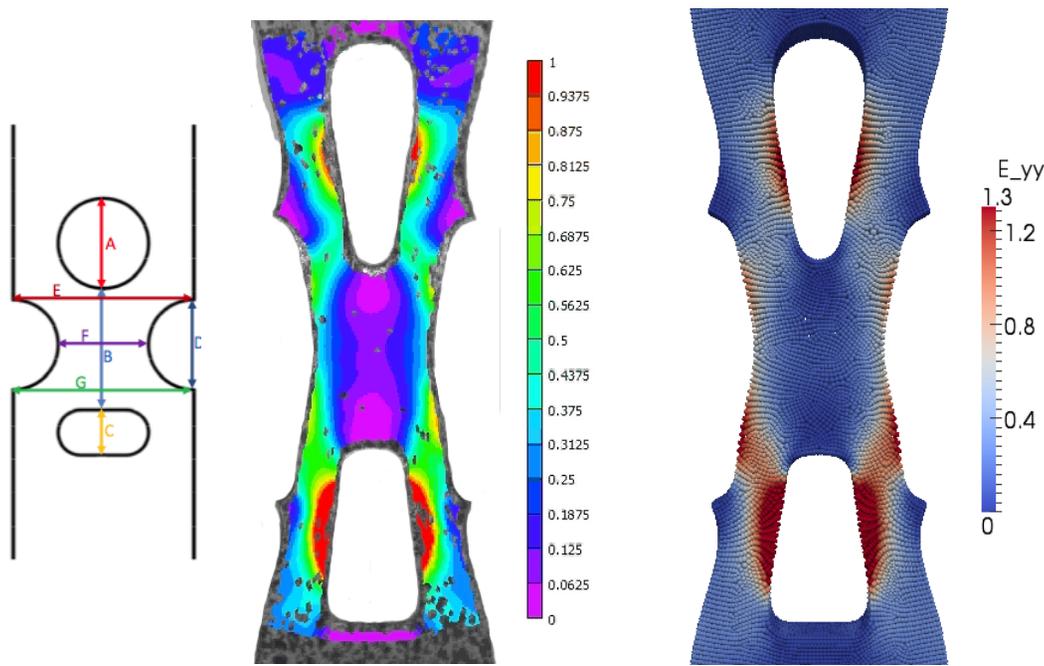
Simulation result



Necking Experiment: Test Geometry

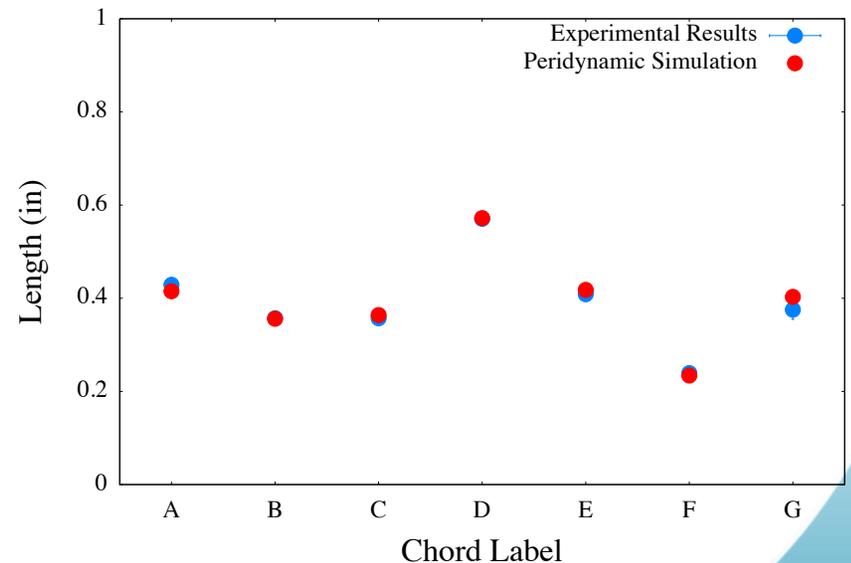
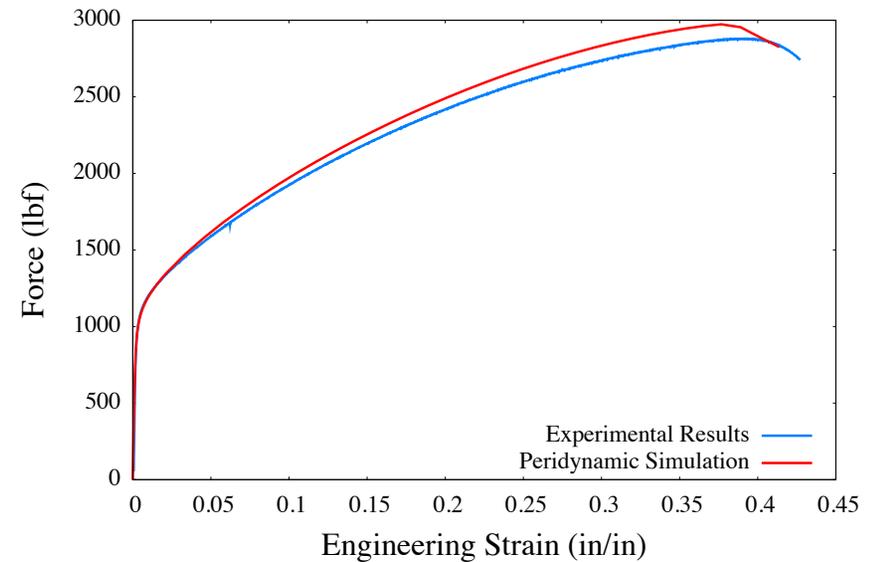
REDUCTION OF PERIDYNAMIC HORIZON

- Peridynamic horizon reduced from 1.055 mm to 0.353 mm
- Mesh density increased from 189K elements to 1,507K elements
- Dramatically improved agreement between peridynamic model and experimental data



Experimental DIC image [Boyce]

Simulation result



Questions?

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RESOURCES

Advanced Simulation and Computing (ASC)

<http://www.sandia.gov/asc/>

Peridigm: A publicly-available peridynamics code

<https://software.sandia.gov/trac/peridigm/>